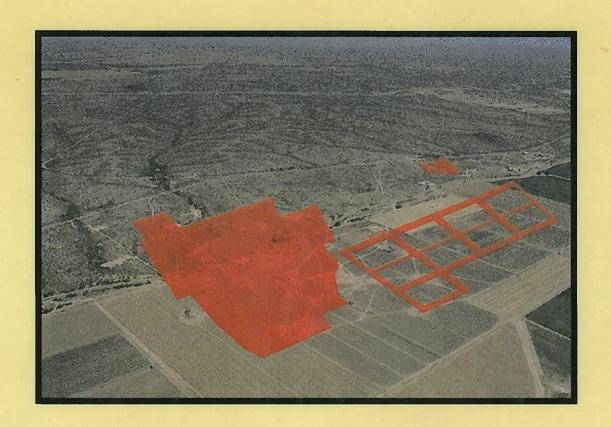
MAGMA

MAGMA COPPER COMPANY



MAGMA FLORENCE IN-SITU PROJECT

Underground Injection Control
Permit Application, Form 4
and
Request for Minor Aquifer Exemption

# UNDERGROUND INJECTION CONTROL PERMIT APPLICATION, FORM 4 AND REQUEST FOR MINOR AQUIFER EXEMPTION

# MAGMA FLORENCE IN-SITU PROJECT

**JANUARY 1996** 





FLORENCE PROJECT

January 19, 1996

Mr. Clyde Morris
Section Chief
Region IX
Environmental Protection Agency
75 Hawthorne Street
San Francisco, California 94105

15-1899/08/09

Subject:

Aguifer Exemption Application and

Underground Injection Control (UIC) Act

Permit Application for the Magma Copper Company

In-situ Leach Mine Florence, Arizona

Dear Mr. Morris:

At the instruction of Mr. Jose Luis Gutierrez, Project Officer for the Magma Copper Company (Magma) in-situ permits, Magma is hereby submitting the Aquifer Exemption Application for a minor exemption as per the requirements of 40 CFR 144-146. Also submitted is UIC Form 4 "UIC Permit Application", along with the required supplemental information.

Also included at the request of Mr. Gutierrez is Volume I of the Aquifer Protection Permit (APP) Application submitted on this same date to the Arizona Department of Environmental Quality (ADEQ), APP Mining Unit. Magma trusts that your staff will find the Aquifer Exemption and UIC Applications complete.

Magma would like to take this opportunity to commend you on the cooperation of your staff, and especially Mr. Gutierrez, in the preparation of these documents. Early on, it was recognized by Magma, the ADEQ, and the EPA that these applications paralleled sections of Arizona's APP Application. Through the suggestions and efforts of Mr. Gutierrez, and Ms. Shirin Tolle, APP Officer, Magma was able to organize the two permits at a substantial reduction of paper work and time. Ms. Tolle, as you are probably aware, is a Region IX EPA employee on temporary duty assignment to the ADEQ.

Magma has appreciated EPA attendance at joint Magma/ADEQ meetings, and in joint meetings with other interested parties.

Submitted with this letter are the following documents required by Mr. Gutierrez:

Volume I - UIC Contains the Aquifer Exemption and UIC Applications.

Volume II Site characterization. Volume II is the exact same volume for the

UIC Application as the APP Application.

Volume III Sampling and Analysis Plan. Same volume for UIC and Arizona

APP Applications.

Mr. Clyde Morris January 19, 1996 Page 2

Volume IV

Hydrogeological Modeling. Same volume for Arizona APP and

UIC Application.

Volume V

Facility Design. Same volume for Arizona APP Application and

UIC Application.

Volume I - APP

APP Application. Submitted at the request of Mr. Gutierrez.

Volume I - Appendix A

This appendix contains confidential business information submitted as part of the Aquifer Exemption Application. Magma claims

confidentiality of this information under 40 CFR 144.5.

Magma is looking forward enthusiastically to working with Mr. Gutierrez and others on your staff over the next several months. This is a breakthrough project for Magma and the copper industry as a whole as this site would be the first fully-operational Class III copper in-situ mining of its type.

Congress, through its funding of the U.S. Bureau of Mines and the Santa Cruz Joint Venture Insitu Project Site in Arizona, has recognized that in-situ mining is an efficient way of meeting the needs of the nation for copper as a strategic metal, and yet doing so in a manner conducive to minimize environmental impacts on the land. Magma believes this mine to be the first of several of its type over the next years.

Sincerely,

John T. Kline

Environmental Project Manager

JTK:kw Enclosures

cc:

Mr. Mike Eamon, Magma Copper Company

Mr. Jose Gutierrez, U.S. Environmental Protection Agency

Mr. Charles Taylor, Magma Copper Company

Ms. Shirin Tolle, Arizona Department of Environmental Protection

CONTENTS

# TABLE OF CONTENTS

		LOSSARY OF TECHNICAL AND MODELING	::
IEKW	15		. 111
SECT	ION 1.0	INTRODUCTION	1-1
1.1		OSE	
1.2		NIZATION	
1.3	GENEF	RAL FACILITY INFORMATION	1-1
SECT	ION 2.0	REQUEST FOR MINOR AQUIFER EXEMPTION	2-1
2.1		FOR EXEMPTION	
	2.1.1	Exempted Aquifer (40 C.F.R. 144.7)	
2.2		ITY DATA	2-2
	2.2.1	Location	
	2.2.2	Prior and Existing Uses	
	2.2.3	General Surface Conditions	2-2
2.3	AQUIF	ER DATA	
	2.3.1	Description of the Regional Groundwater System	2-3
	2.3.2	Groundwater Use	
	2.3.3	Community Drinking Water Systems	2-4
	2.3.4	Agricultural Withdrawals	2-5
•	2.3.5	Nearby Property Owners	2-5
2.4	PROJE	CT TYPE - AREA PERMIT FOR CLASS III WELLS	
	2.4.1	In-Situ Mining Process	
	2.4.2	Injection/Withdrawal Practices	
	2.4.3	Operating Status of Injection/Extraction Wells	2-7
2.5		NG OF ALL US ENVIRONMENTAL PROTECTION AGENCY	
	(USEP	A) PERMITS OR CONSTRUCTION APPROVALS	2-7
2.6		R QUALITY IMPACTS	2-7
2.7		YSES OF ENVIRONMENTAL IMPACTS AND	
	COMM	MITMENT OF RESOURCES	2-7
2.8		PTION CHECKLIST	
2.9	CERTI	FICATION	2-9
SECT	TION 3.0	UNDERGROUND INJECTION CONTROL (UIC) PERMIT	
		APPLICATION FORM 4	
3.1		4	
3.2	FORM	4 CHECKLIST	3-1
SECT	ΓΙΟΝ 4.0	REFERENCES	4-!

# **TABLE OF CONTENTS - Continued**

APPENDICES	
APPENDIX A. APPENDIX B.	PRE-FEASIBILITY STUDY, FLORENCE PROJECT A-1 SECTION 5, VOLUME I AQUIFER PROTECTION PERMIT APPLICATION
	LIST OF TABLES
Table 2.2-1 Table 2.2-2	Property Owners Within 1 Mile
Table 2.3-1	Mile of the In-Situ Mine Area
Table 2.3-2	Within 5 Miles of the Florence In-situ Mine Area 2-12 Summary of Information Concerning Existing Wells
1 4016 2.5-2	Within One-Half Mile of the Florence Project Area 2-22
Table 2.3-3 Table 2.3-4	Large Municipal Water Providers, Pinal AMA, 1985 2-33 Summary of Groundwater Use Within a 5-Mile Radius
1 auto 2.5-4	of the Florence In-Situ Mine Area 2-34
Table 2.5-1 Table 2.8-1	Explanation of the Following Permits
Table 3.2-1	Form 4 - Underground Injection Control (UIC) Permit Application - Information Summary
	LIST OF FIGURES
Figure 2.1-1	Hydrogeologic Cross-Section D-D'
Figure 2.1-2 Figure 2.2-1	Hydrogeologic Cross-Section F-F' Existing Features of the In-Situ Mine Area
	LIST OF SHEETS
Sheet 2.1-1	Florence Project Area Map (10 miles by 10 miles) Showing Locations of Existing Wells and Regional Hydrological Features

# SELECTED GLOSSARY OF TECHNICAL AND MODELING TERMS

To clarify several technical and modeling terms in this application, Magma has prepared the glossary presented on the following pages.

**Alert Level**: A numeric value, expressing either a concentration of a pollutant or a physical or chemical property of a pollutant, which is established in an individual Aquifer Protection Permit and which serves as an early warning indicating a potential violation of either an AWQS at the applicable point of compliance, or any permit condition.

Alteration: Any change in the mineralogic composition of a rock brought about by physical or chemical means, especially by the action of hydrothermal solutions; also, a secondary, i.e. supergene, change in a rock or mineral.

Anion: A negatively charged ion (as a hydroxide, chloride, or acetate ion): the ion in an electrolyzed solution that migrates to the anode and is there discharged and liberated or deposited.

**Application** Verification: Using the set of parameter values and boundary conditions from a calibrated model to verify a second set of field data measured under similar hydrologic conditions.

**Aquifer**: A geologic unit that contains sufficient saturated permeable material to yield usable quantities of water to a well or spring (A.R.S. § 49-201.2). The Aquifer Boundary and Protected Use Classification Rules (A.A.C. R18-11-501.4) have defined "usable quantities" at 5 gallons per day (gpd).

Aquifer: An aquifer is defined (40 C.F.R. §144.3) as a geological formation, group of formations, or part of a formation which is capable of yielding a significant amount of water to a well or spring.

**Aquifer Protection Permit**: An individual or general permit issued pursuant to A.R.S. § 49-221 and 49-223.

Aquifer Water Quality Standards (AWQS): AWQS represent maximum allowable concentrations of a contaminant in surface water or groundwater. AWQS are in numeric and narrative form. Narrative standards as set forth in A.A.C. R18-11-405 prohibit discharges which (a) cause a pollutant to be present in an aquifer classified for drinking water protective use in a concentration which endangers human health, (b) cause or contribute to a violation of surface water quality standard established for navigable waters of the state, or (c) cause a pollutant to be present in an aquifer which impairs existing or reasonably foreseeable uses of water in an aquifer. Numeric standards are set forth in A.A.C. R18-11-406.

# SELECTED GLOSSARY OF TECHNICAL AND MODELING TERMS

Atterberg Limits: In a sediment, the water-content boundaries between the semiliquid and plastic states (known as the liquid limit) and between the plastic and semisolid states (known as the plastic limit).

**BADCT**: The best available demonstrated control technology, processes, operating methods, or other alternatives to achieve the greatest degree of discharge reduction determined for a facility by the Director pursuant to A.R.S. § 49-221 and 49-223.

Calibration: The process of refining the model representation of the hydrogeologic framework, hydraulic properties and boundary conditions to achieve a desired degree of correspondence between the model simulations and observations of the groundwater flow system.

Cation: A positively charged ion (as a hydrogen, calcium, or ammonium ion). The ion in an electrolyzed solution that migrates to the cathode and is there discharged and liberated or deposited.

Chemical Transport: Chemical transport involves further refinement of the groundwater flow model to include simulation of chemical movement and distribution in a groundwater flow system. Chemical transport modeling includes diffusion, dispersion, chemical decay and reactions between the chemical and the porous media.

Conceptual Model: An interpretation or working description of the characteristics and dynamics of the physical system. Conceptualizing the hydraulic system is one of the most important parts of the modeling process. Before a mathematical model can be developed, a conceptual model involves identifying all of the inflows, outflows and hydraulic stresses on the aquifer system.

Constant Flux Boundary: A numerical boundary condition in MODFLOW through which the inflow or outflow flux of groundwater remains constant, and does not vary due to changing groundwater flow gradients.

**Discharge**: Defined as the addition of a pollutant from a facility either directly to an aquifer or to the land surface or the vadose zone in such a manner that there is a <u>reasonable probability</u> that the pollutant will reach an aquifer (A.R.S. § 49-201.10).

Discharge Impact Area (DIA): The "potential areal extent of pollutant migration, as projected on the land surface, as the result of a discharge from a facility." (A.R.S. § 49-201.12). The perimeter of the DIA is the point at which pollutant concentrations are diluted to a level indistinguishable from background concentrations by standard test methods.

**Enrichment**: The supergene processes of mineral deposition, including near-surface oxidation, downward migration, and precipitation, e.g. sulfide enrichment.

# SELECTED GLOSSARY OF TECHNICAL AND MODELING TERMS

**Facility**: Any land, building, installation, structure, equipment, device, conveyance, area, source, activity or practice from which there is, or with reasonable probability may be, a discharge (A.R.S. § 49-201.15).

**Flow Line**: Is a representation of the direction of groundwater flow. Flow lines are always perpendicular to lines of equal groundwater elevation. Flow lines only converge in areas of groundwater discharge or recharge. A groundwater particle trace or pathline is the actual tortuous paths of the water molecules as they flow through pores, cracks and crevices of the soil or other aquifer material.

**Freeboard**: (a) The additional height that is above the recorded or design high-water mark of an engineering structure (such as a dam, seawall, flume, or culvert) associated with a body of water and that represents an allowance against overtopping by transient disturbances. (b) The vertical distance between the water level at a given time and the top of an engineering structure, such as the distance between the normal operating level of a reservoir and the crest of the associated dam.

General Head Boundary: The general head boundary is a numerical constraint in MODFLOW that simulates regional flow beyond the finite difference grid. The general head boundary will adjust the flux of water in or out of the model depending on simulated groundwater flow gradients.

Granodiorite: A group of coarse-grained plutonic rocks intermediate in composition between quartz diorite and quartz monzonite, containing quartz, plagioclase (oligoclase or andesine), and potassium feldspar, with biotite, hornblende, or more rarely, pyroxene, as the mafic components. The ratio of plagioclase to total feldspar is at least 2 to 1 but less than 9 to 10. With less alkali feldspar it grades into quartz diorite, and with more alkali feldspar, into granite or quartz monzonite.

**Gravity Anomaly**: The difference between the observed value of gravity at a point and the theoretically calculated value is based on a simple gravity model, usually modified in accordance with some generalized hypothesis of subsurface density variation as related to surface topography.

**Hydraulic Conductivity**: Hydraulic conductivity describes the ease with which water can pass through an aquifer. The hydraulic conductivity multiplied by the thickness of the aquifer is equal to the transmissivity.

**Hydraulic Gradient**: (a) In an aquifer, the rate of change of pressure head per unit of distance of flow at a given point and in a given direction. (b) In a stream, the slope of the hydraulic grade line.

# SELECTED GLOSSARY OF TECHNICAL AND MODELING TERMS

**Hydraulic Head**: (a) The height of the free surface of a body of water above a given subsurface point. (b) The water level at a point upstream from a given point downstream. (c) The elevation of the hydraulic grade line at a given point above a given point of a pressure pipe.

**Hydrothermal**: Of or pertaining to heated water, to the action of heated water, or to the products of the action of heated water, such as a mineral deposit precipitated from a hot aqueous solution, with or without demonstrable association with igneous process (also, said of the solution itself).

**Hydrothermal Alteration**: Alteration of rocks or minerals by the reaction of hydrothermal water with pre-existing solid phases.

Injection Well: A well which receives a discharge through pressure injection or gravity flow.

**Modflow**: The United States Geologic Survey (USGS) Modular Three-Dimensional Finite Difference Groundwater Flow Model. By McDonald and Harbaugh, 1988.

MT3D: A Modular Three-Dimensional Finite Difference Chemical Transport Model. By Chunmiao Zheng (Papadopulos and Associates), 1990.

Oxide: A mineral compound characterized by the linkage of oxygen with on metallic element, such as cuprite, Cu<sub>2</sub>O, rutile, TiO<sub>2</sub>, or spinel, MgAl<sub>2</sub>O<sub>4</sub>.

**Oxidized Zone**: An area of mineral deposits modified by surface waters, e.g. sulfides altered to oxides and carbonates.

**PATH3D**: A Ground-Water Path and Travel-Time Simulator. By Chunmiao Zheng (Papadopulos and Associates) 1992. A general particle tracking program for calculating groundwater paths and travel times in steady-state or transient two- or three-dimensional flow fields.

Particle Tracking: A technique is used to trace out flow paths, or pathlines, by tracking the movement of infinitely small imaginary particles placed in the groundwater flow field. Particle tracking is primarily used to understand the transient movement of groundwater flow and calculate groundwater travel times.

Point of Compliance (POC): Defined as a vertical plane downgradient of the facility that extends through the uppermost aquifer(s) underlying the facility (A.R.S. § 49-244). AWQS may not be violated at the POC as a result of discharge from the facility. If a pollutant already violates an AWQS at the POC, a discharge cannot cause further degradation of the aquifer at the POC by that pollutant (A.R.S. § 243.B.3). Separate POC may be defined for hazardous and non-hazardous substances. For hazardous substances, the POC is the limit of the pollutant

# SELECTED GLOSSARY OF TECHNICAL AND MODELING TERMS

management area (the area on which pollutants are or will be placed), which can include dams, dikes or other retaining structures (A.R.S. § 49-244.1). An alternate hazardous POC may be designated if it is demonstrated that it is technically impractical to monitor at the downgradient edge of the pollutant management area, or that an alternative POC will allow installation and operation of the monitoring facilities at substantially lower cost (A.R.S. § 49-244.2). It must, however, be located in the downgradient direction no further from the source of discharge than 750 feet or the property boundary, whichever is closer. A non-hazardous POC must be located as to ensure protection for current and reasonably foreseeable future uses of the aquifer (A.R.S. § 49-244.3).

**Porosity**: Porosity is the amount of void space between soil or rock particles, and reflects the ability of the aquifer to store water.

**Porphyry**: An igneous rock of an composition that contains conspicuous phenocrysts in a fine-grained groundmass; a porphyritic igneous rock.

**Porphyry Copper**: A copper deposit in which the copper-bearing minerals occur in disseminated grains and/or in veinlets through a large volume of rock. Today, the term implies a large low-grade disseminated copper deposit which may be also in schist, silicated limestone, and volcanic rocks, but quartz-bearing igneous rocks are always in close association.

**Public Water System:** A public water system is defined (40 C.F.R. §142.2(k)) as a system for the provision to the public of piped water for human consumption, if such system has at least 15 service connections or regularly serves an average of at least 20 individuals daily at least 60 days out of the year.

Quartz Monzonite: Granitic rock in which quartz comprise 10 percent to 50 percent of the felsic constituents, and in which the alkali feldspar/total feldspar ratio is between 35 percent and 65 percent; the approximate intrusive equivalent of rhyodacite. With an increase in plagioclase and femic minerals, it grades into granodiorite, and with more alkali feldspar, into a granite.

**Sewage**: Wastes from toilets, baths, sinks, lavatories, laundries, and other plumbing fixtures in residences, institutions, public and business buildings, mobile homes, watercraft, and other places of human habitation, employment, or recreation.

**Sewage Disposal System**: A system for sewage collection, treatment, and discharge by surface or underground methods.

# SELECTED GLOSSARY OF TECHNICAL AND MODELING TERMS

**Substances**, **Hazardous**: Substances defined as hazardous under various laws and regulations, including:

- Any substance designated pursuant to §§311(b)(2)(a) and 307(a) of the Clean Water Act.
- Any element, compound, mixture, solution or substance designated pursuant to §102 of Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA).
- Any hazardous waste having the characteristics identified under or listed pursuant to §49-922.
- Any hazardous air pollutant listed under §112 of the Federal Clean Air Act (42 United States Code §7412).
- Any imminently hazardous chemical substance or mixture with respect to which the administrator has taken action pursuant to §7 of the Federal Toxic Substances Control Act (15 United States Code §2606).
- Any substance which the director of the Arizona Department of Environmental Quality, by rule, either designates as a hazardous substance.

Sulfide: A mineral compound characterized by the linage of sulfur with a metal or semimetal, such as galena, PbS, or pyrite,  $FeS_2$ .

**Sulfide Zone**: An area of enrichment of sulfide deposits that have not yet been oxidized by near-surface waters.

Supergene: A mineral deposit or enrichment formed by descending solutions; also, refers to those solutions of that environment.

**Surface Impoundment**: A pit, pond or lagoon, having a surface dimension that is equal to or greater than its depth, which is used for the storage, holding, settling, treatment or discharge of liquid pollutants or pollutants containing free liquids.

Storativity/Specific Yield: Storativity and specific yield are related parameters. Storativity is defined as the amount of water released or added to storage per change in pressure due to pumping or recharge in a confined aquifer. Specific yield is the percentage of water that would drain from a unit volume of aquifer material (i.e., 1 cubic foot) in an unconfined aquifer. For coarse sands and gravel, the specific yield is roughly equal to the porosity. Storativity and

# SELECTED GLOSSARY OF TECHNICAL AND MODELING TERMS

specific yield control the time it will take for changes in pumping or recharge to propagate throughout the aquifer system.

**Temporary Cessation**: Any cessation of operation of a facility for a period of greater than 60 days but which is not intended to be permanent.

**Transmissivity**: In an aquifer, the rate at which water of the prevailing kinematic viscosity is transmitted through a unit width under a unit hydraulic gradient. Though spoken of as a property of the aquifer, it embodies also the saturated thickness and the properties of the contained liquid.

Underground Source of Drinking Water (USDW): A USDW is defined at 40 C.F.R. §144.3 as an aquifer or its portion which:

- 1. a. supplies any public water system; or
  - b. contains sufficient quantity of groundwater to supply a public water system; and
    - (1) currently supplies drinking water for human consumption; or
    - (2) contains fewer than 10,000 milligrams per liter (mg/L) total dissolved solids (TDS); and
- 2. is not an exempted aquifer.

Vadose Zone: A subsurface zone containing water under pressure less than that of the atmosphere, including water held by capillarity; and containing air or gases generally under atmospheric pressure. This zone is limited above by the land surface and below by the surface of the zone of saturation, i.e. the water table.

**Zone of Saturation**: A subsurface zone in which all the interstices are filled with water under pressure greater than that of the atmosphere. Although the zone may contain gas-filled interstices or interstices filled with fluids other than water, it is still considered saturated. This zone is separated from the zone of aeration by the water table.

### **SECTION 1.0**

#### INTRODUCTION

## 1.1 PURPOSE

The Magma Copper Company (Magma) is herewith submitting to the United States Environmental Protection Agency (EPA), Region 9, the enclosed Underground Injection Control (UIC) Permit Application, Form 4, and a related request for a minor aquifer exemption. The EPA approvals will enable Magma to proceed with the development and operation of an in-situ copper mining operation near Florence, Arizona.

Magma has also submitted a five-volume application for an Aquifer Protection Permit (APP) to the Arizona Department of Environmental Quality (ADEQ). Approval of the APP will also be required before Magma may proceed with its Florence Project.

# 1.2 ORGANIZATION

This document contains both the request for a minor aquifer exemption and the UIC Permit Application. General facility information applicable to Form 4 and the exemption request is presented in Section 1.3 below.

Information that explains and supports the request for minor aquifer exemption is provided in Section 2.0. The Region 9 Aquifer Exemption Guidance Manual dated March 1993 was used in the development of Section 2.0 and in the development of the aquifer exemption checklist which is provided in Section 2.0.

Section 3.0 includes the UIC Permit Application Form 4. It also includes a checklist that provides a cross-reference to information supporting the application. Items presented in the checklist are listed in order of the attachments specified under Item XI of Form 4.

Much of the information presented in this volume or referenced in the checklists is found in Volumes II through V of the APP Application. To ensure that both the EPA and the ADEQ have the same information, Magma has provided copies of the five-volume APP Application to Region 9, EPA and has provided copies of this volume to ADEQ.

# 1.3 GENERAL FACILITY INFORMATION

Magma Copper Company (Magma) refers to the proposed facility as the Florence Project. The following serves as both the facility address and mailing address:

Magma Copper Company Florence Project 14605 East Hunt Highway Florence, Arizona 85232 For correspondence concerning this application, the facility contact person is:

Mr. John Kline Magma Copper Company 14605 East Hunt Highway Florence, Arizona 85232

Telephone Number: (520) 868-5094 FAX Number: (520) 868-0463

The required information in regards to the responsible party for the Florence Project is presented below:

Owner of Magma Copper Company

Operation: Suite 200

7400 North Oracle Road Tucson, Arizona 85704

Telephone Number: (520) 575-5600 FAX Number: (520) 575-5639

Operator: Magma Copper Company

Florence Project

14605 East Hunt Highway Florence, Arizona 85232

Telephone Number (520) 868-5094 FAX Number: (520) 868-0463

# **SECTION 2.0**

# REQUEST FOR MINOR AQUIFER EXEMPTION

# 2.1 NEED FOR EXEMPTION

Magma requests the proposed minor aquifer exemption in order that the Environmental Protection Agency (EPA) may proceed with the review and approval of Magma's UIC application for an area permit. The requested permit will enable Magma to develop a facility to recover copper from the orebody that lies below the water table.

The copper will be extracted by use of in-situ leach mining methods. In-situ mining is a technically and economically viable approach, and allows the mining to be conducted with minimal land disturbance. Normal open-pit mining was considered, but is not a preferred alternative as it produces a sizable land disturbance and provides a lower economic outcome.

The area for which the exemption is requested covers the areal extent of the orebody (about 300 acres) and buffer zone extending 1/2-mile outward. There is no other area which could be considered for mining the orebody.

The proposed injection zone is not now used as source of drinking water and will not be used as a source of drinking water during the 15-year life of the mine. Simulation models were used to evaluate the impacts of the proposed mining operation. The models indicate that the proposed mining operation will not interfere with known or reasonably foreseeable sources of drinking water and as such meets the requirements of 40 C.F.R. 146.4 (a). Information presented in Appendix A of this volume demonstrates the economic viability of the proposed mining operation and establishes the economic justification for the exemption in accordance with 40 C.F.R. 146.4 (b)(1). Appendix A includes operating costs, capital costs, and profitability numbers, that is released, may cause loss of competitive advantage in the sale and revenues of the copper produced at Florence.

The economic justification in Appendix A of this volume includes information that is considered confidential, and is marked with the words "CONFIDENTIAL BUSINESS INFORMATION" in compliance with 40 C.F.R. 144.5.

Information included in the application and attached volumes further explain the need for the exemption and the potential impact of this relatively small site within the 100-square-mile impact study area.

Magma submits the application to mine the in-situ resource in compliance with regulatory goals to reduce waste and minimize pollution. In-situ leaching will leave virtually no impact on the surface of the land after closure when compared to other mining methods.

# 2.1.1 Exempted Aquifer (40 C.F.R. 144.7)

The area for which Magma is requesting exemption includes the copper mineralized zone shown in the attached plan view (Sheet 2.1-1 [UIC]). Two typical cross sections are shown that illustrate the outline of the orebody. The orebody is located approximately 350 to 1,240 feet below land surface. Figure 2.1-1 (UIC) is a typical east-west section and Figure 2.1-2 (UIC) is a typical north-south section. Magma is requesting a minor exemption that extends horizontally outward from the orebody 1/2 mile. The planned production schedule includes the copper extraction rate for the life of the mine.

# 2.2 FACILITY DATA

#### 2.2.1 Location

The 213-acre in-situ mine area is located approximately 1 mile west/southwest of Poston Butte and 2 miles northwest of Florence, Arizona (as shown on Sheet 2.1-1 [UIC]). The Gila River trends west-southwest and is located approximately 1/2 mile south of the mine area.

# 2.2.2 Prior and Existing Uses

Magma purchased the mine property from Conoco Oil Company in 1992. Conoco operated the underground mine during the 1970s but ceased activities by 1975. Magma controls the uses of the water within the proposed boundary. The mine site and the few homes associated with Magma's drilling and farming operations use imported bottled water and not well water for drinking due to excessive nitrate levels in the water. The area will not be used for drinking water in the future as Magma owns or controls the land.

Three irrigation wells are located on the mine site. Two of these wells are used by the San Carlos Irrigation and Drainage District (SCIDD) and discharge to the North Side Canal. The remaining installation is utilized by local farmers and discharges into small irrigation ditches. The wells are generally located near the center of the site along the SCIDD Canal. Tables 2.2-1 and 2.2-2 provide the addresses of the property owners in the area and contains more information related to these wells. Use of irrigation wells that could potentially interfere with leaching operations will either be closed or relocated to other areas of Magma's 10,000-acre property.

# 2.2.3 General Surface Conditions

The project site is located on both agricultural and undisturbed land. It is at a nominal elevation of 1,475 feet above sea level. The elevation of the site declines approximately 25 feet from north to south. At least three river terraces are present on the site. These terraces mark past base levels and northern extent of the active channel of the Gila River. The northern-most extent of the active floodplain is currently located approximately 1/4 mile south of the mine site.

The surface of the project site can be divided into two segments based on land usage. As depicted in Figure 2.2-1 (UIC), this division occurs approximately where the San Carlos Irrigation and Drainage District (SCIDD) North Side Canal traverses the property. The southern portion is dominated by agricultural activities, whereas the northern portion has remained relatively

undisturbed desert land. Numerous archaeological sites exist in the northern portion. Primary disturbances north of the canal consist of dirt roads. These roads provide access from Hunt Highway to adjacent agricultural and mine-related areas. The Southern Pacific Railroad also passes north of the proposed site.

# 2.3 AQUIFER DATA

# 2.3.1 Description of the Regional Groundwater System

The Arizona Department of Water Resources (ADWR) has divided the saturated materials within the area into four main hydrogeologic units. The Upper Alluvial Unit is analogous to the Upper Basin-Fill Unit (UBFU) referenced in this report. The Middle Silt and Clay Unit is analogous to the Middle Fine-Grained Unit (MFGU), and separates the UBFU and Lower Basin-Fill Unit (LBFU). The Lower Conglomerate Unit is analogous to the LBFU referenced in this report. The Hydrologic Bedrock Unit is similar to the bedrock zones referenced in this report.

The Upper Alluvial Unit consists mainly of unconsolidated to slightly consolidated, interbedded gravels, sands and silt, with some finer-grained materials existing as lenses. The lower half to one-third of this unit is a transition zone containing interbedded-coarse and fine-alluvial material typical of the underlying Middle Silt and Clay Unit. The upper alluvial unit is a significant aquifer throughout the area, with well yields that have been reported up to 3,000 gallons per minute (gpm).

The Middle Silt and Clay Unit generally separates the upper basin-fill from the lower basin-fill. This fine-grained unit is reported to be laterally extensive throughout the basin. Near the margins of the basins, this unit may not be distinguishable from the overlying or underlying materials. The Middle Silt and Clay Unit is known for groundwater production in and of itself in the Eloy sub-basin. The middle alluvial unit has been intercepted during drilling at the in-situ mine area, and has been identified on off-site water well logs for wells within the 100-square mile Florence Project Area (see Sheet 2.1-1 [UIC]).

The Middle Silt and Clay Unit has been divided into two sub-units (Hardt and Chattany, 1965). The uppermost sub-unit consists of about 90 percent clay with intermittent gravel and sand lenses. This sub-unit has been described in core and water well logs throughout the study area as presented in Volume II of the Aquifer Protection Permit Application. The lower fine-grained sub-unit is the thickest and is found in deeper areas of the basin where which it may exceed 3,000 feet in thickness (Hardt and Chattany, 1965). It is predominantly an evaporite unit consisting of anhydrite with minor clay and silt. This sub-unit has been identified to the north and northeast of the proposed mine site, but not within 3 miles of the site.

Beneath the Middle Silt and Clay Unit is the Lower Alluvial Unit. This unit is also known as the Lower Conglomerate Unit, as reported by Montgomery (1994) and Conoco (1976). It is the deepest alluvial unit in the Eloy basin and was intercepted during current investigation drilling activities. The lithology of the Lower Alluvial Unit is characterized by semi-consolidated to consolidated coarse sediments consisting of granite fragments, cobbles, boulders, sands, and gravels.

The Lower Alluvial Unit locally produces groundwater. In many cases, yields from wells penetrating the lower basin-fill can exceed 1,000 gpm and can be as large as 2,500 gpm (Montgomery, 1994). Where the lower basin-fill occurs directly beneath the middle fine-grained unit, groundwater may exist under confined or semi-confined conditions. Where the Lower Alluvial Unit is in direct contact with the Upper Alluvial Unit groundwater exists under generally unconfined conditions.

The Lower Alluvial Unit rests on fractured and faulted bedrock. The bedrock consists of Precambrian granite, gneiss, and schist. The bedrock is considered to be impermeable and non water-bearing compared to the basin-fill units, but is reported to be locally permeable in areas where it is highly fractured. Many wells completed in the area are screened in the basin-fill units as well as the bedrock.

# 2.3.2 Groundwater Use

Based on ADWR records through May, 1995 (ADWR, 1995), there are 382 registered wells within the 100-square mile Florence Project Area. Sheets 2.1-1 (UIC) and 2.1-2 (UIC) show the locations of these wells. As presented in Table 2.3-1, these wells are used for irrigation, domestic, public water supply, and monitoring purposes. Agricultural and municipal entities are the primary consumers of groundwater in the project area.

Water well data (ADWR, 1995) are more concentrated east and west of the Florence Project Area where the thickness of the basin-fill units is greater. With the exception of the Gila River channel area, water well log coverage is significant south of the Florence Project Area. However, wells in this area are generally less than 500 feet deep and do not encounter bedrock. Very few water wells are located within 2 miles north of the Florence Project Area. This area does contain exploration coreholes. Sheet 2.1-1 (UIC) shows locations of water wells with available logs and other information.

# 2.3.3 Community Drinking Water Systems

The Town of Florence owns five public supply wells in the general vicinity of the Florence Project area. Two wells are located approximately 2 1/2 miles east of the Florence proposed insitu mine area at Florence Gardens. Three wells are located in the Town of Florence, approximately 3 miles southeast of the mine area (see Sheet 2.1-1 [UIC]). The three wells located in the Town of Florence provide drinking water to the residents and businesses of Florence. The two wells located at Florence Gardens provide drinking water to the residents of Florence Gardens, the Air National Guard (ANG), and the Immigration and Naturalization Service (INS).

The Arizona Department of Corrections owns two water supply wells; one located approximately 2 1/2 miles south, and one located approximately 3 miles east of, the proposed in-situ mine area (see Sheet 2.1-1 [UIC]). These wells provide drinking water to approximately 4,200 inmates at the Florence Complex of the Arizona State Prison. The majority of privately owned domestic wells are located outside of the Florence Project Area region serviced by the Town of Florence, in rural areas to the south of the project area. Tables 2.3-1 and 2.3-2 present additional information concerning these wells.

Table 2.3-3 summarizes large municipal water providers in the Pinal AMA (ADWR, 1995). Of the providers listed in Table 2.3-3, the Arizona State Prison at Florence and the Town of Florence are within 5 miles of the proposed in-situ mine area (see Sheet 2.1-1 [UIC]). Groundwater pumped from wells in 1985 which serve these two entities, as presented in Table 2.3-3, consist of 1,055 acre/feet (ac-ft) and 1,284 ac-ft, respectively.

# 2.3.4 Agricultural Withdrawals

The majority of groundwater reported in Table 2.3-4 is used by SCIDD, which is an element of San Carlos Irrigation Project (SCIP). SCIP is the primary user of surface water diverted from the Gila River and groundwater pumped from the area. The other primary element of SCIP is Gila River Indian Community (GRIC). Approximately 80 percent of the land in the region is used for agriculture (Beer, 1988). The main crop is cotton which is watered using flood irrigation methods. Approximately 12 percent of the farmers in the area use groundwater from private wells. The remaining farms utilize surface water supplied by SCIDD through three canals; the Florence-Casa Grande Canal, the North Side Canal, and the Florence Canal.

# 2.3.5 Nearby Property Owners

There are only two property owners within the 1/2-mile exemption boundary other than Magma. Sheet 2.1-1 (UIC) shows that ASARCO, Inc., another mining company, has a portion of their land that lies to the west of the proposed in-situ mine site. There are no wells of any type found on that land.

A portion of land owned by the State of Arizona lies in the south half of Section 28 of Township 4 South, Range 9 East. This land is leased to Magma under Mineral Lease 11-26500. Another portion of State of Arizona land lies in the northeast corner of the proposed exemption area. Again, there are no wells on that land either.

The San Carlos Irrigation District (SCID) has two irrigation wells located inside the 1/2-mile exemption area. These wells will be closed and replaced outside of the exemption area prior to mining operations.

# 2.4 PROJECT TYPE - AREA PERMIT FOR CLASS III WELLS

Magma plans to commence facility construction in March 1997 and to ship the first copper in January 1998. Operations are expected to continue for approximately 15 years.

# 2.4.1 In-Situ Mining Process

Magma proposes to mine copper at the facility using an in-situ leaching process. The process involves the following principal components:

• A series of injection wells to inject diluted sulfuric acid into selected segments of the copper oxide orebody.

- A series of recovery wells to recover copper sulfate solutions from the orebody.
- A series of hydraulic control wells to prevent production fluids from entering the surrounding aquifer.
- A solvent extraction/electrowinning (SX/EW) plant to recover copper from the production fluids.
- A neutralization unit to neutralize raffinate (spent sulfate solutions).
- An evaporation/tailing impoundment to contain and evaporate neutralized raffinate.
- An impoundment to collect stormwater and or spills.
- Fuel and chemical storage tanks.

A detailed description of the operational components associated with the proposed in-situ facility are presented in Volume V of this application.

The classification of the wells will be Class III. There will be 2,000 to 3,000 wells drilled and used during the expected 15-year mine life; therefore, this is an application for an area permit as described in 40 C.F.R. 144.33. The project type is extraction of copper. The classification of wells is described in 40 C.F.R. 144.6 (c) (2).

# 2.4.2 Injection/Withdrawal Practices

For purposes of this application, the analysis of the production well field contains an array of design, operational and closure components, and an evaluation of the alternatives related to these components. These environmental control aspects are coupled with the opportunity to optimize resource recovery throughout the life of the project.

Magma has developed a reference design that incorporates the most advanced discharge control technologies (DCTs) commercially available. Many of these technologies have been demonstrated to be effective in controlling fluid migration in related industrial applications, including oil and gas resource recovery, construction dewatering, and groundwater remediation. These cross-over technologies are only applicable to the acidified solution recover of oxide copper reserves of the subject orebody by recognizing the site specific hydrogeologic conditions of the Florence site, and the chemical and physical characteristics of the process fluids. In recognition of these factors, Magma has developed a design, operational approach and closure strategy that demonstrates the ability to meet the requirements of Underground Injection Control (UIC) regulations.

The Magma Florence oxidized copper orebody lies below the water table. The orebody is slated for in-situ leach extraction of its metallic values through deep well injection of acidified raffinate and pumped well recovery peripheral to the point of injection. Therefore, key elements of the

Magma Florence in-situ operations plan include: (1) hydraulic control to prevent excursions beyond the perimeter of the mined area; (2) corrective actions to prevent existing boreholes from becoming conduits for acidified process fluids; and (3) the proper design, construction and operation of the well system, including applicable verification of through mechanical integrity testing. Equally important is the close-as-you-go concept which is discussed in Section 2.7.

# 2.4.3 Operating Status of Injection/Extraction Wells

There are no operating wells at this time.

# 2.5 LISTING OF ALL US ENVIRONMENTAL PROTECTION AGENCY (USEPA) PERMITS OR CONSTRUCTION APPROVALS

Magma's Florence mine is not yet in operation and, as such, has few permits. Information presented in Table 2.5-1 shows the status of permits listed.

Permit requirements for Florence include an Aquifer Protection Permit (APP) from Arizona Department of Environmental Quality (ADEQ). In addition, an Air Quality Permit from Pinal County for the boilers, metal furnaces, and dust collection system for the processing plant will be required. The Arizona State Land Department will require a Mine Plan of Operation for those areas of the in-situ leaching that will occur on State lease land. Mineral lease 11-26500 is in place, but the current Mine Plan of Operations covers only exploration drilling. The ADWR will require permits for injection wells, monitor wells, and hydraulic control wells.

Under 40 C.F.R. Part 144 of the Safe Drinking Water Act (SDWA), the in-situ operation must be approved prior to operation for an aquifer exemption and a Class III Underground Injection Control (UIC) Permit issued. Under the UIC Permit program, the mine will have to show compliance with the Endangered Species Act (ESA), National Historic Preservation Act (NHPA), and the Fish and Wildlife Coordination Act (FWCA).

# 2.6 WATER QUALITY IMPACTS

Potential impacts on groundwater quality have been carefully evaluated and described in Magma's APP application. Section 5.0, Volume I, of the APP Application provides a brief overview of those evaluations and is attached to this application as Appendix B. As described therein, state-of-the-art models were used to evaluate the potential impacts of the proposed in-situ mining operation. the models indicate that drinking water quality standards will be maintained at the boundaries of the in-situ mine area during operations and during the 30-year post-closure period.

# 2.7 ANALYSES OF ENVIRONMENTAL IMPACTS AND COMMITMENT OF RESOURCES

Magma Copper Company's (Magma) policy is to effect closure on an on-going basis during operation. Once a series of wells has depleted an ore zone of copper, closure will begin in phases expected to last about 18 months each. The closure process will begin with a period where only injection occurs without acid being added. This period will be followed by a rest period of about 1 week to 1 month, depending on the acid consumption residual in the leach ore. The solutions

will then be withdrawn without injection. Withdrawal will continue until the copper and acid values drop to a low level in the solutions pumped from the spent orebody. There may then be a period where fresh water will be injected or infiltrated to sweep the ore zone in the leached area. The solution pumped during these periods will be added to the process stream and any residual acid will be consumed by the production of copper in other areas. The copper will then be removed and processed in the solvent extraction/electrowinning (SX/EW) plants.

Throughout the closure process, Magma will maintain hydraulic control over all regions of the orebody that have been subjected to in-situ leaching. During active sweeping of the individual ore blocks, this control will be accomplished in the same manner as that utilized during leaching. This approach will use surrounding recovery wells as a means of sustaining an inward gradient around the region being closed. After sweeping and reduction of the concentrations of dissolved constituents, a series of secondary control wells will continue to function and serve to capture any affected groundwater within the confines of the proposed in-situ mine area. The effectiveness of both the primary and secondary control strategies has been demonstrated as part of the groundwater modeling simulations presented in Volume IV.

The advantages of the close-as-you-go process is that water is used in an economical manner, as water must be added to the system to compensate for salts bled to the Evaporation/Tailings Pond. The net result is that most of the orebody will have been rinsed of the majority of sulfate and other leachable ions during normal operation. The closure cost will be absorbed as part of the normal operating cost, and will be accrued and expensed at an estimated \$0.035 per pound of copper produced, as described more fully in Appendix A.

Once the last set of wells on line begin closure, it is expected that closure of these wells will take less than 1 year. Again, the process solutions will ultimately be neutralized and reside in the Evaporation/Tailings Pond.

The rinse solution during the sweep operation will be analyzed for sulfate. When the sulfate level decreases to below a level of 750 parts per million (ppm), then the wells will be shut down and closed in accordance with the well closure plan. The ultimate goal is to flush to a level where, upon closure, no hazardous or non-hazardous constituents will exceed Arizona Water Quality Standards (AWQS) at the Point of Compliance (POC).

Magma believes that environmental impacts will be temporary and limited to the aquifer exemption area and only during the life of the mine. Residual waters remaining in the ore zone after closure will meet primary drinking water standards, and consequently there will be no long term or irreversible environmental impacts. The operation of the in-situ leaching mining operation will allow recovery of the copper resource that otherwise would have been lost.

# 2.8 EXEMPTION CHECKLIST

Table 2.8-1 (UIC) is submitted as an aid to the Environmental Protection Agency (EPA) in determining completeness. The left column is the regulatory guidelines while the right two columns indicate the reference location of the required information and any pertinent comments.

# 2.9 CERTIFICATION

I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

Bradford A. Mills, Executive Vice President NAME AND OFFICIAL TITLE

SIGNATURE

DATE SIGNED

TABLES

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Table 2.2-1 Propert	y Owners Within 1 Mile of t	the In-situ Mine Area	
Company or Individual	Address	Approximate Acres	Direction from the In-situ Mine Area
Scott Riggins	P.O. Box 2150 Coolidge, AZ 85228	300	West
ASARCO, Inc.	Duane Yantorno 1150 N. 7th Avenue Tucson, AZ 85705	394	West
State of Arizona	Shirin Tolle 3033 North Central Avenue Phoenix, AZ 85012	182	Northeast

			1002 37/-4	1004 \$\$7-4
ADWR Registration Number	Well ID	Owner	1993 Water Use (Acre-Feet)	1994 Water Use (Acre-Feet)
55-627614	D(4-9)27cad Supply Well 1	Magma Copper Company	0.00	0.00
55-627612	D(4-9)27cbd1 England No. 3	Magma Copper Company	210.67	519.90
55-627611	D(4-9)27ddd England No. 2	Magma Copper Company	66.03	416.07
55-627608	D(4-9)28cdb WW3, PW-3	Magma Copper Company	395.40	754.66
55-609666	D(4-9)29dab	Riggins Pinal	0.00	0.00
55-609667	D(4-9)29dac	Riggins Pinal	0.00	0.00
55-627610	D(4-9)29dca PW-20	Magma Copper Company	217.66	511.20
55-609672	D(4-9)32baa2	Riggins Pinal	471.50	859.34
55-609671	D(4-9)32bda	Riggins Pinal	0.00	0.00
55-609668	D(4-9)32cbd1	Riggins Pinal	517.96	730.60
55-609670 .	D(4-9)32cbd2	Riggins Pinal	379.36	593.13
55-609669	D(4-9)32dda	Riggins Pinal	0.00	0.00
55-627609	D(4-9)33aad PW-4	Magma Copper Company	0.00	0.00
Total Water Use			2,258.58	4,384.90

NA - Not applicable Source: ADWR, 1995

See Appendix B for additional well information See Sheet 1.2-2 for locations

				C	asing		Reported	Surface			Non-P	umping Ws	ter Level				
ell Number	Owner *	Date Completed	Depth Drilled (ft)		Depth (ft)	Perforated Interval (ft)	Pumping Rate (gpm)	Elevation (ft, msl)		Measured Depth (ft)		Date	Altitude (ft, msl)	Logs	Chemical Analyses <sup>k</sup>	Use	Remarks <sup>1</sup>
(D-04-08) laaa	Nalbandian Farms	0440	472	20	472	178-460	699	1,528		149.3		6/11/41	1,378.70	D		lr	55-610620
lbaa	MAGMA	8-22-75	800	3	800	440-800	4	1,518.40	S	429	R	8/22/75	1,089.40	D		M	55-627625; UTL
Ibca	U.S.Army Engineers	2-1-68	201	12	200		107	1,510	Ε	75	R				***	D	55-651042
2aaa1	Conkie	5-8-41	647	20	647	130-625	1,140	1,515		321	•••	2/12/63	1,194.00	D	RP	U	55-610411; chkd; UTM; obstructed; loose cap
2aaa2	Collinic			20				1,515		382.5		11/15/91	1,132.50			U	Chkd; UTM; obstructed; uncapped
2aaa3	Conkle	2-8-80	520	10	467	380-467	***	1,515		381.1		3/3/93	1,133.90	D		U	Chkd; uncapped
Zanas	COIRIC			8	440-520	467-520			,								
2aad	Zellweger	8-13-57	400	20	400	269-400		1,509								U	Also reported as 2add
. 2add	Conkle	5-10-05	600	20	600			1,508	E	425	R	***		D		***	55-610413
	Conkle	9-20-52	338	20	338	208-322		1,520	٠	Dry		12/1/82		D		D	55-610412; registered as 2abb
2baa	********	3-27-41		20		***		1,532		240.2		3/3/93	1,291.80	D		U	Chkd; uncapped
2ccc	Conkle	4-30-05	485		485			-,					***				
				3	40			1,505	Е	155	R			D		İr	
12acc	Johnson	4-22-05	355 500					1,502	E							lr	***
12ccd	Thompson	***			500			1,479		210.2		3/3/93	1,268,80		***	E	55-504706; chkd; capped
13ddc	Conoco		500	6			35	1,525	E	135	R	3/3/73	-,			D	55-602458
14baa	Hooper	4-12-05	200	10	200		33	1,525	E	150	R					lr.	55-623857
14caa	Wolfswinkle	0652	370	16	265	***	25	1,525	E	150	···					D.	55-518644
14ddc	Vermeer								E							lr	55-623861
23acb	Wolfswinkle						***	1,520							***	ir Ir	55-623862
23ccc	Wolfswinkle							1,500	E							11	
23dbb	Conoco							1,517		Dry	****	3/13/84				Ir	55-623863
24add	Wolfswinkle				***	***	***	1,475	Е		***				***		55-621537
35daa	Bean	6-28-57	323	16	323	160-318	450	1,422		117.8		11/1/88	1,304.20	D		lr	
35dda	Bean	7-30-72	815	20	605	190-600	184	1,420		72.2	***	3/3/93	1,347.80	D	RP	ir >	55-621538; chkd; cqpd
36aad	Feliz	4-5-05	420	10	420		34	1,438	:	144.6		11/1/88	1,293.40			D	55-638448
36abd1	Feliz	6-2-05	80					1,445	Ε	***		***		D		0	
36abd2	Felix	7-18-55	720	20	720	320-400	1,650	1,445		126.2		3/3/93	1,318.80	D	RP	lr,S	55-616927; registered as 36aba; chkd eqpd
	•					440-720										_	
36bad	Felix	4-3-05	250	8	250		30	1,440	E	197	R					D	55-634418
36bcd	Bean	2-22-51	550	20	522	70-510	524	1,427		122.3		11/1/88	1,304.70	D	RP	Ir,D	55-621536
36dab1	Felix	4-3-05	250	8	250		30	1,430	E	197	R				***	D	55-634397
36dab2	Feliz	4-23-05	212	7	212	***	25	1,430	E	175	R			***		D	55-639694
36dab3	Feliz	0452	150	6	150	***	8	1,430	E	125	R		***			D	55-638408
36dab4	Rameriz		200	6	200		8	1,430	E	125	R	***	•			D	55-638407
(D-04-09) 3ana	Herseth Feedlots	0842	504	20	504	220-500	1,933	1,600		361.3		1/3/69	1,238.70		RP	Ir,S,D	55-619404
3aad	Herseth Feedlots	1-30-75	838	16	838	470-825		1,597		410.5		3/3/93	1,186.50	D	RP	Ir,S,D	55-619401; registered as 3aba; chkd eqpd
3aau 3aba	Herseth Feedlots	5-10-05	504	20	504	400-504	650	1,591		372		12/20/71	1,219.00			Ir,S,D	
	Baxter	0351	433	20	433	200-431	1,200	1,575		396.9		11/15/91	1,178.10	D		Ir	55-625476
4aaa		4-24-05	580	20	580		4	1,575	E	450	R			D	***	Ir	***
4aad	Brooks	4-24-03	700	20	J80			1,571							***	Ü	***
4ada	77.11	1 20 41		20	434	200-420	943	1,564		254.1		3/3/93	1,309.90	D		11	Chkd; loose cap
4baa	Kirkland	1-20-51	434				1,500	1,560		254.1 364.5		11/8/84	1,195.50		RP	lr	55-625475; registered as 4ddd
4ddc	Baxter	2-4-77		20	750	250-750							•	D			55-625477; registered as 44444 55-625477; chkd; eqpd
4ddd1	Baxter	3-15-73	690	20	690	330-620	1,500	1,564		341.7	 n	3/3/93	1,222.30		RP	lr 1-	33-023477, caku, cupu
4ddd2	Brooks	5-30-05	750	20	750	***	1,300	1,564	£	351	R			D	***	Ir	About and a form
5aab l	Jobe	0441	403	20	403	200-390	1,776	1,555		388,2		11/15/91	1,166.80	D		U	Also reported as 5aaa
5aab2	Chapman	6-24-67	600	20	427	390-427	20	1,550		406.2		11/15/91	1,143.80	D		D	55-612176; registered as 5aaa
				16	420-600	420-600											
5aad	Jobe	5-15-05	640			***	1,500	1,551				***		D		U	
Shab	Demetria	5-3-69	635	20	629	420-620	1,100	1,546		416.6		11/15/91	1,129.40	D		ìr	55-612173
(D-04-09) 5bbb	Demetria	7-1-73	800	20	571	450-571	1,100	1,540		445.6		11/7/84	1,094.40	D		lr	55-612172
				16	546-780	580-780											
5cdb	Demetria	5-1-76	683	18	408	275-380		1,530		365	R		1,165.00	D		lr	55-612170; registered as 5cca
				14	408-680												
5daa	Demetria	11-20-51	460	20	448	200-438	2,680	1,548		366.9		3/3/93	1,181.10	D		Ir,U	55-612174; chkd; loose cap
6aaal	Clemans Bros. Cattle	5-14-40	463	20	463	200-450	1,020	1,541		173.9		1/31/47	1,367.10	D		U	,
6aaa2[No.4]	Nalbandian Farms	0171	1,000	20	600	450-600	1,148	1,541		412.4		12/19/89	1,128.60	D,L	RP	lr	55-610623
0aaa2[110.4]	i vaivanulan 1 aims	0171	1,000	16	600-1,000	600-1,000	.,	-,	_	,			-,	,			
6-1-01-01	Nalbandian Farms	5-9-46	466	20	466	190-460	1,598	1,536		172.6		8/30/46	1,363.40		RP	ir	55-610622
6aba[No.3]	ivatoangian Parms		466 860	20	460 860	190-400	1,398	1,537	E	172.0		9/50/40	1,303.40				
		3-23-71							_			12/10/00			RP	lr	55-610632
6ada[No.6]	Nalbandian Farms	0773	1,529	20	1,000	350-1,000	641	1,537		398.6		12/19/89	1,138.40	D,L	r.r	ır	JJ-0100J£

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magma.floluic.upplvolume.1023-1.XLS\1/16/96\rbb

The state of the s					C	sing		Reported	Surface			Non-P	umping Wa	iter Level				
Contact Book Conta	Well Number	Owner *		-	Diameter			Pumping	Elevation		Measured			Altitude	Logs		Use¹	Remarks <sup>1</sup>
Change   C	6addIOB 4NI	MAGMA	9-5-75	800	3	800	440-800	4	1,535				9/5/75					55-627624; UTL
Manufact Forms			4-18-57	592	20		290-585											
Manufacture   19-79   941   20   704   941   20   704   941   20   705   941   20   705   941   20   705   941   20   705   941   20   705   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20   941   20	6baa2[No.5]	Nalbandian Farms	1272	1,534	20	980	500-	1,025	1,537		411.2		12/19/89	1,125.80	D,L	RP	lr	55-610624; also reported as 6can
Manual   M															-	n.n.	1-	66 (10(2)
Total   Second	6bba[No.2]													.,				
	7aaa l	B & W 308 Ltd	0651	760				1,100	1,524		373.6		11///84	1,150.40	D		11,3,0	33-622013
A work of the part of the p								2 400	1.424		170	D		1 251 00	D		1-	
Table   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1														•	-		•	
Table   Control   Contro	7aaa3	B & W 308 Ltd	3-23-73	862				1,800	1,324		330	•••	0473	1,174.00	Ь		••	33-022014, registated as raine
Modername   Mode		n.tt.	5 2 05	210				1.000	1 517		173.8		2/20/52	1.343.20	D		U	
MACINAL   MACI																	lr	55-623858
Katz         Palmer         480         20         480         20         480          1,522         E            5,353/59         50         16          1,523															D		М	55-627623; chkd; capped
Math										Ε								55-634595
Pass     1988			5-12-05	600									***					
		USBR				613	16-613								G			
Time			12-9-77	613	1-1/4	499	491-499				332.9		4/21/78	1,232.10				
1786   1786   1796   1994   20   439   20   439   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   430   43	17acc	Conoco																
Table   Tabl	17bbc	MAGMA													-			
TriAshi]Ole-N   MAGMA   121-275   441   6   456   296-456     1,325   08   291     3,099   1,234 \ 0   0     M   55-47737; chid, capped   1,240   1,000     M   55-47737; chid, capped   1,240   1,000     M   55-47737; chid, capped   1,240     M   1,000		Conoco																
MAGMA										-								
1																		
11   Control										_								
Hand   Sanh   6-11-52   426   16-14   9   16-14   9   15-14   9   16-14   9   16-14   9   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18-14   18																	_	
Hand   McGMA   4-21-78   530   3   520									1 513		250.6		3/2/93	1.262.40	D			
Hace    Cance								***							D		U	
Hacc    Concoo																***	Е	55-504704
Nacco   Nacc				***				***				•				***	E	55-503052
The control		Conoco																
NACIMA	18acc4	Conoco									***							
Biddail   MAGNA   1-25-52   435   20   435   190-435   1,493   1,512     278     1,223/71   1,234.00   D   RP   r   55-507705   r	18bab	Сопосо																
184dd  C   Conco   G-3-05   290   8	18ccc																-	
19aak   19aa																		
19dd   LC    10d		Conoco	6-3-05		-												-	
20abs   Coneco   Co		1416141	10 10 72			267		***										
(D-04-09)20ads[502] MAGMA 4-19-78 1,060 3 1,060 1,522 E D 55-627647; registered as 20acs; chkd; UTM; obstructed; uncappe 20bb Conoco 6-3-05 1,000 8						267												
20bb Concco 6-3-05 1,000 8 D E 21bcd MAGMA 8-4-77 465 6 465 1,534.80 S 278.4 1,256.40 D E 55-627648 221 Concco 9-1-84 6 E 55-508803 222 Concco E 55-508803 222 Concco						1.060												
21bcd   MAGMA					_				•						_			
22 1 Conoco 9-1.84 6				•	-						278.4				-			
22 Conoco																		
22bad   Conoco		Conoco		•••	***	***	***						***			•••	E	
22ddc   Conoco		Conoco		***		***	***	***	•••		***						E	
23 1 Conoco 9-1-84 6		Сопосо		***	***	***		***										
23 2 Conoco		Conoco											***					
23cda   Conoco																		
23ccd2   Conoco											***							
23ccd2 Conoco																	_	
25ac Pace 4-26-05 350 6																		
25bed[No.2] Florence Gardens 0242 300 20 1,200 1,475 143.3 11/8/84 1,331.70 D RP PS,D 55-601432 25bed Florence Gardens 4-23-05 350 16 350 1,400 1,482 E 200 R 2/16/83 1,380.30 D PS 55-501433; recharge 25bed Florence Gardens 4-23-05 350 20 350 1,400 1,475 E 200 R 2/16/83 1,380.30 D PS 55-501433; recharge 25bed Florence Gardens 4-23-05 350 20 350 1,400 1,475 E 200 R 2/16/83 1,380.30 D PS 55-501432; recharge 25ded Florence Gardens 4-23-05 350 20 350 1,400 1,475 E 200 R 2/16/83 1,380.30 D PS 55-501432; recharge 25ded Brooks Farms 6-15-49 250 20 250 80-240 805 1,480 54.3 3/4/93 1,425.70 D PS 55-61432; registered as 25-da; chkd; eqpd 25ded Poston Butte Farms 12-31-40 180 8 180 1,478 139.2 11/1/88 1,338.80 1/1/88 1,338.80 1/15,5 55 806268																	_	
25bdc No.2  Florence Gardens 0242 300 20 1,200 1,475 143.3 11/8/84 1,331.70 D RP PS,D 55-601432 25bdc  Florence Gardens 4-23-05 350 16 350 1,400 1,482 E 200 R PS 55-610433; recharge 25bdc No.1  Florence Gardens 3-22-83 540 16 540 200-530 1,200 1,482 101.7 2/16/83 1,380.30 D PS 55-504767; also registered as 55-504696-25bdd 25bdd Florence Gardens 4-23-05 350 20 350 1,400 1,475 E 200 R PS 55-610432; recharge 25ddd Brooks Farms 6-15-49 250 20 25 80-240 805 1,480 54.3 3/4/93 1,425.70 D Ir 55-618028; registered as 25cda; chkd; eqpd 25dcc  Poston Butte Farms 12-31-40 180 8 180 1,478 139.2 11/1/88 1,338.80 Ir,S,D 55-806268		1 aCC			-												-	
25bdc1 Florence Gardens 4-23-05 350 16 350 1,400 1,482 E 200 R 1. 101.7 2/16/83 1,380.30 D PS 55-610433; recharge  25bdc2[No.1] Florence Gardens 3-22-83 540 16 540 200-530 1,200 1,482 101.7 2/16/83 1,380.30 D PS 55-504767; also registered as 55-504696-25bdd  25bdd Florence Gardens 4-23-05 350 20 350 1,400 1,475 E 200 R PS 55-610432; recharge  25dcd Brooks Farms 6-15-49 250 20 25 80-240 805 1,480 54.3 3/4/93 1,425.70 D Itr 55-618028; registered as 25cda; chkd; eqpd  25dccl Poston Butte Farms 12-31-40 180 8 180 1,478 139.2 11/1/88 1,338.80 Itr, S, D 55 806268		Florence Cardens			-													
25bdc2[No.1] Florence Gardens 3-22-83 540 16 540 200-530 1,200 1,482 101.7 2/16/83 1,380.30 D PS 55-504767; also registered as 55-504696-25bdd  25bdd Florence Gardens 4-23-05 350 20 350 1,400 1,475 E 200 R PS 55-610432; recharge  25cdd Brooks Farms 6-15-49 250 20 250 80-240 805 1,480 54.3 3/4/93 1,425.70 D Ir 55-618028; registered as 25cda; chkd; eqpd  25dcc1 Poston Butte Farms 12-31-40 180 8 180 1,478 139.2 11/1/88 1,338.80 Ir,S,D 55 806268				200									11/5/84	1,251.70	Ŋ			
25bdd Florence Gardens 4-23-05 350 20 350 1,400 1,475 E 200 R PS 55-610432; recharge 25cdd Brooks Farms 6-15-49 250 20 250 80-240 805 1,480 54.3 3/4/93 1,425.70 D 1r 55-618028; registered as 25cda; chkd; eqpd 25dccl Poston Butte Farms 12-31-40 180 8 180 1,478 139.2 11/1/88 1,338.80 1r,S,D 55 806268													2/16/83	1 380 30	D.			· =
25cdd Brooks Farms 6-15-49 250 20 250 80-240 805 1,480 54.3 3/4/93 1,425.70 D lr 55-618028; registered as 25cda; chkd; eqpd 25decl Poston Butte Farms 12-31-40 180 8 180 1,478 139.2 11/1/88 1,338.80 lr,S,D 55 806268													2/10/03	,				
25dcc1 Poston Butte Farms 12-31-40 180 8 180 1,478 139,2 11/1/88 1,338.80 Ir,S,D 55 806268													3/4/93					
					6					E			***					

magma.floluic.applvolume.1\2'3-1.XI.S\1/1696\rbb 2- 13

				_	sing		Reported	Surface			Non-P	umping Wa	ter Level				
Well Number	Owner *	Date Completed	Depth Drilled (ft)	Diameter (in)		Perforated Interval (ft)	Pumping Rate (gpm)	Elevation (ft, msl)		Measured Depth (ft)		Date	Altitude (ft, msl)	Logs*	Chemical Analyses <sup>k</sup>	Use '	Remarks <sup>J</sup>
		4-12-78	90									***	***				***
		4-23-79	140	5	40												55-627653
26bda2	MAGMA	6-1-05						1,491	E			***				М	55-627642; UTL
26caa	Rankin	9-1-47	258	20	258	70-248	2,500	1,473		68		3/3/93	1,405.00	D		lr	55 805235; chkd; eqpd
26ccb	SCIDD	5-18-34	212	20	212	68-198		1,477.20	S	145	R	4/21/61	1,332.20	D	***	lr	Chkd; destroyed
		4-21-61	317	16	283	198-278						***					***
26ccd	England & Coker	4-3-61	410	20	410	210-400		1,465	E					D		lr	Chkd; destroyed
26dad	Rankin	4-1-48	200	20	198	64-193		1,465	E	***				D		lr	UTL
27bbd	MAGMA	8-15-77	765	6	765			1,510	Ε	252.8		8/15/77		D		M	55-627646; UTL
27cac	MAGMA	2-3-55	305	10	305	203-295		1,480		167.3		3/2/93	1,312.70	D		D	55-627613; registered as 27cab; chkd; eqpd
	MAGMA	12-9-44	290	20	290	62-275		1,473		160	R	3/25/62	1,313.00	D		lr	55-627614; chkd; eqpd; UTM; no access
27cad	MAGMA	3-25-62	500	16	290-500	290-490		1,475	Е								
				20	410	210-400	1,251	1,470		161.4		3/2/93	1,308.60		RP	Ir,U	55-627612; England No. 3
27cbd1	MAGMA	5-14-05	410					1,472	E			31233	1,500.00				55-627656
27cbd2	MAGMA				100			1,472	E	188	R	5/29/92		D		M	55-535365
27dba	MAGMA	5-29-92	220	4	180	70.244	1.2/7						1,376.50	D	R.P	lr	55-627611; England No. 2; chkd; cqpd
27ddd	MAGMA	2-21-50	270	20	270	70-255	1,267	1,464		87.5		3/2/93					55-027011, England 110. 2, Clike, equa
		3-14-62	600	16	265-600	265-590						***		D.		E	55-508805
28	Conoco	9-1-84		6	***									-			
28add[No.84]	MAGMA		340	3				1,483		150.9		3/2/93	1,332.10			Е	Chkd; capped
28bdc[PW 2]	MAGMA	1-24-75	981	24	80		1,600	1,478		181.4		3/4/93	1,296.60	D	RP,C	I,U	55-627607; registered as 20cab; chkd;capped
				18	621	234-621											
				14	621-981	621-981											
28bdd	Conoco	8-30-85			23											E	55-512144
28caa[420-S]	Conoco	0574	1,662		1,662			1,480		201.3		12/23/71	1,278.70	D,L		U	
0-04-09)28cac[DM B]	Conoco	0874	700	5	611		17	1,477.30	S	244		10/7/74	1,233.30			T	55-806521; also reported as 28cad; UTL
-04-05)ZacacįDivi Dj	Colloco			4	611-700	611-700											
20311011/21	Camana	10-29-72	1,600	13	51			1,471		163.5		3/2/93	1,307.50	D		M	Chkd; uncapped; plugged below 1,030'
28cad1[OW 2]	Conoco	10-25-72	1,000	8	295			.,									
				5	1,030	295 1,030											
		0874	700	5	382	273 1,030	30	1,477.10	S	251		10/7/74	1.226.00	D		U	Also reported as 28dbd; UTL
28cad2[DM A]	Conoco	08/4	700	4	362			1,478		178		3/4/93	1,300.00			М	•••
28cad3[OB-6]	MAGMA				80			1,470				3/4/23	1,200.00	D		M	55-627645
28cbc1	MAGMA	8-1-77	80	5	80		***	1,470									55-627644
		4-12-78	180				***		***					***			55-627654
		4-23-79	280	***					***								55-627643
		4-9-80	430						***								
28cbc2	Сопосо	8-27-85			48									D		E	55-511901
28cbc3	Conoco	8-9-86	55	6	26	***								D		E	55-515041
28cbc4	Conoco		520							***	***			D		E	55-500731
28cbc5	Conoco		***											D		E	55-504703
28cbc6				***						***				D		E	55-502876
28ccal	McFarland	5-14-05	520					1,468	Ε			•		· D	***	lr	
28cca2[BIA9]	SCIDD	4-26-34	254	20	254	80-242	1,632	1,472.00	S	172		1/1/93	1,296.00	D	RP	ir	55-621948; chkd; eqpd
		4-28-65	500	16	495			, .							***		-
28cca3		4-20-03		20	***			1,474		184.2		11/1/88	1,289.80			U	
200083				3		==		.,		.07.2			.,207.00				
29-4-11032 21	C	12.10.45	272	_	270	75-270	740	1,474		165		3/4/93	1,309.00	D	RP	ir,U	55-627640; also reported as 28cdb; McFarland well #1; chkd; capped
28cda1[OW-3]	Conoco	12-10-45	272	20			740	1,4/4		165		214133	1,200,00		KP	ir,U	55-5270-0, also reported as 20000; Micrariand Well #1; cnkd; capped
		7-6-63	560	16	260-560	260-560	2.210			1400							66 (2)040 H.L H.L. (8) L H.L. 2(0)
28cda2[BIA10B]	SCIDD	8-15-72	2,006	24	0-76		2,240	1,467		160.2		3/2/93	1,306.80	D	RP	Ir,I	55-621949; chkd; eqpd; backfilled and plugged below 369'
				20	0-1,000	200-909											
				13	909 1,909	909 1,909											
28cda3[OW-1]	Conoco	10-25-72	1,498	10	68			1,474		161.2	***	3/4/93	1,312.80	***	RP	M	55-627657; chkd; loose cap
				5	1,035	495-1,035											
28cdb1	McFarland	4-28-05	560	20	560			1,474		170	R		1,304.00	D		Ir,U	McFarland Well #2; chkd; capped
28cdb2[PW-3]	MAGMA	11-21-74	938	24	81	***	2,095	1,474		164.3		3/2/93	1,309.70	D	RP,C	lr	55-627608; chkd, eqpd
				18	496	240-496											
				14	496-936	496-936											
28cdb3		11-21-74		3				1,474	***	***			***			U	***
28dad[BIA10]	SCIDD	4-16-34	259	20	259	107-247		1,472.30	S	213.5		2/24/75	1,254.50	D		lr	***
		0874	635	5	364		7	1,472.30	S	176.4		11/1/88	1,234.50			Ü	Also reported as 28dbd; UTL
28dba[DM-D]	Conoco			-			•									-	•
28dbc1	MAGMA	7-6-74	706	42 72	700 715			1,475	***	173.4		3/2/93	1,301.60	***		T	Shaft No. 1; north pilot mine shaft; chkd; capped

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				~	gnita		Reported	Surface			Non-P	umping Wa	ter Level				
eli Number	Owner *	Date Completed	Depth Drilled (ft)		Depth (ft)	Perforated Interval (ft)	Pumping Rate (gpm)	Elevation (ft, msl)		Measured Depth (ft)		Date	Altitude (ft, msl)	Logs <sup>6</sup>	Chemical Analyses <sup>k</sup>	Use¹	
28dbd1[DM-C]	Conoco	0874	610	5	358		20	1,473.10	S	162.5		12/20/85	1,310.60			U	55-806520; also reported as 28dae; chkd; UTM; obstructed
	Conoco	12-2-74	949	24	80		450	1,467		158.9		3/2/93	1,308.10	D	RP,C	U	chkd; capped
200000[1 ]				18	540	243-539											
				14	540-939	540-938											
28dbd3[365 S]	MAGMA		1,299	3	•••			1,478		168.6		3/2/93	1,309.40		***		chkd; loose cap
28ddb[DM E]	Conoco	0874	700	5	392		60	1,465		213	R	10/7/74	1,252.00			T Ir	UTL
29cbc	SCIDD	5-15-05	334	20	334		1,125	1,460	Ε	167	R		. 204 20	D		ır İr	55 C21050; annistant on 20 share ability aged
29ccb[BIA11]	SCIDD	5-9-34	290	20	290	64-277	805	1,457.80	S	151.5		3/2/93	1,306.30	D		11	55-621950; registered as 29cbc; chkd; eqpd
		2-9-62	334	16	334	160-330	i.	1.476	 E							1	55-609666
29dab	Riggins Pinal	8-25-71	1,625	7	1,600	***	35	1,475 1,465	E							i	55-609667
29dac	Riggins Pinal	7-31-71	1,098	11	1,098		35									lr	55-627610; registered as 29dca; chkd; cqpd
29dcb[PW 20]	MAGMA	1-10-75	1,180	24	81		1,881	1,460		144.6		3/2/93	1,315.40	D	RP,C	11	33-627610, registered as 27dea, criku, edpu
				18	1,176	229 1,176				212.0		11/1/00	1 260 10			11	UTL
(D-04-09)30add				3			***	1,482		212.9		11/1/88	1,269.10			E	
30bcc	MAGMA			3				1,468		156.5		3/3/93	1,311.50			lr.D	chkd; uncapped 55-618023; registered as 30cc
30cca	Yeo	5-20-05	415	12	415		***	1,461								ir,D A	55-618023; registered as 30cc 55-627655
30cdc	MAGMA							1,448	Е	127.0		11/1/00	1 795 20			A U	33-02/033
30dad				3				1,463		177.8 184.7		11/1/88 11/15/83	1,285.20 1,260.30		***	lr	
30dcd								1,445							RP		55-627617; also reported as 30daa; chkd; UTM
30dda[No.6]	Conoco	5-11-65	355	20	346	165-345	809	1,458		130	R	5/1/65	1,328.00	D D		lr Ir	55-62/61/; also reported as 30daa; cnkd; O1M
3 laba	McFarland	11-24-48	250	20	224	100-216		1,445	E	220	R		1,229.00	D D		D	55-600580
3 i baa i	Chandler	5-5-05	300	4	300	. 250 520	25	1,449		156.1	K	3/9/93	1,229.00	D.	RP	ir,D	55-600577; chkd; eqpd
31baa2	Riggins Pinal	5-20-68	620	16	620	350-620	668	1,448		136.1		319193	1,291.90			11,15	55-000577, cinku, eqps
		12-20-74	850	12	620-820 320	620-820 100-300	1,411	1,444		160.5		11/1/88	1,283.50	D	RP	lr	55-600579; chkd; UTM; no access
31bba	Riggins Pinal	7-14-51	382	20	320 300-400	300-400	1,411	1,444		100.5			1,285.50				
		2-14-80	763	16 14	400-703	400-703											
				10	703-763	703-763											
		12-9-75	360	3	360	200-360		1,429		73		3/9/93	1,356.00	D		М	55-627630; chkd; capped
31ccd[OB-1W]	Conoco	3-5-61	448	20	446	140-440	1,634	1,434		139		11/1/88	1,295.00	D	RP	Ir	55-600578; chkd; eqpd; UTM; no access
31dca	Riggins Pinal	1-18-72	890	16	429-889	450-865	1,051	.,,,,,					***		***		
32ada	MAGMA	5-1-05		20	265	100-265	1,400	1,453		155.1		11/2/84	1,297.90			U	McFarland Well No. 3; replaced 1975; UTL; destroyed; 55-62760-
32844	MINOMA	5-14-05	473	16	265-473	265-473		,				•••					***
32baa1	Espinoza	0552	346	20	346	70-340		1,449	E	***				D	***	Ir	
32baa2	Riggins Pinal	5-5-05	410	20	410		1,082	1,448		152.4		12/20/85	1,295.60		RP	ir	55-609672
32bda	Riggins Pinal	1-26-47	193	20	193	50-193	1,270	1,443		83.5		3/9/93	1,359.50	D	RP	Ir	55-609671; chkd; eqpd
	<b>30</b> · · · ·	11-6-51	397	16	190-368	200-352				***							***
32caa	Chandler & Chandler	4-7-05	100	20	100	***	2,531	1,438	E	36	R			D		0	•••
32cbd1	Riggins Pinal	4-30-05	250	20	250	***	200	1,435		28		3/9/93	1,408.00			D,U	55-609668; registered as 32cac; chkd; eqpd
32cbd2	Riggins Pinal	12-18-53	450	20	442	100-430	1,107	1,435		29.4		3/9/93	1,405.60	D	RP	lr	55-609670; registered as 32bca; also reported as 32caa; chkd; eqpd
32dda	Riggins Pinal	2-9-47	203	20	203	50-200	1,428	1,438		142		11/2/84	1,296.00	Đ	RP	Ir	55-609669
		12-13-57	583	16		197-512				***							
33aad[PW-4]	MAGMA	12-15-74	997	24	80		741	1,456		124,8		3/3/93	1,331.20	D	RP,C	Ir,U	55-627609; Terry Bros. Farm Well #3; chkd; eqpd; no motor
				18	598	252-598											
				14	598-997	598-997			_					_			
34add	Robertson	5-2-05	550			***		1,458	٠E					D		lr 	AL
34daa	Robertson	4-26-49	184	20	184	80-175	•••	1,457		54	R	4/26/49	1,403.00	D	***	U	Also reported as 34add
34dda[OB-1E]	MAGMA	7-30-75	392	3	392	264-392	11	1,460		144.1		11/2/88	1,315.90	D		M	55-627619; UTL
35aaa	Giles	7-20-51	270	18	224	1-224		1,468	***	47.7		3/8/93	1,420.30	D		Ir,S	55-625921; registered as 35aab; chkd; eqpd
4-	p. 1.		200	14	224-254	224-254	20			140	В	•••	***		***	D	55-631674
35c	Rankin	5-5-48	208	8	208		20			160	R				***	S,D	55-643744
35d	Taylor	2-20-05	25	8	25			1,485		176	R	1175	1,309.00			5,0	53-643/44
35dda	Smith	10.21.01						1,485	E	176	к	11/3	1,309.00	D	,	U	55-533207
35ddc	Southwest Gas	10-31-91 7-5-39	230 575	20	575		950	1,483	E	135.5		3/8/93	1,352.50		,	PS	55-619535; chkd; eqpd
36cac1[No.3]	Florence Water	7-3-39 4-30-05	375	20 16	375	335-370	950 850	1,488		133.5		11/3/88	1,352.50	D		PS PS	55-619533; chkd; eqpd
36cac2[No.4]	Florence Water		375	6	373 150	333-370	850 35	1,487		173,5	R	11/3/88	1,2.20			D,S,Ir	55-606117
36d	Butte View Palmer	5-16-05 12-3-59	335	20	30		2,600	1,515	E	110	R					lr lr	55-617189
(D-04-10)17cad1		12-3-39	400	6	400		30	1,515	E	120	R					D D	55-638410
17cad2 17cbd	Palmer Palmer	5-12-05	400		+00		JU	1,525	E	140.2		3/8/93	1,384.80			lr	chkd; eqpd
	FAUUCT	3-12-03	400		20	***		1,565		140.2	***	310173	1,504.00			11	enau, eqpa

2- 15

				_			Danastad	Surface			Non.	umping Wa	ter Level				
ell Number	Owner *	Date Completed	Depth Drilled (ft)		nsing Depth (ft)	Perforated Interval (ft)	Reported Pumping Rate (gpm)	Elevation (ft, msl)*		Measured Depth (ft)		Date	Altitude (ft, msl)	Logs	Chemical Analyses <sup>h</sup>	Use <sup>1</sup>	Remarks <sup>J</sup>
18dcd2[PZ-1]	USBR	4-13-79	1,560	1-1/4	1,258	1,250-1,258		1,565		225.7		1/24/84	1,339.30		***	Pz	
18dcd3[PZ-2]	USBR	4-13-79	1,560	1-1/4	588	580-588		1,565		224.5		1/24/84	1,340.50			Pz	
19dad[OB-3E]	MAGMA	7-17-75	355	3	355	195-355	9	1,491		122.9		10/31/88	1,368.10	D		M	55-627621; UTL
	MAGMA	7-11-75	365	3	365	205-365	7	1,512		131.1		10/31/88	1,380.90	D		M	55-627622; UTL
29add1	Clark				***	***		1,529								U	
29add2	L and M Farms	5-17-05	230	8	230		30	1,529		190	R		1,339.00			D	55-616519
29baa[BIA3B]	SCIDD	3-15-68	795	20	492		2,500	1,504		187		0193	1,317.00	D		lr	Also reported as 29cdd; chkd; eqpd
,,				16	495-730												
				14	725-795												
29bdd	ADC	7-23-51	410	20			1,441	1,509		109.8 -		3/8/93	1,399.20	D	RP	łr,l	55-610141; also reported as 29ade; chkd; eqpd
29cda	Cansino	6-2-05	300	8	300	***		1,520	E	180	R		***	D		U	55 085529
29cdd	Padilla	5-4-05	265	8	265		34	1,525	E	230	R					D	55-638406
29dad[BIA2]	SCIDD	1-23-62	622	20	532	170-524	1,760	1,539.10	S	190		0193	1,350.00	D		ir	55-621940; also reported as 29daa; chkd;eqpd
29Gau[DIA2]	SCIDD	. 25 02		16	527-622	535-618											
29ddc1	L and M Farms	10-10-46	400	20		130-400	1,500	1,544		125	R	1/21/52	1,419.00	D		D,Ir	55-616515
		10-10-40	330				1,900	1,544		192		10/31/88	1,352,00	D		lr	
29ddc2	Clark	0946	300	20	300	100-300	1,800	1,490		157.2		12/16/91	1,332.80			lr	55-605530
30bdd	Poston Butte Farms	7-22-75	370	3	370	210-370	1,000	1,481		164	R	7/22/75	1,317.00	D		М	55-627620; UTL
30сьь[ОВ-2Е]	MAGMA	7-22-73 4-29-05	. 368	20	370	210-370	2,200			90	R	***		D		lr	
31 1	Zellweger	4-29-03 8-27-79	300	8	300	***	30		***	180	R					D	55-633750
31 2	Potter	8-27-79	521	10	470		35	1,510	Е	220	R					D	55-612520
31acc	Lewis		350	20	350	90-334	2,244	1,495.60	s	116		3/3/93	1,382.00	D	RP	ļr	55-621943; registered as 31abb; chkd; eqpd
31baa1[BIA5]	SCIDD	4-17-34			491	20-334		1,495.00				3/3/73	1,502,00	D		D	***
31baa2	Lewis	7-18-73	521	10			1,367	1,498						D		lr	WANT.
31baa3[BIA5B]	SCIDD	4-15-77	700	20	278	320-640	1,367	1,498		***						••	
				16	278-700			1,535	E							D	55-639999
31ccb	Jamka					200 420			_	192.9		3/8/93	1,341.10	D		lr	55-612516; chkd; eqpd
31cdd	Lewis	2-9-77	934	20	845	280-420	2,000	1,534		192.9		כניוסוכ	1,341.10	D			55-012510, cina, capa
				18	830-930					100.0		1051/88	1,341.10	D	RP	İr	chkd; eqpd; UTM
31daa[BIA4]	SCIDD	4-4-34	220	20	220	100-207	1,160	1,534.30	S	198.9		10/31/88	1,341.10	-	K.F	11	enku, eqpu, o rivi
		0747	370	10	370	213-262				227.6		0/12/90			RP	lr,I	55-610135; Dairy Farm Well
31dad	ADC	•••	400	20	***		1,125	1,541		227.5		9/13/89	1,313.50		KP	ır,ı İr	55-618027
32aad	Brooks Farms					1,500						***				Ir D	55-639919
32ь	Padilla		300	8	300		35	1,560	E	220	R					-	
32bad1[BIA3]	SCIDD	4-4-34	212	20	212	98-198	1,800	1,535.80	S					D	RP	İr	55-621941; also reported as 29cdd
		7-16-47	392	16	392	207-384						***					•••
32bad2	Bowling	5-4-05	354	20			2,000	1,535	E	125	R			D	•••	lr	
32bcc	Lewis	9-1-60	810	20	810	185-798		1,535		165	R		1,370.00	D		lr	55-612515
32cbb[BIA4B]	SCIDD	6-14-79	931	20	495	255-495	1,811	1,535		205		0193	1,330.00	D		lr	55-621942
			16	928	495-928											_	
(D 05 08) laacl			60	16	54			1,428	E						**-	0	
laac2				16			***	1,428		69.1		11/24/53	1,358.90			U	Destroyed
labo	LDS	5-9-05	400	6			***	1,425						D			55-627913; registered as Iba
1bcb[BIA13]	SCIDD	4-17-05	230	20	230		800	1,415	E	68		0193				lr	55-621952; also reported as 1bbb
Icda	Krappenberger	0751	360	20	230	55-194		1,419		88.3		11/2/88	1,330.70	D	***	U	
Idca	LDS	5-18-61	525	20	484	200-472		1,422		117.9		11/2/88	1,304.10	D		lr	55-608010
i dda	LDS	5-9-46	508	20	308	36-258	1,200	1,420		89.8		2/1/63	1,330.20	D		lr	55-608009; registered as 1d
(D-05-08) 2aaa	SCIDD	0534	230	20		30-56	2,377	1,419		50,4		3/3/93	1,368.60	D	RP	lr	chkd; eqpd
					91-108 187-217												
2acd		4-29-05	295	20		90-		1,408	E	96	R					lr	
2cda	Kenworthy	5-3-05	286		***		1,600	1,405	E					D		lr	***
2daa1	Swanson	4-7-05	204	20	204			1,417		100.1		11/2/88	1,316.90		RP	lr	55-616763; registered by section number only
2daa1 2daa2	Swanson	6-2-65	480	20	480	•••	1,260	1,412		95.6		3/15/84	1,316.40			lr	55-616764; registered by section number only
2dab[OB-2W]	MAGMA	5-23-75	223	3	223	140-223	3	1,410		176	R	5/15/64	1,234.00	D		M	55-627631; UTL
libedi	ASLD	0630	150	48	50	25-50	1,000	1,410		75	R		1,329.00	D		lr	
110001	NOLD	0030	170				1,000	1,404		15	Λ.		1,525,00	J		"	
				20	50-150	50-150		1 405		(A. 7			1 227 20				
11bcd2				5				1,405		68.7		10/29/84	1,336.30			U	***
11bcd3			80	48	***	***		1,408	E	17	R		***	D		ir	er (10040 11 ) . I 1004
llccc		12-14-63	685	20	685	140-645	985	1,421		164.1		8/30/89	1,256.90	D	RP	1r	55-612747; chkd; eqpd; UTM; no access
l l cdd	Faul	7-14-52	650	20	650	85-635	551	1,428		60.9		3/3/93	1,367.10	D	RP	lr	55-612748; chkd; eqpd
l l daa		***	300	18			1,250	1,420	E				***	Ð		lr	

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				Ca	sing		Reported	Surface			Non-P	umping Wa	ter Level				
eli Number	Owner *	Date Completed	Depth Drilled (ft)		Depth (ft)	Perforated Interval (ft)	Pumping Rate (gpm) <sup>c</sup>	Elevation (ft, msl)		Measured Depth (ft)		Date	Altitude (ft, msl)	Logs	Chemical Analyses <sup>b</sup>	Usc	Remarks <sup>J</sup>
11dcd	Faul	1-8-58	715	20	698	125-686	1,339	1,432		116.5		12/19/89	1,315.50	D	RP	lr	55-612749
11ddc1		4-18-05	200	16	45	***		1,432		***					RP	lr	
	AFS Enterprises			•••			50	1,431							RP	lr	55-610523
12	Blue Circle Atlantic	7-3-01		12	540		180			120	R					ī	55-622483
12aad	Blue Circle Atlantic	2-25-48	220	20	164	38-152	808	1,418		13		3/2/93	1,405.00	D	· RP	lr	55-606372; registered as 12ada; chkd; eqpd
12aba l	Blue Circle Atlantic	5-18-05	430	20	430		1,400	1,412	Ε	250	R		***	D		lr	55-606374
12aba2	Gila River Tribe						778	1,412	'	102.9		2/16/83	1,309.10		RP	ir	***
12abd	Gila Farm	2-24-65	430	20	430	100-424		1,412	***					D		U	Destroyed
· 12ada1	Chill t min	4-12-40	610	20	***	70-445	1,000	1,416		70	R		1,346.00	D			***
12ada2	Blue Circle Atlantic	5-1-05	500	16	500		800	1,416		250	R		1,166.00	D		lr	55-606372
12ada2	Anderson	5-1-05	220	20		164-	1,000	1,416		38	R			D		lr	
12ccb1	Bundrick	1-28-82	465	8	465	210-228	13	1,432		122.2		11/2/88	1,309.80	D		D	55-501839
120001	Dullulick	1-20-02	100	-	260-280			•									
					399-465												
12- 12	D duint.	1-30-82	465	8	465		100	1,432				***		D			55-630364
12ccb2	Bundrick	1-30-82	403	•	405			1,432		160	R	***	1,272.00		RP	D	***
12ccb3	Tabert	5-8-05	300	8	250		35	1,435	E	165	R					D	55-630362
12ccd1	Meijer		390	6	360		35	1,435	E	165	R		***		•••	D	55-630365
12ccd2	Meijer	5-26-05		6	365			1,435	E	235	R			D		D	
12ccd3	Bundrick	5-27-05	365	8	460	360-460		1,435	E	105	R			D		D	55-519619
12ccd4	Squaw Mtn. MHP	12-10-87	460	-	380	150-375		1,435		120	R	3/6/66	1,315.00	D		lr.	55-610674
12cda1	Hohokam Country Club	3-6-66	500	16				1,433		120	κ.	3/0/00	1,313.00	0			33-010071
				14	380-500	380-500		1.427		119.7		11/2/88	1.317.30	D		D	55-635855
12cda2	Moody	0772	360	12	360	280-355		1,437					1,298.60	D		D	
12cdb	Lofgreen	7-30-71	400	12	330	200-326		1,434		135.4		11/2/88				D	***
12cdc1						***		1,438		132.5		10/31/84	1,305.50			D	***
12cdc2			***			***		1,438		127.5		11/2/88	1,310.50			D	
12cdd1	Moody		350	8	350			1,445	E	170	R					-	55 800869
12cdd2	Menkin	9-10-92	380	8	380	320-360		1,445	Е	110	R	9/10/92		Đ	***	D	55-534883
12d1	Hohokam Country Club	8-1-51		8	268		20		***	220	R	***				D	55-610675
12d2	Pratt	5-17-05	400	12	400		35			230	R					D	55-611468
12d3	Pratt	5-17-05	400	12	340		40			230	R					D	55-605784
(D-05-08) 12dad1	Blue Circle Atlantic	8-3-51	420	20	418	100-406	600	1,435		125.9		11/2/88	1,309.10	D		lr	55-606373
12dad2	Pinal Mammoth Gypsum	***						1,440	***	126.7		11/2/88	1,313.30			I	
12dcb1	Hohokam Country Club	0452	500	12	500		500	1,440	Е	236	R		***	D		lr	55-610674
12dcb2	Hohokam Country Club	5-19-05	500	16	500			1,440	E	120	R			D		Ir	•••
12dcd	Hohokam Country Club	1-9-01						1,451		128.4	***	10/31/84	1,322.60			D	55-610675
12ddd1	Elks Lodge	3-16-75	385	12	385	145-230	35	1,455		95.2		3/3/93	1,359.80	D		D	55 801684; chkd; eqpd
					260-280												
12ddd2	Maddock	5-14-88	452	6	452	352-452	26	1,455	E	220	R	5/14/88	***	D		D	55-520852
13	Payne	4-14-05	180	16				1,200		72	R		***	D	***	Ir	•••
13aab1	Attaway Ranches	0247	323	20	323	110-323	1,800	1,459		140.1		10/31/84	1,318.90	Ð		U	Also reported as 13aaa
13aab2	Mutual Farms, Inc.	5-31-05	520	18	520	***	1,100	L,459		144.8		10/31/84	1,314.20		RP	lr,D	55-622015; registered as 13aaa
13bbd	•		292	16				1,445					***		RP	U	Destroyed
13bca	Riggs	7-5-51	418	20	416	107-400	600	1,450		122.6		10/31/88	1,327.40	D		İr	55-601791
13cad[B1A20]	SCIDD	0534	204	20	204 153-184	70-120	1,210	1,453		89		6/1/47	1,364.00	D		Ir, A	Destroyed
		0647	340									***					•••
13cdb[BIA20B]	SCIDD	7-23-75	630	20	396	110-383	1,200	1,455		101.8		3/2/93	1,353.20	D		İr	55-621929; chkd; eqpd
		. 22 .2		16	385-616	400-610	-,	-,					.,	-			
		8-27-80	990	12	990												***
13daa	U.S. Indian Irr Serv	4-3-05	312	24	90		***	1,460		80	R		1,380.00	D		U	Destroyed
13ddd	Riggs	4-5-05	418	6	418		20	1,462	E	218	R		1,380.00			D	55-601793
13ddd 14abb	Faul	4-24-05	200	8	200		20	1,402	E	170	R						55-612750
14abb 14cadi				20			2,107	1,430		52			1,393.00	D		U	
	U.S. Indian Irr Serv	4-17-05	216		216 704	140-696					R	0534			 DD	-	Destroyed 55 621020
14cad2	SCIDD	1056	730	20			1,700	1,445		136.2		10/31/88	1,308.80	D	RP	Ir	55-621930
14cba[BIA21B]	SCIDD	1-23-79	913	20	550	155-183		1,439		103.1		3/2/93	1,335.90	D	***	ir,U	chkd; eqpd
					210-546						•						
				16	550-800	555-796											
14cbc	Anderson		340	10	340		35	1,438	E	240	R		***	***		D	55-606375 55-631292
14d	Skousen	4-26-05			***		***	***								D	

magma.floluic.applvolume.1\2'3-1.XLS\1/16/96\trb 2- 17

				C	sing		Reported	Surface			Non-P	umping Wa	ter Level				
ell Number	Owner *	Date Completed	Depth Drilled (ft)		Depth (ft)	Perforated Interval (ft)	Pumping Rate (gpm)	Elevation (ft, msl)		Measured Depth (ft)		Date	Altitude (ft, msl)	Logs	Chemical Analyses <sup>h</sup>	Use	Remarks <sup>1</sup>
23add	Benedict Feeding	4-12-84	415	5	415	340-415	15	1,445	Е	190	R	4/12/84		D	***	D	55-507613
23bdd			1,050		***			1,567						L		U	
23cbb1	SCIDD	0534	228	20	228	67-70	1,749	1,437		47	R	0534	1,390.00	D	RP		•••
					92-132												
					204-214					120.2		1/11/74	1,297.70	D			***
23cbb2	SCIDD	9-7-54	800	20	800	130-785		1,437		139.3 111.8		3/2/93	1,325.20	L	RP	lr	55-621931; chkd; eqpd
23cbb3[BIA23B]	SCIDD	10-30-72	1,060	20 16		220-530 535-1,055		1,437	•••	111.0		3/2//3	1,525.20	-			
22111	110 1 F 1 C	4-30-05			···· ,		1,256	1,448		79		0146	1,369.00			U	Destroyed
23ddd 24b	U.S. Indian Irr Serv Myers	4-30-03	230													D	55-800287
24bcc	Lillie	5-3-05	250	8	250		25	1,448	E	207	R					Ð	55-634184
24cda1	U.S. Indian Irr Serv	4-17-05	216	20	87		1,525	1,462		64	R	0534	1,398.00	D	RP	U	Destroyed
24cda2[BIA19]	SCIDD	11-16-51	600	20	600	145-590	1,800	1,462		138.8		3/2/93	1,323.20	D	RP	Ir	55-621928; registered as 24cad; chkd; eqpd
(D 05 09) I	Trejo Oil Co.						•••		*					D		Е	55-528940
laad	ADC							1,520	Е				•••	D		М	55-531739
lacd	ADC	3-27-89	1,100	16	1,100	580 1,100		1,530	Ε	196	R	3/27/89		D		, D	55-523133
laddl	ADC	2-15-54	450	20	432		2,500	1,535	Ε	240	R		1 202 00			lr,PS,I	55-610137 55-610139
ladd2	ADC	12-21-62	453	20	451	200-440	2,000	1,535		232		11/10/75	1,303.00	D		lr,PS,I E	55-521351
lbbb	Trejo Oil Co.				620	140 510	2.120	1,494		161		3/8/93	1,333.00	D		ir,U	55-627616; chkd; poorly capped
(D 05 09) 2abd	MAGMA	0558	520	20	520	140-510	2,120	1,494		167.7		3/8/93	1,335.30	D		PS	55-619534; chkd; cqpd
2ada[No.5]	Florence Water	9-30-53	575	20	562	350-547	1,300	1,480		80.2		2/14/51	1,399.80			lr.	Destroyed
2bdc	USDA Florence Unified	4-29-05 4-16-05	260	10	254			1,500	E	228	R			D		1r	55-801142
2ca <b>a</b> 2ddd	Alston Campbell	10-11-01			234			1,520	E				***			Ir	•••
3adc	USDA	4-29-05			***		3,000	1,470	E					D	***	lr	
3ccd	Neely & French	10-27-00			301			1,485						D			55-633910
3dab	HRS Farms	5-1-05	450	20	450	***	3,000	1,475		182.5		12/11/91	1,292.50		RP	Ir	55-603850
3dac							'	1,490	Ε	98	R		***			lr	***
4bdd	Layton	5-31-57	600	20	598	290-590	1,441	1,446		110.1		3/2/93	1,335.90	D	RP	lr	55-624355; registered as 4cdd; also reported as 4caa; chkd; eqpd
4cab					***			1,445		159.9		4/14/70	1,285.10			lr	
4cda	Layton	0148	341	20	322	100-310	2,180	1,453		148.8		11/2/88	1,304.20	D	RP	lr 	55-624355
5edc1		0241	355	20	355	40-260		1,434		37.4		3/2/93 11/14/83	1,396.60 1,285.20	D D	RP RP	U Ir	chkd; capped 55-624358; registered as 5ccd; chkd; UTM; no access
5cdc2	Layton	1-12-66	505	20 20	505	140-505	1,978	1,433 1,435	 E	147.8		11/14/03	1,265.20	D		lr	53-024550, registered as youd, bland, or the, no docess
5cdd		4-24-05 0846	320 225	20	208	50-195	2,225	1,437		130.8		11/1/84	1,306,20	D	R.P	lr	55-624357
5dbd	Layton	4-23-05	604	20	604	30-175		1,434	Е	118	R			D	•••		•••
6aaa 1 6aaa 2	England Gibson	4-18-80	405	8	400		20	1,434	-	140	R	***	1,294.00			D,S	55-600753; registered as 6acb
6aac	Gloson	0740	504	20		120-	1,600	1,425		148.4		2/15/83	1,276.60	D		Ir	Live
6bad	Lamoreaux	5-3-05	450	20	450		1,131	1,428		101.2		11/1/88	1,326.80		RP	1r	55-604492
7cacl	Myers	4-15-05	100	8			25	1,435		Dry		10/31/84	***	D		U	
7cac2	England	1054	314	12	314	50-314	700	1,435		131.7		11/2/88	1,303.30	D		Ir,D	55 801137
7cad1	Young	10-3-63	336	12	336	210-235	40	1,450		137.4		11/2/88	1,312.60	D	***	D	55-620629
					300-310				_							_	** (3042)
7cad2	Riggins	6-5-78	230	6	230	170.706	220	1,450	E	100	R	100606	1 294 00			D D	55-638436 55-610534
7dbb	Hearty	8-28-57	314	16	313	170-306	220	1,438	 E	153.1	p	10/25/75	1,284.90	D D		מ	55-516955
7dbd	Wilkerson	4-27-87 5-28-75	352 400	6 3	352 400	252-352 240-400	4	1,450 1,465	E	140 115.6	R	4/27/87 3/8/93	1,349,40	D		M	55-627627;chkd; capped
7ddb[OB 2S] 8aaa	MAGMA	3-28-75	400	12	400	270-700		1,440		113.6		210123	1,349.40		RP	lr	and any or the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
saaa Saadl	Clemans Cattle Co.	3-28-05	200	12	200		1,470	1,442		Dry		11/1/84			RP	Ü	***
8aad2	Layton	10-25-51	621	20	220	70-200	1,540	1,442		135.5		11/2/88	1,306.50	D	RP	lr	55-624360
Judit				16	210-420	221-410	** **	,							-		
8acc	Clemans Cattle Co.	5-27-05	403	5	403			1,470	E	234	R			D		D	
8cdd		3-26-52	500	16	500	177-488	***	1,477		168.1		11/1/84	1,308.90	Ð		U	Also reported as 8dbb
8dbb	Deputy MD	0574	410	8	400		11	1,473		142.7		3/3/93	1,330.30			D	55-635712; chkd; eqpd
8dbd1	Yco	6-3-85	303	8	303	260-303	45	1,485	E	190	R	6/3/85		D		D,Ir	55-508251
8dbd2	Gammons	4-9-86	700	6	700	600-700	35	1,485	Æ	160	R	4/9/86	***	D		D	55-513663
8ddb	Boswell	5-6-05	500	16	500	***		1,485	E	108	R			D		i	
8ddd		0852	254	12		196-245	200	1,485		105	R		1,380.00	D		i	***
9aba l	Neely	4-29-05	460	20	460		250	1,462	E	128	R			D		lr	er conner
9aba2	HRS Farms	3-11-57	500	20 20	496 707	120-480 320-690	2,000 2.940	1,462 1,455		159,4		11/2/88	1,302.60	D	RP	lr	55-603851; registered as 9aaa; also reported as 9abb

				C	sing		Reported	Surface			Nun-P	umping Wai	er Level				
ell Number	Owner *	Onte Completed	Depth Drilled (ft)		Depth (ft)	Perforated Interval (ft)	Pumping Rate (gpm)	Elevation (ft, msl)*		Measured Depth (ft)		Date	Altitude (ft, mal)	Logi	Chemical Analyses <sup>b</sup>	Usc	Remarks 1
9bad	Leiden		194	20	194			1,458								D,S	55-624361, registered as 9ban
9cbb[OB 15]	Layton MAGMA	6-2-75	380	3	380	220-380	5	1,460		119.4		3/8/93	1,340.60	D		м	55-627626; chkd, uncapped
9dad	Urton	0447	406	20	406	110-396	1,700	1,493		1874		11/3/88	1 305 60	D		Ir	55-605133
10acd	Lewis McFarland	12-31-48	550	20	550	130-538		1,510		120	R	12/31/48	1,390 00	D	-4-	lr ~	_
10566	Necly	2-19-82	700	5	700	640-700	35	1,485		245	R	2/19/82	1,240.00	D		D	55-501969
(D-05-09) 10cbc1	,		85	48				1,494								U	Destroyed
10ebc2	Lewis		320	18			453	1,494		187 1		11/3/88	1,306.90			lr,D	55-608734
10ebc3	Hiscox	6-3-43	362	10	362	240-362	35	1,494		167.1		3/3/93	1,326.90	D		D,Ir D	55-505335, replaced 55-608734-10cbc2, chkd, eqpd 55-527325
10ccd	Gentry	5-7-90	310	6	280	220-280		1,498	E	160	R	5/7/90		D	***	מ	55-612199
Hbdb	McFertand	5-31-05	600	10	600		35	1,518	E	260	R	207/17		D		le le	55-612196
115441	McFarland	4-30-05	412	20		***	2,000	1,540		126	R	2/27/47	1,414.00	D		lr	55-612197
116dd2	McFarland	5-1-05	550	20	550		2,000	1,540		120	R	12/22/48	1,420.00 1,307.90			lr	55-612195
Head	McFarland	5-1-77	973	20			2,000	1,538		230 I		11/3/88	1,307 90	D		ir Ir	55-612198
1 leeb!	McFarland	7-14-64	940	20	940	230-940	2,600	1,525	E	260	R.	4/29/83		D		D	55-504806
Hccb2	McFarland	4-29-83	720	16	720	360-720	35	1,525			н.	1/1/93	1,314 00	Ð	R.P	lr	55-621922, registered as 11cdb
Hcdc[BIA80]	SCIDD	3-30-61	845	20	545	210-535	2,000	1,540		226		1/1/72	1,024,00		***		
				16	530-831	540-825	14	1,558		255	R	***	1,303.00	D		D	55 087356; registered as 12ace
12acd	Apel	6-3-05	500	6	500		12	1,535.60	S	167.7		1/16/57	1.362.30	D		lr.	
12566 BIA110	SCIDD	0447	316	20		150-304		1,535.60		215.2		3/3/93	1,313.80	Ď		Ĭr	55-621913, chkd, egpd
1266c[BIA110A]	SCIDD	1-17-80	695	20	448 448-695		2,000	1,327		115.2			-,- 10.00	_			· · <del>-</del>
			***	16		120-468	2,000	1,538		244.9		11/9/84	1,293.10	D.L		Ir	55-621912
12bcb[BIA110B]	SCIDD	3-17-67	535 805	20 20	461	200-780	1,800	1,537 30	S	217		3/3/93	1,321.00	D		ŀτ	55-621919; also reported as 14cbb, chkd, eqpd
14bcc[BIA89]	SCIDD	12-56	1,598	6	15	200-760	1,400	1,545						D,L,G		Pz	-
[4cac1[SG 1]	USBR	2-24-78		1-1/4	1,363	1,354 1,363	1,545		_	271 8		3/1/79	1,273.20			Pz	
4cac2[PZ 1]	USBR	2-24-7 <b>8</b> 2-24-7 <b>8</b>	1,598 1,598	1-1/4	1,101	1,092 1,101	1,545			271 2		3/1/79	1,273 80			Pz	
14cac3[PZ 2]	USBR	2-24-78 2-24-78	1,598	1-1/4	702	698- 702		1.545		276.4		3/1/79	1,268.60			Pz	
14cac4[PZ 3]	USBR	1256	805	20		200-780	2,250	1,530		241 2		12/16/91	1,288 80	•	R.P	- 1	55 800875
14cbb	ASLD U.S. Indian Irr Serv	4-29-05	***				1,571	1,530	E	79	R	_		D		lr	
14dad 15cac	Lewis	5-11-05	400	8	400	•••	35	1,520	E	250	R			•••		D	55-612519
15dbc[BIA79]	SCIDD	8-24-46	424	20	***	120-400	2,000	1,526.70	S	203 3		3/3/93	1,320 70	Đ	RP	ĺr	55-621923; chkd, eqpd
		2-29-36	480	8	480		30	_	***	285	R			_	***	S.D.I	55-633674
16c	Kempton Dairy Inc. Urton	5-7-05	300	1	300		15	1,486		265	R.		1,221 00	•~•	***	D	55-605135
17aan 17cdc1[No.1]	Arizona Water Co.	4-13-05	345	10				1,475				••-				D,PS,	1 55-6166B6
17cdc2[No.2]	Arizona Water Co.			_			222			1,475			***		RP	PS	pan
17das	Cook	4-12-05	260	6	260		11	1,486		153 2		3/3/93	1,332 80			D,S	55-638612; chkd, eqpd
[ Babb	Adams	5-13-90	335	ß	322		12	1,440	E	225	R	-		D		D	55-527020
18haa	Tanner Co.	0852	254	12	254	196-245	300	1,450		223	R		1,227 00	D		I	55-605123
18bab	Tanner Co.	5-5-72	500	16	450		***	1,454		147.8		11/2/88	1,306.20		-	]	55-605124; registered as 18baa
185bc1	Anderson Clayton Co				***		***	1,465	Е						•••	D,S	55-626794
18bbc2	•	***		-		_		1,465		162.2		10/31/88	1,302.80		_	J Ir	55-601790
18bda	Riggs	8-18-75	800	20	B00	500-800	1,860	1,457		222.3		10/20/75	1,234.70	D D	R.P	ir Ir	55-601792
186441	Riggs	3-30-40	396	20	396	80-382	922	1,464		152.1		12/16/91	1,311 90 1,283.90	D	K.P	ur Ir	53-601792
Ebdd2	Riggs	1-3-71	950	20	620	490-620	1,800	1,464		180.1	•	12/16/91	1,283,90	D		u	22-001707
				16	620-950	620-950			_	.,	R					D,S	55-615370
18daci	ASLD	9-2-5B	210	12			27	1,468	E E	<b>86</b> 120	R.			D.		D,S	***
l 8dac∑	Webb	5-11-05	235	8	200	175-	20	1,468 1,475	E	120						D	55-638430
19aab 1	Ogle	5-19-05	300	6	300	110 300	20 1,600	1,475		134.5		3/3/93	1,340,50	Đ	RP	lr	55-621945; chkd, eqpd
19aa62[BIA111]	SCIDD	05-47	412	20 16	500	110-3 <del>99</del> 196-795	1,000	1,412		134.3		3/3/73				_	
		10-24-75	800		800	130-133		1,475	E	_		***		D		0	55-533218, eathodic protection
19 <b>aab</b> 3	Southwest Gas	8-17-00	201	 8	381			1,473		220	R	3/26/73	1,251.00	D		D	55-638426
19abb	Martin	3-26-73	386	8 12	400		35	1,471		270	R			_		ď	55-629521
1966	Henry	4-26-77	400	12 10	130		33	1,472	Е	130	R	9/2/86		D		D	55-514208
19cac	Graham	9-2-86	400	10 LU	130 110-400	120-400		*,***			-			_			
				3	110 <del>-1</del> 00	120-400	***	1,396					_			U	Destroyed
(D-05-09)19cdd		1-4-40	300	20	300	94-285	1,800	1,490	•			11/1/88	1,360.50	D	RP	ſ	***
19ddd1	USDA	1-4-40	300	20	300		15	1,490	E							D	55-619762
19ddd2			402	20 8	402	362-392		1,485	E	240	R	5/15/91		D		ír,S	55-528330
20acb		5-15-91	402	о б		302-372		1,485	E	***						D,S	55-633548
20b <b>d</b> d	Mauldin	1-15-65	560	12	554	290-542	60	1,495		225			1,270.00	Ð	RP	1. 5 F	55 800831, registered as20c

				c	asing		Reported	Surface			Non-P	umping Wa	ter Level				
/ell Number	Owner*	Date Completed	Depth Drilled (ft)	Diameter (in)		Perforated Interval (ft)	Pumping Rate (gpm) <sup>c</sup>	Elevation (ft, msl)		Measured Depth (ft)		Date	Altitude (ft, msl)	Logs	Chemical Analyses <sup>k</sup>	Use¹	
20dad[BIA25]	SCIDD	4-21-05	300	20	300		1,600	1,504		176.1		3/2/93	1,327.90	D		lr	55-621933; chkd; eqpd
		6-8-61	760	16	760				***	***			•••				***
				14		175-755	2 200	1,504		178.6		3/2/93	1,325.40	D	RP	lr	55-621905; chkd; eqpd
20dcc[BIA122B]	SCIDD	7-28-78	1,225	20	598 590-1,223	220-588 594 1,215	2,300	1,304		170.0		312173	1,525.40	U	144		55 OZIVOV, ORAK, ORPA
			400	16 8	400	394 1,213	15	1,517		209.4		11/3/88	1,307.60			D	55-605136
2 laas l	Lewis	***	400	6	400			1,517	Е	130	R					D,S,Ir	55 805870
21aaa2 21add	Lewis  J & D Lewis Farms	6-15-51	510	20	473	225-473	2,000	1,527		245.2		11/13/84	1,281.80	D	RP	lr	55-605134
21add 21bba	Kempton	8-21-81	925	5	925	420-920	30	1,497	E	165	R			D		D	55-500587
21caa	Mosley	1077	350	8	350		35	1,512	E	200	R	***			•••	D	55-638446
21cdc	Yoakum	5-16-85	385	8	385	345-385		1,518	E	220	R			D		D	55-510303
	SCIDD	1-7-77	1,175	20		250-530	2,000	1,520		200.2		3/2/93	1,319.80	Đ	RP	İr	55-621927; registered as21dcb chkd; eqpd
, -				16		550 1,170											
22abb	Lewis	8-15-58	600	20	600	350-582	2,700	1,531		219.8		11/3/88	1,311.20	D		lr	55-612518
		12-13-77	1,132	18	585-785	585-785							***			***	
				16	765-1,050	765 1,050											
				12	1,040-1,130	1,040 1,130	3.000	1.663	r	1/0	р	•••		D		lr	Also reported as 22adc
22add1	England	2-4-48	580	20	580	170-568	2,000	1,552 1,552	E E	168	к					lr	Also reported as 22ade
22add2	England	6-9-05	1,000	20	348	124-335	2,800	1,532		113		11/18/46	1,418.00	D		Ü	Also reported as 22abb
22baa		12-22-36	348	20	348	124-333	2,800	1,528		251.4		4/14/70	1,276.60			lr	
22bab	1446144	 6-4-75	440	3	440	281-440	5	1,520		209.7		11/3/88	1,310.30	D	***	М	55-627628
22bbb1 22bbb2	MAGMA Southwest Gas	8-17-00						1,520	Ε					D		0	55-533188; cathodic protection
22cba[BIA112]	SCIDD	3-14-47	432	20	432	155-420	1,700	1,529		208		0193	1,321.00	D .	RP	lr.	55-621911; also reported as 22cbb; chkd; eqpd
22C0a[DIX112]	SCIDD	7-31-75	1,154	16	1,152	245-1,145											
22daa	England Farms	2-4-48	580	20	580	170-568	2,000	1,554		248.1		11/4/88	1,305.90	D	***	lr	55-618508; registered as22ddd
22ddd	England Farms	12-23-47	636	20	636	180-624	2,200	1,559		251.6		11/4/88	1,307.40	D	RP	ir	55-618509
24ddd	Hilgeman	4-13-05		12			15	1,630	E	204	R				***	S,D	55-638760
-05-10) 6abc1[SG-3]	USBR	11-23-77	1,170	8	20			1,545						D,L,G		Pz Pz	
6abc2[PZ 2]	USBR	11-23-77	1,170	1-1/4	219	210-219		1,545		246.1		3/21/78	1,298.90			Pz Pz	
6abc3[PZ 1]	USBR	11-23-77	1,170	1-1/4 20	513	504-513 150-408	1,713	1,545 1,540		213.5		3/8/93	1,326.50	D	R.P	ir,PS,I	55-610136; chkd; cqpd
6bcc	ADC	10-15-47	416 1,100	20 5	1,100	130-408 580 L080	1,713	1,540	E	204	R	4/26/88	1,520.50	D		M	55-520262
6bdc1	ADC ADC	4-26-88 3-3-89	1,100	16	1,100	580 1,100		1,540	E	201	R		***	D		D	55-523132
6bdc2	England	5-15-05	165	8		40	3	1,590	E	28	R			D	***	S	
7aaa 8aaa	Ryan					***		1,640	E						•	D	55-530542
8aad	Corbin		400	6			35	1,650	Ε	390	·R					D,S	55-634980
8baa	Underwood	5-11-05	480	8	480			1,618		280	R		1,338.00			D	55 803767; registered as 8aac
8bab l	Underwood	5-6-05	350	6	350		35	1,612	E			***				D	55 800855
8bab2	Mayfield	0375	492	8			35	1,612		302	R		1,310.00		***	D	55-630222
8bad	Corbet			6				1,625								D	
8bba	Mayfield	2-17-89	460	6	340		14	1,605	Ε	300	R	2/17/89		D	***	D	55-523233
(0.04.40) 0111:	M 6.11	9 22 95	410	5	320-460	279 410	25	1,600	E	278	R	8/23/85		Đ	***	D	55-508658
(D-05-10) 8bbb1	Mayfield	8-23-85 1-5-92	418 500	8 6	500	378-418 360-500	25	1,600	E	300	R	8/23/83 1/5/92		D		ם	55-533444
8bbb2 8bbb3	Mayfield Underwood	1-3-92 2-12-92	500	5	500	360-300		1,600	E	300	R	1/3/92		D		D	55-533745
8bcb1	Mayfield	8-3-84	403	8	403	358-403	23	1,610	É	296	R	8/3/84		D		D	55-508659
8bcb2	Carrasco	2-9-87	420	6	420	300-420	7	1,610	E	305	R	2/9/87		D		D,Ir	55-514613
8bcc	Mayfield	7-11-84	409	8	409	364-409	23	1,610	E	296	R	7/11/84		D	•••	D	55-508530
8bcd	Mayfield	7-25-84	405	8	405	360-405	23	1,620	E	296	R	7/25/84		D		D	55-508531
8dcc	Kimbrell	6-25-92	500	4	480	380-480		1,650	E	320	R	6/25/92		D		D	55-535322
8dda	Montgomery							1,670	E	***	***	***		Ð		D	55-516383
8ddc1	Contreras	5-27-05	510	8	510			1,668	E	350	R			D		D	
8ddc2	Beeler	9-4-79	530	10	12		35	1,668		370	R		1,298.00	D		D	55-632587
				8	530												
8ddc3	Whitworth	10-21-91	508	4	490	370-490	19	1,668	E	300	R	10/21/91		D		D	55-533107
8ddd 1	Contreras	5-24-01	8	110		***	13	1,675		345	R					D	55-646077
17	Showmake		535	6	535		10			350	R				***	D	55-631478
17aaa	Curtis	9-5-86	500	6	500	380-500	12	1,678		349,3		3/8/93	1,328.70	D		D	55-514512; chkd; cqpd
17aab	Stephens	2-13-74	507	8	500	400-500	10	1,672		340	R		1,332.00	D	***	D,Ir	55-629979

Table 2.3-1. Summ	ary of Information	n Concernin	g Existin	g Wells	Within 5	Miles of th	e Florence	e In-Situ	Mine	Area							
Well Number	Owner *	Date Completed	•	Diameter	asing Depth (ft)	Perforated Interval (ft)	Reported Pumping Rate (gpm) <sup>c</sup>	Surface Elevation (ft, msl)*		Measured Depth (ft	l	umping Wa Date	ater Level Altitude (ft, msl)	Logs*	Chemical Analyses <sup>k</sup>	Use '	Remarks <sup>1</sup>
17-1-	Kelm							1,659					***			D	***
ii .		4-3-82	500	6	490	340-490	7	1,660		343	R	4/3/82	1,317.00	D		D	55-502088
17acbl	•		480	6	450	***	35	1.660		350	R		1,310.00			D	55-632780
	Montgomery	4 20 40	480	4	430		5	1,665	F	340	R					Ð	55-602376
11	Montgomery	8-20-80		0			11	1,685	E	355	P	3/6/82		D		D	55-500849
17add	Kelm	3-6-82	500	6	490	340-490	11	,			ĸ			n n			55-507127
19bcc	Hassett							1,625	E					U			
10/45	Wood	5-2-86	520	6	520	420-520	10	1,660	E	357	R	5/2/86		D	•••	D	55-513829

Source: Montgomery (1994)

a MAGMA = Magma Copper Company USBR - United States Bureau of Reclamation SCIDD = San Carlos Irrigation and Drainage District

19dab Wood

ADC = Arizona Department of Corrections

LDS = Church of Jesus Christ of Latter Day Saints ASLD = Arizona State Land Department

USDA = United States Department of Agriculture

b feet = feet below land surface

c gpm = gallons per minute

d Altitude of land surface

S = determined from survey data

E = estimated from topographic map

All other values obtained from USGS and ADWR files

e feet,msl = feet above mean sea level

f Depth in feet below land surface

R = reported

g Logs available

D = Driller

L = Lithologic

G = Geophysical

h Water chemistry analyses available

RP = Routine parameters

C = Common constituents

i Well use

5-2-86

lr = irrigation

M = monitor D = domestic

U = unused

E = mineral exploration borehole

O = other

S = stock

Pz = piczometer

PS = public supply

I = industrial

T = test

A = abandoned

j Remarks

UTL = unable to locate, March 1993

Chkd = field checked, March 1993

UTM = unable to measure, March 1993

Eqpd = equipped with pumping equipment

Note: Selected data included in this table also included in Table B-4

Table 2.3-2.	Summary	of Inform	nation Concern	ing Existing V	Vells With	in One-Hal	f Mile	of the Floren	ce In-Situ	Mine Are	a			
Well ID*	Well Correlation Tables <sup>a</sup>	Well Type	Location/ ADWR No.**	Location Coordinates (Northing Easting)	Land Elevation (feet) <sup>b</sup>	Reference Point Elevation (feet) <sup>b</sup>	Total Depth (feet) <sup>c</sup>	Casing Diameter	Screened Interval (feet) <sup>c</sup>	Screened Zone	Top of Bedrock (feet) <sup>c</sup>	Date Installed	Well Owner	Condition/Remarks
Supply Well 1 (Magma Supply)	B-5	Irrigation	D(4-9)27cad 55-627614	745868.98N 654275.22E	1473	NA	500	20";0-290 16";290-500	62-490	G	NA	3-25-62	Magma	No access. Supplies water to Magma facilities.
Supply Well 2 (Farm Supply)	C1, C2, B-5	Domestic	D(4-9)27cac 55-627613 aka: D(4-9)27cab	746414.26N 653019.03E	1480	NA	305	10"	203-295	G	NA	2-3-55	Magma	Supplies to local domestic water Pump: Tri-clad induction motor 230/460V, 1755 RPM, 20 HP, Model 5K6236XH4B, 3 phase, 60 cycles
D(4-9)27cbd	B3, C1, C2, B-5		D(4-9)27cbd 55-627656 aka: 27cbd2	745976.72N 652973.87E	1472									Unable to locate. Limited information available.
MF2 (MF-Y)	B1, B3, B-5	Irrigation	D(4-9)28cdb 55-627641 aka: D(4-9)28cdbc D(4-9)28cdb1	745425.00N 647830.00E	1474.20	1477.10	520	20"	NA	NA	NA	1961	NA	Discharge rate in 1971 was 1,225 gpm. 2.85-foot stickup of 5.7-inch steel casing.
			D(4-9)32ada 55-627604	743140.00N 646505.00E	1453	NA	473	20";0-265 16";265-473	100-473	NA	NA	1961	Magma	Well is abandoned.
England 3	B3, B-5	Irrigation	1 \ /	746050.00N 652800.00E	1470	NA	410	20";0-410	210-400	G	400	1961	Magma	20-inch casing from 0 to 410 feet. Production rate was 1,440 gpm in 1971.
PW-1 (Conoco	B1, B3, B-5	Industrial	D(4-9)28dbd 55-627606 aka: D(4-9)dbd2	746030.00N 650070.00E	1467.80	1467.80	949	18";0-540 14";540-937	243-947	- G,O	340	12-2-74		18-inch steel surface casing from 0 to 538 feet. 14-inch steel casing from 0 to 949 feet. Production rate was 450 gpm in 1976.

<sup>&</sup>quot;The following are other tables which correlate with wells listed in the table.

<sup>·</sup> C1, C2: Existing water quality data, Appendix C, Volume II

<sup>·</sup> B1, B2, B3: Water level data, Appendix B, Volume II

<sup>·</sup> B5, Well data included in Montgomery and Associates (1994)

<sup>&</sup>lt;sup>b</sup>Feet above mean sea level (MSL)

Feet below ground surface

<sup>\*</sup> The well ID listed first identifies the well name most commonly used with respect to documentation and well recognition. Any other names found for a particular well are also listed as a reference.

<sup>\*\*</sup> The correct well identification is based on location and is listed first followed by all other numbers referenced to that well as found in various reports and documents.

Table 2.3-2.	Summary	of Inforn	nation Concern	ing Existing \	Vells With	in One-Hal	f Mile	of the Floren	ice In-Situ	Mine Are	a			
Well ID*	Well Correlation Tables*	Well Type	Location/ ADWR No.**	Location Coordinates (Northing Easting)	Land Elevation (feet) <sup>b</sup>	Reference Point	Total Depth (feet) <sup>c</sup>		Screened Interval (feet) <sup>c</sup>		Tóp of	Date Installed	Well Owner	Condition/Remarks
PW-2 (Conoco	B1, C1, B-5	Industrial	, ,	747070.00N 647940.00E	1483.17	1483.57	981	18";0-621 14";621-981	234-981	G,O	580	1-29-75	Magma	18-inch steel surface casing 0 to 621 feet. 14-inch steel casing from 0 to 981 feet. Production rate was 1,600 gpm in 1976.
- PW-3 (Conoco 3, WW-3)		Irrigation	D(4-9)28cdb 55-627608 aka: D(4-9)28cdbb D(4-9)28cdb2		1470	1470	938	18";0-496 14";496-936	240-933	G,O	372	11-21-74	Magma	18-inch surface casing from 0 to 496 feet. 14-inch casing from 496 to 933 feet. Production rate was 1,500 gpm in 1976. Previously Conoco 3.
PW-4 (Conoco 4, WW-4)	B1, B3, C1,		D(4-9)33aad 55-627609 aka: D(4-9)33aada	743778.00N 651583.00E	1456.60	1456.60	997	18";0-598 14";598-997	252-997	G,O,S	375	12-15-74	Magma	18-inch steel casing from 0 to 598 feet. 14-inch casing from 0 to 997 feet. Production rate was 1,000 gallons per minute (gpm) in 1977. Previously Conoco 4.
PW-20 (Conoco 20)	C1, C2, B-5		D(4-9)29dca 55-627610 aka:D(4-	745370.00N 644620.00E	1460	NA	1180	18";0-1176	229- 1,176	G,O	930	1975	Magma	18-inch surface casing from 0 to 1,176 feet. Production rate was 2,000 gpm in 1976. West of the in-situ mine area. Pump: 4 stage Worthington, 15H-277, 400 HP, 460 V, set at 600 feet.
OB-1 (OW-1,	B1, B3, C1,	Monitor	D(4-9)28cda aka: D(4-9)28cda3	745613.75N 648660.86E	1472.12	1472.12	1498	5";0-1,035	470- 1,035	0	455	1972	Magma	10 5/8-inch steel surface casing from 0 to 68 feet. 8 5/8-inch blank steel casing from 0 to 47 feet. 5 1/2-inch steel casing perforated from 470 to 1,035 feet. Cement plug set at 1,035 feet.

<sup>\*</sup>The following are other tables which correlate with wells listed in the table.

<sup>·</sup> C1, C2: Existing water quality data, Appendix C, Volume II

<sup>·</sup> B1, B2, B3: Water level data, Appendix B, Volume II

<sup>·</sup> B5, Well data included in Montgomery and Associates (1994)

<sup>&</sup>lt;sup>b</sup>Feet above mean sea level (MSL)

<sup>&#</sup>x27;Feet below ground surface

<sup>\*</sup> The well ID listed first identifies the well name most commonly used with respect to documentation and well recognition. Any other names found for a particular well are also listed as a reference.

<sup>\*\*</sup> The correct well identification is based on location and is listed first followed by all other numbers referenced to that well as found in various reports and documents.

Table 2.3-2.	Summary	of Inform	nation Concern	ing Existing \	Vells With	in One-Hal	f Mile	of the Floren	ce In-Situ	Mine Are	a			
Well ID*	Well Correlation Tables*	Well Type	Location/ ADWR No.**	Location Coordinates (Northing Easting)	Land Elevation (feet) <sup>b</sup>	Reference Point Elevation (feet) <sup>b</sup>	Total Depth (feet)	Casing Diameter	Screened Interval (feet) <sup>c</sup>	Screened Zone	Top of Bedrock (feet) <sup>c</sup>	Date Installed	Well Owner	Condition/Remarks
OB-2 (OW-2, OB-2 Conoco)	B1, C1, C2,		D(4-9)28cad aka: D(4-9)28cad1	745947.97N 649003.90E	, .** 1473.47	1473.47	1600	8";0-295 5";295- 1,030	285- 1,030	S	368.5	1972	Magma	13 3/8-inch blank steel surface casing from 0 to 51 feet. 8 5/8-inch blank steel casing from 0 to 295 feet. 5 1/2-inch casing perforated from 285 to 1,030 feet. Cement plug set at 1,030 feet.
OB-3 (McFarland 1, OW-3,Mf H20, MFZ)	B3, C1, C2, B-5	Irrigation	D(4-9)28cda 55-627640 aka: D(4-9)28cda1 D(4-9)28cdab		NA	NA	560	20";0-260 16";260-560	75-560	G	NA	7-6-63	Magma	Unused
OB-4	B-5	Monitor	D(4-9)28ddb	745194.72N 650636.16E	NA	NA	350	3"	160-340	G	NA	NA	Magma	Unable to locate
OB-5	B-5	Monitor	D(4-9)28cda	745115.23N 649038.11E	NA	NA	350	3"	160-340	G	NA	NA	Magma	Unable to locate
OB-6	B1, B-5	Monitor	D(4-9)28cad	746472.00N 648486.00N	1470.52	1472.30		4"					Magma	Aquifer test conducted 2/7/94 to 2/14/94. Pumped from PW-1.
OB1-1	B-5	Monitor	D(4-9)28caa	746428.25N 648750.08E	1476.48	NA	760	4"	360-740	О	360	1994	Magma	Aquifer test conducted 2/7/94 to 2/14/94.
OB2-1	B-5	Monitor	D(4-9)28dbc aka: D(4-9)28dbd	746157.89N 649563.89E	1471.56	NA	640	4"	400-620	o	340	1994	Magma	Aquifer test conducted 3/8/94 to 3/21/94.
OB2-2	B-5	Monitor	D(4-9)28dcb	745500.7N 649879.13E	1464.02	NA	800	4"	460-760	, O	360	1994		Pump test conducted 4/20/94 to 5/2/94.
	B-5	Monitor	D(4-9)28cbb	746204.02N 647890.16E	1475.78	NA	800	4"	500-780	0	430	1994	Magma	Aquifer test conducted 3/24/94 to 3/31/94.
OB4-1	B-5	Monitor	D(4-9)28cca	745584.31N 647783.01E	1471.70	NA	800	4"	440-780	0	380	1994	Magma	Aquifer test conducted 5/19/94 to 5/31/94.

<sup>\*</sup>The following are other tables which correlate with wells listed in the table.

<sup>·</sup> C1, C2: Existing water quality data, Appendix C, Volume II

<sup>·</sup> B1, B2, B3: Water level data, Appendix B, Volume II

<sup>·</sup> B5, Well data included in Montgomery and Associates (1994)

<sup>&</sup>lt;sup>b</sup>Feet above mean sea level (MSL)

<sup>&#</sup>x27;Feet below ground surface

<sup>\*</sup> The well ID listed first identifies the well name most commonly used with respect to documentation and well recognition. Any other names found for a particular well are also listed as a reference.

<sup>\*\*</sup> The correct well identification is based on location and is listed first followed by all other numbers referenced to that well as found in various reports and documents.

Table 2.3-2.	Summary	of Inforn	nation Concern	ing Existing V	Vells Withi	n One-Hal	f Mile	of the Floren	ice In-Situ	Mine Area	a			
Well ID*	Well Correlation Tables*	Well Type	Location/ ADWR No.**	Location Coordinates (Northing Easting)	Land Elevation (feet) <sup>b</sup>	Reference Point Elevation (feet) <sup>b</sup>	Total Depth	Casing Diameter	Screened Interval (feet) <sup>c</sup>	Screened Zone	Top of Bedrock (feet) <sup>c</sup>	Date Installed	Well Owner	Condition/Remarks
OB7-1	B-5	Monitor	D(4-9)28cda	745455.55N 648872.17E	1468.27	NA	900	4"	540-880	0	370	1994	Magma	
PW1-1	B1, B-5	Test	D(4-9)28caa	746476.50N 648742.16E	1477	1477	760	6"	360-740	О	360	1994	Magma	Aquifer test conducted 2/7/94 to 2/14/94.
PW2-1	B1, B-5	Test	D(4-9)28dbc aka: D(4-9)28dbd	746199.14N 649536.12E	1471	1471.90	640	6"	400-620	О	340	1994	Magma	Aquifer test conducted 3/8/94 to 3/21/94.
PW2-2	,	Test	D(4-9)28dcb	745543.15N 649854.34E	1464.30	1465.20	800	6"	460-760	О	360	1994	Magma	Pump test conducted 4/20/94 to 5/2/94.
PW3-1	B1, B-5	Test	D(4-9)28cbb	746250.70N 647873.55E	1475.50	1476.40	800	6"	500-780	0	430	1994	Magma	Aquifer test conducted 3/24/94 to 3/31/94.
PW4-1	B1, B-5	Test	D(4-9)28cca	745530.80N 647769.65E	1471.80	1472.15	800	6"	440-780	0 ,	380	1994	Magma	Aquifer test conducted 5/19/94 to 5/31/94.
PW7-1	B1, B-5	Test	D(4-9)28cda	745467.86N 648823.52E	1468.60	1468.60	900	6"	540-880	О	370	1994	Magma	·
Airshaft (North Shaft)	B-5	Test	D(4-9)28dbc aka: D(4-9)28dbc1	746460.43N 649349.76E	1476	NA	706	42";0-700	NA	NA	NA	1974	Magma	
Shaft No. 1 (South Shaft)	B-5	Test	D(4-9)28dbc aka: D(4-9)28dbc2	746374.85N 649349.49E	1476	NA	730	72";0-715	NA	NA	NA	1974	Magma	
84	B1, B-5	Explorati on Borehole	D(4-9)28add	747250.00N 651188.00E	1480.5	ŅĀ	340	3"	NA	NA	NA	NA	Magma	Well has been plugged off.

<sup>\*</sup>The following are other tables which correlate with wells listed in the table.

<sup>·</sup> C1, C2: Existing water quality data, Appendix C, Volume II

<sup>·</sup> B1, B2, B3: Water level data, Appendix B, Volume II

<sup>·</sup> B5, Well data included in Montgomery and Associates (1994)

<sup>&</sup>lt;sup>b</sup>Feet above mean sea level (MSL)

<sup>&</sup>lt;sup>e</sup>Feet below ground surface

<sup>\*</sup> The well ID listed first identifies the well name most commonly used with respect to documentation and well recognition. Any other names found for a particular well are also listed as a reference.

<sup>\*\*</sup> The correct well identification is based on location and is listed first followed by all other numbers referenced to that well as found in various reports and documents.

Table 2.3-2.	Summary	of Inform	nation Concern	ing Existing V	Vells Withi	in One-Hal	f Mile	of the Floren	ce In-Situ	Mine Area	a			
Well ID*	Well Correlation Tables <sup>a</sup>	Well Type	Location/ ADWR No.**	Location Coordinates (Northing Easting)	Land Elevation (feet) <sup>b</sup>	Reference Point	Total		Screened Interval (feet) <sup>c</sup>	Screened Zone	Top of Bedrock (feet) <sup>c</sup>	Date Installed	Well Owner	Condition/Remarks
BIA 9	B1, B3, C1, C2, B-5	Irrigation	D(4-9)28cca 55-621948 aka: D(4-9)28cca2 D(4-9)28cdb	745732.41N 647305.26E	1472.50	1472.50	500	20";0-254 16";254-495	80-495	G,O	NA	NA	SCIDD	Top oil drip. Sounding tube. Flow meter removed.
BIA 10B	B3, C1, C2, B-5	Irrigation	D(4-9)28cda 55-621949 aka: D(4-9)28cda2	745638.16N 649114.65E	1468.60	1468.60	2006	20";0-909 13";909- 1,909	200- 1,909	G,O,S	345	8-15-72	SCIDD	Sounding tube. Drip oil. Flow meter. Plug in side of discharge pipe.
BIA-10	B-5	Irrigation	D(4-9)28dad aka: D(4-9)27cac	746222.00N 651764.00E	1472.3	NA	259	20";0-259	107-247	NA	NA	4-16-34	NA	Concrete slab with 3-inch steel pipe protruding up with no access.
DM-A	B3, C1, C2,	Test	D(4-9)28cad aka: D(4-9)28cad2	746381.80N 649148.51E	1477.05	1478.70	700	5";0-382	NA	NA	350	NA	Magma	Unable to locate.
DM-B	C1, C2, B-5	Test	D(4-9)28cac 55-806521	746381.71N 648246.90E	1477.30	1478.11	700	5";0-611 4";611-700	NA	NA	574	NA	Magma	Unable to locate.
рм-с	B1, B3, C1, C2, B-5	Test	D(4-9)28dbd 55-806520 aka: D(4-9)28dbd1	746384.92N 650185.43E	1471.49	1473.10	610	5";0-358	NA	NA	335	1974	Magma	
DM-D	B3, C1, C2, B-5	Test	D(4-9)28dba aka: D(4-9)28dbd	746842.25N 649740.28E	1478.85	1480.10	635	5";0-364	NA	NA	350	NA	Magma	Unable to locate.
DM-E	B3, C1, C2, B-5	Test	D(4-9)28ddb	745516.10N 650741.49E	1465.0	1464.94	700	5";0-392	NA	NA	342	NA	Magma	Unable to locate.
D(4-9)27bbd	B-5	Recharge	D(4-9)27bbd 55-627646	NA	NA	NA	765	6";0-765	NA	NA	NA	8-15-77	Magma	Unable to locate.

<sup>&</sup>quot;The following are other tables which correlate with wells listed in the table.

<sup>·</sup> C1, C2: Existing water quality data, Appendix C, Volume II

<sup>·</sup> B1, B2, B3: Water level data, Appendix B, Volume II

<sup>·</sup> B5, Well data included in Montgomery and Associates (1994)

<sup>&</sup>lt;sup>b</sup>Feet above mean sea level (MSL)

<sup>&#</sup>x27;Feet below ground surface

<sup>\*</sup> The well ID listed first identifies the well name most commonly used with respect to documentation and well recognition. Any other names found for a particular well are also listed as a reference.

<sup>\*\*</sup> The correct well identification is based on location and is listed first followed by all other numbers referenced to that well as found in various reports and documents.

Table 2.3-2.	Summary	of Inforn	nation Concern	ing Existing \	Vells With	in One-Hal	f Mile	of the Floren	ce In-Situ	Mine Area	a			
Well ID*	Well Correlation Tables*	Well Type	Location/ ADWR No.**	Location Coordinates (Northing Easting)	Land Elevation (feet) <sup>b</sup>	Reference Point Elevation (feet) <sup>b</sup>	Total Depth (feet) <sup>c</sup>	· Casing Diameter	Screened Interval (feet)	Screened Zone	Top of Bedrock (feet) <sup>c</sup>	Date Installed	Well Owner	Condition/Remarks
D(4-9)27dbb		Unknown	unknown.	746486.00N 654444.00E	NA	NA	NA	6"	NA	NA	NA	NA	unknow n	1-foot steel casing stickup. Wel cap is locked.
D(4-9)28cbc	B-5	Monitor	D(4-9)28cbc	746208.00N 646722.00E	NA	NA	NA	. 5"	NA	NA	NA	NA	Magma	.9-foot casing stickup. Steel plate tack welded over casing.
D(4-9)29dab	B-5	Industrial	D(4-9)29dab 55-609666		1,475.0	NA	1,625	7";0-1,600	NA	NA	NA	8-25-71	Magma	1.2-foot casing stickup.
D(4-9)29dac	B-5	Industrial	D(4-9)29dac 55-609667		1,465.0	NA	1,098	11";0-1,098	NA	NA	NA	7-31-71	Magma	Unable to locate.
M1-GL	В1	Monitor	D(4-9)33bac 55-547617	743799.85N 648550.02E	1461.1	1462.4	420	5";0-365	315-355	G	NA	6-17-95	Magma	1.5-foot LCS casing stickup. Installed Pump at 280 feet: Grundfos Model 10S-10-15, 1.0 HP, 460V
M2-GU	B1	Monitor	D(4-9)33bbc	743737.92N 651658.43E	1459	1460.8	270	5";0-258	198-238	G	NA	5-25-95	Magma	1.5-foot LCS casing stickup. Installed pump at 180 feet: Grundfos Model 10S-10-15, 1.0 HP, 460V
M3-GL	B1		D(4-9)33bbc 55-547614	743685.56N 651636.79E	1458.8	1460.74	370	5";0-358.5	298-338	Ġ	NA	5-23-95	Magma	1.5-foot LCS casing stickup. Installed pump at 200 feet; Grundfos Model 10S-10-15, 1.0 HP, 460V
M4-O	B1	Monitor	D(4-9)33bbc 55-547615	743717.36N 651635.22E	1458.9	1460.6	510	5";0-485	405-465	0	370	5-21-95		1.5-foot LCS casing stickup. Installed pump at 380 feet; Grundfos Model 10S-15-21, 1.5 HP, 460V.
M5-S	B1	Monitor	D(4-9)33bbc 55-547616	743719.46N 651685.49E	1459.1	1460.47	613	5";0-516 4";516-597	516-576	. S	370	5-18-95	Magma	1.5-foot LCS casing stickup. Installed pump at 500 feet; Grundfos Model 25S-20-26, 2.0 HP, 460V.

<sup>\*</sup>The following are other tables which correlate with wells listed in the table.

<sup>·</sup> C1, C2: Existing water quality data, Appendix C, Volume II

<sup>·</sup> B1, B2, B3: Water level data, Appendix B, Volume II

<sup>·</sup> B5, Well data included in Montgomery and Associates (1994)

<sup>&</sup>lt;sup>b</sup>Feet above mean sea level (MSL)

<sup>°</sup>Feet below ground surface

<sup>\*</sup> The well ID listed first identifies the well name most commonly used with respect to documentation and well recognition. Any other names found for a particular well are also listed as a reference.

<sup>\*\*</sup> The correct well identification is based on location and is listed first followed by all other numbers referenced to that well as found in various reports and documents.

Table 2.3-2.	Summary	of Inforn	nation Concern	ing Existing V	Wells Withi	in One-Hal	f Mile	of the Floren	ce In-Situ	Mine Area	a			
Well ID*	Well Correlation Tables	Well Type	Location/ ADWR No.**	Location Coordinates (Northing Easting)	·	Reference Point Elevation (feet) <sup>b</sup>	Total Depth (feet) <sup>c</sup>	Casing Diameter	Screened Interval (feet) <sup>c</sup>	Screened Zone	Top of	Date Installed	Well Owner	Condition/Remarks
M6-GU	B1	Monitor	D(4-9)28bcc 55-547815	747556.46N 647256.92E	1480.5	1481.72	590	5";0-583	524-564	G	NA	3-31-95	Magma	1.5-foot PVC casing stickup. Installed pump at 500 feet; Grundfos Model 10S-20-27, 2.0 HP, 460V.
M7-GL	B1	Monitor	D(4-9)28bcc 55-547611	747531.69N 647282.21E	1480	1480.95	940	5";0-592 4";592-928	859-919	G	NA	4-6-95	Magma	1.0-foot LCS casing stickup. Installed pump at 580 feet; Grundfos Model 10S-50-58DS, 5.0 HP, 460V.
M8-O	B1	Monitor	D(4-9)28bcc 55-547612	747523.83N 647230.35E	1479.1	1480.46	1115	5";0-591 4";591-1091	1,011- 1,071	О	940	4-12-95	Magma	Installed pump at 580 feet; Grundfos Model 7S-15-26, 1.5 HP, 460V.
M9-S	В1	Monitor	D(4-9)28bcc 55-547613	747555.92N 647207.61E	1479.5	1481.18	1578	5";0-502 4";502-1570	1,510- 1,570	S	930	3-23-95	Magma	Installed pump at 1377 feet; Grundfos Model 10S-50-48DS, 5.0 HP, 460V.
M10-GU	В1	Monitor	D(4-9)28dcb 55-547816	745467.53N 649798.29E	1464.3	1465.77	290	5";0-268	218-258	G	NA	5-10-95	Magma	Installed pump at 200 feet; Grundfos Model 10S-10-15, 1.5 HP, 460V.
M11-GL	B1	Monitor	D(4-9)28dcb 55-547817	745471.70N 649749.77E	1464.6	1466.01	370	5";0-350	290-330	G	NA	5-9-95	Magma	1.5-foot LCS casing stickup. Installed pump at 260 feet; Grundfos Model 10S-10-15, 1.0 HP, 460V.
M12-O	B1	Monitor	D(4-9)28dcb 55-547818	745506.14N 649798.24E	1464.3	1465.56	510	5";0-501	420-480	0	350	5-6-95		1.5-foot LCS casing stickup. Installed pump at 260 feet; Grundfos Model 10S-15-21, 1.5 HP, 460V.
M13-S	BI	Monitor	D(4-9)28dcb 55-547819	745507.59N 649748.96E	1464.3	1465.86	943	5";0-931	851-911	S	360	4-25-95		1.8-foot LCS casing stickup. Installed pump at 840 feet; Grundfos Model 16S-50-38, 5.0 HP, 460V.

<sup>\*</sup>The following are other tables which correlate with wells listed in the table.

- · C1, C2: Existing water quality data, Appendix C, Volume II
- · B1, B2, B3: Water level data, Appendix B, Volume II
- · B5, Well data included in Montgomery and Associates (1994)

<sup>&</sup>lt;sup>b</sup>Feet above mean sea level (MSL)

<sup>&</sup>quot;Feet below ground surface

<sup>\*</sup> The well ID listed first identifies the well name most commonly used with respect to documentation and well recognition. Any other names found for a particular well are also listed as a reference.

<sup>\*\*</sup> The correct well identification is based on location and is listed first followed by all other numbers referenced to that well as found in various reports and documents.

Table 2.3-2.	Summary	of Inforn	nation Concern	ing Existing V	Wells With	in One-Hal	f Mile	of the Floren	ice In-Situ	Mine Are	a			
Well ID*	Well Correlation Tables*	Well Type	Location/ ADWR No.**	Location Coordinates (Northing Easting)	Land Elevation (feet) <sup>b</sup>	Reference. Point Elevation (feet) <sup>b</sup>	Total Depth (feet)	Casing Diameter	Screened Interval (feet) <sup>c</sup>	Screened Zone	Top of Bedrock (feet) <sup>c</sup>	Date Installed	Well Owner	Condition/Remarks
M14-GL	B1	Monitor		746414.71N 646961.20E	1472.8	1474.58	950	5";0-859	778-838	G	NA	6-2-95	Magma	1.5-foot LCS casing stickup. Installed pump at 260 feet; Grundfos Model 10S-10-15, 1.0 HP, 460V.
M15-GU	B1	Monitor	D(4-9)28cbc	746418.02N 646908.14E	1472.6	1474.01	630	5";0-615	554-594	G	NA	6-6-95	Magma	1.5-foot LCS casing stickup. Installed pump at 260 feet; Grundfos Model 10S-10-15, 1.0 HP, 460V.
M16-GU	BI	Monitor	D(4-9)28acc 55-549140	745025.42N 647017.35E	1464.3	1466.05	690	5";0-678	598-658	G	NA	6-22-95		1.5-foot LCS casing stickup. Installed pump at 260 feet; Grundfos Model 5S-10-22, 1.0 HP, 460V.
M17-GL	B1	Monitor	D(4-9)28acc 55-549141	744976.80N 647017.02E	1464.4	1466.16	1130	5";0-1,018.5	938-998	G	NA	6-18-95		2.5-foot LCS casing stickup. Installed pump at 340 feet; Grundfos Model 10S-15-21, 1.5 HP, 460V.
M18-GU	B1	Monitor	D(4-9)33bac 55-547809	743800.82N 648501.52E	1461	1461.75	240	5";0-228	178-218	G	NA	6-18-95	Magma	1.5-foot LCS casing stickup. Installed pump at 170 feet; Grundfos Model 10S-10-15, 1.0 HP, 460V.
O3-GL	B1	Monitor	D(4-9)28cda 55-549153	745444.25N 648922.36E	1468.1	1469.35	395	5";0-385	325-365	G	NA	5-11-95	Magma	1.6-foot LCS casing stickup. Aquifer test performed 6/95, 8/95, 9/95.
O5.1-O	B1	Monitor	D(4-9)28dcc 55-549144	744718.01N 649599.80E	1462.2	1463.44	880	5";0-494 4";494-853	674-832	ó	360	5-25-95	Magma	1.5-foot LCS casing stickup.
O5.2-O	B1	Monitor	D(4-9)28dcc 55-549145	744701.23N 649524.74E	1462.2	1463.47	880	4";0-792	712-771	0	380	5-20-95	Magma	1.5-foot LCS casing stickup.

<sup>&</sup>quot;The following are other tables which correlate with wells listed in the table.

<sup>·</sup> C1, C2: Existing water quality data, Appendix C, Volume II

<sup>·</sup> B1, B2, B3: Water level data, Appendix B, Volume II

<sup>·</sup> B5, Well data included in Montgomery and Associates (1994)

<sup>&</sup>lt;sup>b</sup>Feet above mean sea level (MSL)

<sup>°</sup>Feet below ground surface

<sup>\*</sup> The well ID listed first identifies the well name most commonly used with respect to documentation and well recognition. Any other names found for a particular well are also listed as a reference.

<sup>\*\*</sup> The correct well identification is based on location and is listed first followed by all other numbers referenced to that well as found in various reports and documents.

Table 2.3-2.	2.3-2. Summary of Information Concerning Existing Wells Within One-Half Mile of the Florence In-Situ Mine Area								3					
Well ID*	Well Correlation Tables*	Well Type	Location/ ADWR No.**	Location Coordinates (Northing Easting)	1	Reference Point Elevation (feet) <sup>b</sup>	Total Depth (feet) <sup>c</sup>	Casing Diameter	Screened Interval (feet) <sup>c</sup>	Screened Zone	Top of Bedrock (feet) <sup>c</sup>	Date Installed	Well Owner	Condition/Remarks
							,		414-454 473-513 533-572 592-632 671-691 711-730					
P5-O	B1	Test	D(4-9)28dcc 55-549147	744696.96N 649499.22E	1462.4	1463.8	800	6";0-790	750-770	0	375	5-22-95	Magma	1.5-foot PVC casing stickup.
O8-O		Monitor	D(4-9)28dbb 55-549164	74690312N 649393.299E	1479.5	1481.3	610	4";0-599.5	401.5- 579	0	353	8-26-95	Magma	1.5-foot LCS casing stickup. Aquifer test performed 9/95.
O8-GU	B1	Monitor	D(4-9)28dbb 55-549165	746792.74N 649386.23E	1478.0	1479.8	270	4";0-261	133-251	G	NA	8-16-95	Magma	1.5-foot LCS casing stickup. Aquifer test performed 9/95.
P8.1-O	BI	Test	D(4-9)28dbb 55-549166	746793.36N 649403.82E	1478.0	1478.8	616	6";0-600	399.5- 580	0	353	8-14-95	Magma	1.5-foot LCS casing stickup. Aquifer test performed 9/95.
P8.2-O	B1	Test	D(4-9)28dbb 55-549166	746863.66N 649289.85E	1478.2	1479.7	610	6";0-596.5	396-576	0	360	8-23-95	Magma	1.5-foot LCS casing stickup. Aquifer test performed 9/95.
P8-GU	B1	Test	D(4-9)28dbb 55-549167	746846.80N 649293.48E	1477.7	1479.7	270	6";0-259	128-248	G	NA	8-25-95	Magma	1.5-foot LCS casing stickup. Aquifer test performed 9/95.
012-0	B1	Monitor	D(4-9)28cdc 55-549169	744745.55N 648411.81E	1466.5	1469.06	970	4";0-950	434-929	0	380	5-18-95	Magma	2.0-foot LCS casing stickup. Aquifer test performed 6/95, 8/95, 9/95.
012-GL	В1	Monitor	D(4-9)28cdc 55-549170	744739.89N 648436.70E	1466.2	1468.09	395	5";0-385	325-365	G	NA	5-11-95	Magma	1.6-foot LCS casing stickup. Aquifer test performed 6/95, 8/95, 9/95.
P12-O	B1	Test	D(4-9)28cdc 55-549171	744708.34N 648473.26E	1466	1467.85	999	6";0-960	440-940	О	380	5-9-95	Magma	.81-foot LCS casing stickup. Aquifer test performed 6/95, 8/95, 9/95.
013-0	B1		D(4-9)28cba 55-547812	746889.92N 647598.55E	1479.4	1481.48	1440	4";0-1413	770- 1,393	О	650	8-2-95	Magma	1.5-foot LCS casing stickup.

<sup>&</sup>quot;The following are other tables which correlate with wells listed in the table.

<sup>·</sup> C1, C2: Existing water quality data, Appendix C, Volume II

<sup>·</sup> B1, B2, B3: Water level data, Appendix B, Volume II

<sup>·</sup> B5, Well data included in Montgomery and Associates (1994)

<sup>&</sup>lt;sup>b</sup>Feet above mean sea level (MSL)

<sup>&</sup>lt;sup>e</sup>Feet below ground surface

<sup>\*</sup> The well ID listed first identifies the well name most commonly used with respect to documentation and well recognition. Any other names found for a particular well are also listed as a reference.

<sup>\*\*</sup> The correct well identification is based on location and is listed first followed by all other numbers referenced to that well as found in various reports and documents.

Table 2.3-2.	Summary of Information Concerning Existing Wells Within One-Half Mile of the Florence In-Situ Mine Area													
Well ID*	Well Correlation Tables*	Well Type	Location/ ADWR No.**	Location Coordinates (Northing Easting)	Land Elevation (feet) <sup>b</sup>	Reference Point Elevation (feet) <sup>b</sup>	Total Depth (feet)	Casing Diameter	Screened Interval (feet) <sup>c</sup>	Screened Zone	Top of Bedrock (feet) <sup>c</sup>	Date Installed	Well Owner	Condition/Remarks
P13.2-O	BI	Test	D(4-9)28cba 55-547810	746807.64N 647653.82E	1479.2	1480.08	1400	6";0-1380	781- 1,379	0	647	7-27-95	Magma	1.5-foot LCS casing stickup.
P13.1-O	B1	Test	D(4-9)28cba 55-547808	746799.40N 647551.22E	1478.5	1479.97	1475	6";0-1449	772- 1,449	0	770	7-16-95	Magma	1.5-foot LCS casing stickup.
P13-GL	BI	Test	D(4-9)28cba 55-547811	746802.29N 647400.14E	1477.4	1479.29	770	6";0-760	690-760	G	NA	8-11-95	Magma	1.5-foot LCS casing stickup.
015-0	B1	Monitor	D(4-9)28cca 55-549160	745437.85N 647505.19E	1467.5	1468.69	1330	4";0-1,315	632- 1,296	0	553	7-1-95	Magma	Aquifer test performed 8/95, 9/95.
P15-O	BI	Test	D(4-9)28cca 55-549158	745428.58N 647596.44E	1468	1469.32	1380	6";0-1321	580-1300	О	485	6-20-95	Magma	Aquifer test performed 8/95, 9/95.
P15-GL	B1	Test	D(4-9)28cca 55-549161	745376.92N 647508.44E	1468.6	1468.61	500	6";0-491	421-481	G	NA	7-3-95	Magma	Aquifer test performed 8/95, 9/95.
019-0	B1	Monitor	D(4-9)28bdc 55-549149	747413.63N 648397.07E	1482.7	1483.69	630	4";0-627	410-608	О	400	6-7-95	Magma	3.0-foot PVC casing stickup. Aquifer test performed 7/95, 9/95.
019-GL	B1	Monitor	D(4-9)28bdc 55-549150	747359.29N 648233.62E	1481.7	1483.28	460	5";0-455	375-435	G	NA	6-14-95	Magma	1.5-foot LCS casing stickup. Aquifer test performed 7/95, 9/95.
P19.1-O	B1	Test	D(4-9)28bdc 55-549151	747345.78N 648427.94E	1483	1484.72	. 680	6";0-621	402-600	0	355	6-4-95	Magma	2.0-foot LCS casing stickup. Aquifer test performed 7/95, 9/95.
P19.2-O	B1	Test	D(4-9)28bdc 55-549152	747350.40N 648359.48E	1482.6	1484.23	630	6";0-622	404-602	О	420	6-8-95	Magma	1.5-foot LCS casing stickup. Aquifer test performed 7/95, 9/95.
O28-GL	BI	Monitor	D(4-9)28ddb 55-547805	745592.65N 650966.70E	1464.8	1465.66	320	4";0-307	277-307	G	NA	7-4-95	Magma	1.5-foot LCS casing stickup. Aquifer test performed 8/95, 9/95.

<sup>\*</sup>The following are other tables which correlate with wells listed in the table.

<sup>·</sup> C1, C2: Existing water quality data, Appendix C, Volume II

<sup>·</sup> B1, B2, B3: Water level data, Appendix B, Volume II

<sup>·</sup> B5, Well data included in Montgomery and Associates (1994)

<sup>&</sup>lt;sup>b</sup>Feet above mean sea level (MSL)

<sup>&</sup>lt;sup>c</sup>Feet below ground surface

<sup>\*</sup> The well ID listed first identifies the well name most commonly used with respect to documentation and well recognition. Any other names found for a particular well are also listed as a reference.

<sup>\*\*</sup> The correct well identification is based on location and is listed first followed by all other numbers referenced to that well as found in various reports and documents.

Table 2.3-2.	Summary of Information Concerning Existing Wells Within One-Half Mile of the Florence In-Situ Mine Area													
Well ID*	Well Correlation Tables*	Well Type	Location/ ADWR No.**	Location Coordinates (Northing Easting)	Land Elevation (feet) <sup>b</sup>	Reference Point Elevation (feet) <sup>b</sup>	Total Depth (feet) <sup>c</sup>	Casing Diameter	Screened Interval (feet) <sup>c</sup>		Top of Bedrock (feet) <sup>c</sup>	Date Installed	Well Owner	Condition/Remarks
O28.1-O	B1	Monitor	D(4-9)28ddb 55-547803	745652.04N 651027.87E	1464.6	1465.76	530	4";0-514	395-494	0	368	6-21-95	Magma	1.5-foot LCS casing stickup. Aquifer test performed 8/95, 9/95.
O28.2-S	BI	Monitor	D(4-9)28ddb 55-547804	745621.06N 651123.95E	1464.8	1465.54	510	4";0-495	454-494	S	340	6-19-95	Magma	1.5-foot LCS casing stickup. Aquifer test performed 8/95, 9/95.
P28-GL	BI	Test	D(4-9)28ddb 55-547807	745535.76N 651085.74E	1465	1466.48	320	5";0-309	279-309	G	NA	6-30-95	Magma	1.5-foot LCS casing stickup. Aquifer test performed 8/95, 9/95.
P28.1-O	B1	Test	D(4-9)28ddb 55-547802	745558.54N 650998.31E	1464.9	1466.48	520	6";0-509	399-499	О	360	7-2-95	Magma	1.5-foot LCS casing stickup. Aquifer test performed 8/95, 9/95.
P28.2-O	B1	Test	D(4-9)28ddb 55-547806	745516.17N 651118.23E	1465.4	1466.68	519	6";0-507	398-497	О	335	6-29-95	Magma	1.5-foot LCS casing stickup. Aquifer test performed 8/95, 9/95.
O39-O	B1	Monitor	D(4-9)28bcd 55-549174	744220.52N 649098.12E	1463.1	1464.29	916	5";0-910	474-890	О	380	5-7-95	Magma	1.6-foot LCS casing stickup. Aquifer test performed 5/95.
P39-O	B1	Test	D(4-9)28bcd 55-549176	744102.51N 649102.65E	1461.7	1462.85	915	6";0-847	471-826	0	380	5-10-95	Magma	2.0-foot PVC casing stickup. Aquifer test performed 5/95.
O49-O	B1	Monitor	D(4-9)33bba 549179	744195.29N 647517.19E	1461.8	1462.69	1280	4";0-1247	832- 1227.5	0	810	6-6-95	Magma	1-foot PVC casing stickup.
O49-GL	B1	Monitor	D(4-9)33bba 55-549180	744193.98N 647477.36E	1461.2	1462.08	740	5";0-730	661-721	G	NA	6-15-95	Magma	1.1-foot PVC casing stickup.
P49-O	B1	Test	D(4-9)33bba 55-549181	744202.71N 647611.87E	1461.8	1463.12	1288	6";0-1242.5	808-1222	0	770	5-24-95	Magma	.9-foot LCS casing stickup.

<sup>&</sup>quot;The following are other tables which correlate with wells listed in the table.

<sup>·</sup> C1, C2: Existing water quality data, Appendix C, Volume II

<sup>·</sup> B1, B2, B3: Water level data, Appendix B, Volume II

<sup>·</sup> B5, Well data included in Montgomery and Associates (1994)

<sup>&</sup>lt;sup>b</sup>Feet above mean sea level (MSL)

<sup>&</sup>lt;sup>e</sup>Feet below ground surface

<sup>\*</sup> The well ID listed first identifies the well name most commonly used with respect to documentation and well recognition. Any other names found for a particular well are also listed as a reference.

<sup>\*\*</sup> The correct well identification is based on location and is listed first followed by all other numbers referenced to that well as found in various reports and documents.

Table 2.3-3 Large Municipal Water Providers, Pinal AMA, 1985					
Provider	Population Served	1985 Groundwater Use (ac- ft)	gpcd		
Arizona Sierra Utility Company	1,214	161	118		
Arizona State Prison-Florence	4,351	913	187		
Arizona Training Center	485	329	606		
Arizona Water Company					
- Casa Grande System	19,836	6,062	273		
- Coolidge System	8,174	1,350	147		
- Stanfield System	580	100	154		
Central Arizona College	839	155	165		
City of Eloy	5,867	1,259	192		
Maricopa Water Improvement District	709	241	303		
Pinal County Housing Authority	355	147	370		
Thunderbird Water Improvement District	927	112	108		
Town of Florence	2,684	809	269		

Source: ADWR (1991) ac-ft - acre-feet

gpcd - gallons per capita per day

Well Type	Number of Registered Wells	Percentage of Total Registered Wells	Annual Withdrawal Reported to ADWR (Acre- feet) 1994
Private Irrigation Within 5- mile radius	70	18.3	NR
Private Irrigation Within 1- mile radius	12	3.1	4,385
Irrigation (San Carlos Irrigation Project)	22	6.0	13,332
Municipal (Public Supply) (Town of Florence)	5	1.0	1,055
Municipal (Institutional) (Arizona State Prison)	2	0.5	1,284
Domestic	99	26.0	NR
Domestic/Irrigation	13	3.4	NR
Domestic/Stock/Irrigation	8	2.0	NR
Domestic/Industrial	1	0.3	NR
Domestic/Stock	12	3.0	NR
Domestic/Stock/Industrial	1	0.3	NR
Industrial	7	2.0	NR
Industrial/Irrigation	5	1.3	NR
Monitor	62	16.2	NR
Irrigation/Stock	3	0.9	NR
Stock	1	0.3	NR
Utility	1	0.3	NR
Utility/Recharge	2	0.5	NR
Unknown Use	55	14.4	NR
Test	1	0.3	NR .

Source: ADWR (1995) NR - Not Reported

Table 2.5-1. Explanation of the I	Following Permits	
Permit	Permit No.	Description
Resource Conservation and Recovery Act (RCRA)	AZD983481599	EPA-Exempt Small Quantity
NPDES Storm Water	AZR00A224	EPA-General Permit
Pinal County Burn	1383	Renewable every 3 months
Pinal County Air Quality	To be applied for 1996	Renewable every 5 years
Septic Tank Permits	26,500 (existing) 2-new under 2,000 gallons per day	Pinal County 2-new under APP General Permit Program
Mineral Lease	Mineral lease 11-26500	Arizona State Land Department.
UIC	To be applied for November 1995	Region IX EPA
ADWR Well Permits	Over 50 in place	Applied for as needed
Burial Agreement	A.R.S 41-865 Case No. 94-24	Arizona State Museum lead agency with Hopi Tribe, Gila River Indian Community and Magma as signatories
Programmatic Agreement required as Section 106 requirement under the UIC permit and NHPA.	In-process, sent out for signature	Region IX EPA lead agency with State Historic Preservation office, Hopi Tribe, Gila River Indian Community, Magma, Advisory Council on Historic Preservation as signatories
NPDES 404/401 Water Quality Certification	In preparation, disturbance of jurisdiction water to be less than 0.5 acres. Only a 401 Water Quality certification is required by the Corps of Engineers for the ADEQ	Army Corps of Engineers requires permit for dredge and fill of jurisdictional waters of the U.S.
Aquifer Protection	ADEQ	To protect aquifer water quality for drinking water by encouraging discharge reduction, and where practicable, by eliminating discharges to Arizona aquifers.

Table 2.	8-1. Minor UIC Aquifer Exemption Requ	Information Location	Comments
		Information Location	Comments
Α.	General Inventory Information		
1.	Facility name, address	This volume, Section 1.3	Magma Copper Company Florence Project 14605 East Hunt Highway Florence, Arizona 85232
2.	Owner name, address	This volume, Section 1.3	Magma Copper Company Suite 200 7400 North Oracle Road Tucson, Arizona 85704
3.	Operator/legal contact name, address	This volume, Section 1.3	Mr. John Kline Magma Copper Company 14605 East Hunt Highway Florence, Arizona 85232
4.	Project type (e.g., generation, transportation, treatment facility)	This volume, Section 2.4.3	In-situ copper mining.
5.	Operating status of injection well(s)	This volume, Section 3.1	None presently in operation.
6.	Listing of all permits or construction approvals	Volume, Section 2.5, Table 2.5-1	Mine not yet operational,; therefore, it has few permits.
В.	Purpose of Proposed Aquifer Exempt	tion	,
1.	Explain the purpose, need for, and intentions of the exemption, other than those listed in item B4 below.	This volume, Sections 1.1 and 2.1	The purpose of the exemption is to allow for in-situ leaching of copper, which is a primary resource mined to meet the needs of demand within the national economy.
2.	Provide a narrative description of the proposed aquifer exemption, including the proposed exempted aquifer, confining zone, boundaries, injection practices, etc. Discuss the need to inject into this zone as opposed to injecting into other zones which are not USDWs.	This volume, Section 2.1	Exemption covers area of productive orebody.
3.	A declaration that the aquifer is not now and will not in the future serve as a source of drinking water. The burden of proof is left to the applicant.	This volume, Section 1.1	The aquifer cannot now and will not in the future be used for a source of drinking water within the expected area.

Table 2.8	8-1. Minor UIC Aquifer Exemption Req	uest Information Summary	
		Information Location	Comments
4.	Reason for requesting the aquifer exemption. The reason must include either (a) and (b), or (a) and (c) below:		Request for aquifer exemption for reason (a) and (b).
	a. The aquifer does not currently serve as a source of drinking water.	This volume, Section 1.0	The aquifer does not now serve as a source of drinking water.
	b. The aquifer cannot now and will not in the future serve as a source of drinking water because:	·	
	(i) The aquifer is mineral, hydrocarbon or geothermal energy producing, or can be demonstrated by a permit applicant as part of a permit application for a Class II or III operation to contain minerals or hydrocarbons that, considering their quantity and location, are expected to be commercially producible.	This volume, Section 1.0	Magma has shown through its submission of Appendix A of this volume that commercially producible quantities of copper can be produced.
	(ii) The aquifer is situated at a depth or location which makes recovery of water for drinking water purposed economically or technologically impractical (a detailed economic analysis is required).		Justification for B-4-b-i included.
	(iii) The aquifer is so contaminated that it would be economically or technologically impractical to render that water fit for human consumption (a detailed economic analysis is required).		Justification for B-4-b-i included.

Table 2.8-1	1. Minor UIC Aquifer Exemption Requ	est Information Summary	
		Information Location	Comments
	(iv) The aquifer is located over a Class III well mining area subject to subsidence or catastrophic collapse.	Not applicable	Justification for B-4-b-i included.
	c. The total dissolved solids content of the groundwater is more than 3,000, and less than 10,000 mg/L and it is not reasonably expected to supply a public water system.	Not applicable	Justification for exemption under (a) and (b).
•	An estimate of the time duration of the proposed aquifer exemption.	This volume, Section 1.2	Mine life estimated at 15 years followed by 30-year post-closure period.
	An analysis of alternatives to the proposed underground injection project for disposal of the wastes.	This volume, Section 2.7	No underground disposal of wastes. In-situ mining produces minimal waste volume in comparison to conventional mining.
	An analysis of the environmental impacts of the proposed aquifer exemption, including any adverse environmental effects which cannot be avoided; any irreversible or irretrievable commitments of resources which would be involved should the exemption be approved; the relationship between short-term uses of the aquifer for waste disposal purpose; and the long-term benefits of maintaining the present aquifer conditions.	This volume, Section 2.7	There are no irreversible or irretrievable commitments of resource. Area will be returned to levels that does not exceed any primary MCLs.
only for must des Addition injection wastewal	EPA will approve aquifer exemptions specific purposes. Any exemption request cribe the injection activities to be allowed. al approvals shall be required for other activities (e.g., non-hazardous industrial ter disposal into an aquifer exempted for production).	This volume I, Sections 1.1 and 2.0	Injection and recovery wells are proposed specifically for the economic recovery of copper from the mineralized zone.

Table 2.8-1. Minor UIC Aquifer Exemption Requ	est Information Summary	
	Information Location	Comments
Item B-4-a: At a minimum, a survey should be conducted to identify all water supply wells in the area of the proposed exempted aquifer and the buffer zone. If no water supply wells would be affected by the exemption, the request should state that a survey was conducted and no water supply wells were located which will be affected by the proposed exemption. If the proposed aquifer exemption pertains to only a portion of an aquifer, a demonstration must be made that the waste will remain within the exempted portion of the aquifer.	This volume, Section 1.1.11, and Volume IV	All water wells in a 100-square mile area surveyed including exemption request zone and buffer zone. No water supply wells outside Magma's control will be affected by proposed exemptions. Modeling techniques described in Volume IV indicate that contaminant levels above background concentrations will remain within exempted portion of aquifer.
Item B-4-b-i: The applicant for an aquifer exemption is required to furnish the data necessary to demonstrate that the aquifer is expected to be mineral or hydrocarbon producing. If the proposed aquifer exemption is to allow a Class II enhanced oil recovery well or an existing Class III injection well operation to continue, the fact that the aquifer has a history of hydrocarbon or mineral production will be sufficient proof that this standard has been met. Applicants for aquifer exemption to allow new mining must demonstrate that the aquifer is expected to contain commercially producible quantities of minerals.		The economic justification indicate that copper can be produced at an economically justifiable level. Supporting data is submitted Appendix A and marked "Confidential Business Information" as specified under 40 C.F.R. 144.5.

Table 2.8-1. Minor UIC Aquifer Exemption Requ	est Information Summary	
	Information Location	Comments
Information contained in the mining plan for the proposed project, such as a map and general description of the mining area, general information on the mineralogy and geochemistry of the mining zone, analysis of the amenability of the mining zone to the proposed mining method, and a timetable of planned development of the mining zone, shall be required. An analysis of a sample acquired using a formation tester or coring tool shall be required to show that the aquifer contains producible levels of minerals. This should be coupled with reserve calculations and rate of return projections for the aquifer in question. Exemptions relating to any new Class II wells which will be injecting into a producing or previously produced horizon shall include the following types of information: the production history of the well if it is a former production well which is being converted; a description of any drill stem test run on the horizon in question; the production history of other wells in the vicinity which produce from the horizon in question; and a description of the project if it is an enhanced recovery operation, including the number of wells and their location.	This volume, Section 1.0 and Appendix A. Also, Volume II, Sections 1.3, 2.3, 3.8, 4.3, 4.5, and 4.7	Intend to mine orebody using in-situ/SX/EW mining techniques. Operations are intended to commence operations late 1997 and continue for approximately 15 years.
Structural contour maps and cross sections for the zone of injection, along with any available radioactive tracer surveys, would infer if the injection is going to be into a geothermal producing aquifer where steam is produced underground and at the surface.	Volume II, Figure 3.4-6 Volume II, Figure 4.3-5 Volume II, Figure 4.3-6 Volume II, Figure 4.3-1 through 4	Structural contour and cross-section maps

Table 2.8-1. Minor UIC Aquifer Exemption Requ	Table 2.8-1. Minor UIC Aquifer Exemption Request Information Summary					
	Information Location	Comments				
Item B-4-b-ii: An economic analysis coupled with technological considerations is required from the applicant to determine if the aquifer's water could be economically pump to the surface and used as a source of water supply. Specifically, the applicant shall calculate the optimum annual yield of the aquifer and the net present value associated with the development and operation of the aquifer as a water supply source. The optimum annual yield shall be determined by identifying the location of groundwater well which would maximize the water output without dangerous depletion of the storage reserve of the aquifer. The net present value shall be determined by identifying all capital and operating costs associated with the water project and discounting these costs over the life of the project. See Section H below for additional details on economic evaluation of water supply development costs.	Not applicable					
Item B-4-iii: An economic analysis coupled with technological considerations is required to determine if the aquifer's water could be economically pumped to the surface and made fit for human consumption. See Section I below for additional details on economic evaluation of water supply treatment technology and costs.	Not applicable					
Item B-4-b-iv: The aquifer exemption request should discuss the proposed mining method and why the method necessarily causes subsidence or collapse. The possibility that non-exempted USDWs would be contaminated due to the collapse should also be addressed in the application. Structural contour maps and cross sections, pore pressure information from drilling, and mud logs for both the aquifer and the zone being mined are required.	Not applicable					

Table 2.8-	Table 2.8-1. Minor UIC Aquifer Exemption Request Information Summary				
		Information Location	Comments		
Item B-4-c: The aquifer exemption request must include information about the equality and availability of water from the proposed exempted aquifer. Also, the exemption request must analyze the potential for public water supply use of the aquifer. Details required for this analysis are outlined in Section M below.		Not applicable			
C.	Maps of Area of Proposed Aquifer Exemp	tion			
1.	Base map of area (USGS topographic map with a scale of 1:24,000 or larger; maps should extend a minimum of 1 mile beyond the proposed aquifer exemption boundaries; more than one map may be needed). The map should:	This volume, Sheet 2.1-1			
	a. precisely depict, in square miles or acres, the area overlying the proposed exempted aquifer, or portion of the aquifer, both on the map and in some universal unit (e.g., latitude/longitude, distances, bearing);	This volume, Sheet 2.1-1	33° 02' 00" North 111° 25' 00" West		
	b. delineate in square miles or acres the boundaries of the aquifer, both on the map and in some universal unit, e.g. latitude/longitude, distances, bearing (note: this area will be larger than that in Item a. above if only a portion of the aquifer is being requested for exemption);	Volume II, Section 3.0, Figures 3.6-1(II), 3.6-2(II), and 3.6-3(II)	The Pinal Active Management area is approximately 1,100 square miles in Central Arizona. (Wickham and Corkhill, 1989)		
	c. delineate the boundaries of any existing or proposed aquifer exemptions both on the map and in some universal unit (e.g., latitude/longitude, distances, bearing);	This volume, Sheet 2.1-1	Latitude and Longitude 33° 02' 00" North 111° 25' 00" West		

Table 2.8-1.	Minor UIC Aquifer Exemption Requ	est Information Summary	
		Information Location	Comments
d	show a "buffer zone" around the area of the proposed exempted aquifer (this buffer zone should be an area of limited future ground water development extending a minimum of 1/4 mile from the boundary of the proposed exempted aquifer);	This volume, Sheet 2.1-1	Point of Compliance (POC) groundwater quality monitoring well array.
е	show the location of all monitoring wells completed, or to be completed, in the buffer zone to assure that injected fluids do not migrate from the exempted aquifer; and delineate the boundaries of all property owners and holders of water rights within the area of the proposed exempted aquifer and buffer zone for the purpose of public notification (include a list of names and mailing addresses).	This volume, Figure 2.1-2	Planned and existing POC wells have been established downgradient of the proposed mine area.
a b a	Copographic map showing all wells in the rea of the proposed exempted aquifer and uffer zone (same scale as above) with eccompanying explanation or table to include:	Volume II, Figure 2.1-2(II) See tables in Volume II, Appendix B.	Appendix B contains existing well and water level data.
a	. well identification (name and number)	Volume II, Section 2.3, Table 2.3-3 This volume, Table 2.3-2	ADWR registration number
b	<ul> <li>well type (e.g., production, injection, irrigation, water supply, enhanced recovery, monitoring abandoned, dry holes)</li> </ul>	Volume II, Section 2.1, Figure 2.1-2(II), Section 2.3, Table 2.3-3	Wells include monitoring aquifer test pumping and observation wells, and irrigation wells.
С	. well depth	Volume II, Section 2.3, Table 2.3-3	Range 200 to 1,600 feet below ground surface.
d	status (e.g., active, inactive, plugged, abandoned)	Volume II, Section 2.3, Table 2.3-3 Active but not involved in-situ mining	All wells are active, abandonment plans for existing and planned wells have been established as part of the mining plan.
e	date drilled and dates of significant workovers	No mining wells in area.	

Table 2.8	3-1.	Minor UIC Aquifer Exemption Requ	est Information Summary	
			Information Location	Comments
	f.	construction information (including cement, casing, tubing, completion type, and plugging records)	Volume II, Section 5.2.3, Table 2.3-3 Volume II, Appendix A	
	g.	perforated interval	Volume II, Section 2.3, Table 2.3-3	Well ore perforated in water bearing stratigraphic units include UBFU, LBFU, oxider sulfide bedrock zones.
	h.	location (township, range, section)	This volume, Section 3.1, UIC Form 4	Located in Township 4 South, Range 9 East, Section 22, 28 and 33, 34.
	i.	corrective/remedial action for improperly plugged wells	Not applicable	
	j.	history of injection operations (existing wells only)	Not applicable	-Mbc.
3.	dom with num aqui	estic and public water supply wells tables of relevant information such as ber of users, depth of water wells with fer names, and water quality rmation.	This volume, Sheet 2.1-1	Presently 382 registered wells within a 5-mile radius of the proposed in-situ mine area.
D.	Maj	os and Cross Sections of USDWs		
1.		logic cross sections (two perpendicular ions) showing:	Volume II, Section 3.4, Figures 3.4-2(II) and 3.4-3(II) Volume II, Section 4.3, Figures 4.3-1(II), 4.3-2(II), 4.3-3(II), and 4.3-4(II)	Section 3.4 figures regional cross sections Section 4.3 figures are in-situ mine area cross sections.
	a.	geologic formations	Volume II, Section 3.4, Figures 3.4-2(II) and 3.4-3(II) Volume II, Section 4.3, Figures 4.3-1(II), 4.3-2(II), 4.3-3(II), and 4.3-4(II)	Section 3.4 figures regional cross sections. Section 4.3 figures are in-situ mine area cross sections.
	b.	structural features	Volume II, Section 3.4, Figures 3.4-2(II) and 3.4-3(II) Volume II, Section 4.3, Figures 4.3-1(II), 4.3-2(II), 4.3-3(II), and 4.3-4(II)	Section 3.4 figures regional cross section. Section 4.3 figures are in-situ mine area cross sections.
	c.	TDS levels for each formation	Volume II, Sections 3.8 and 4.5, Figure 4.5-2(II) Volume III, Appendix D	Range 790 to 1,400 mg/L.
	d.	underground sources of drinking water	Not applicable	•
	e.	proposed exempted aquifer	This volume, Sheet 2.1-1	
	f.	confining zone	Not applicable	

	ole 2.8-1. Minor UIC Aquifer Exemption Request Information Summary  Information Location Comments			
	(0)	Intol mation Location		
2.	Isopach maps (2)  a. proposed exempted aquifer	Volume II, Section 4.3, Figures 4.3-9(II), 4.3-10(II), 4.3-11(II), and 4.3-12(II)		
	b. injection zone	Volume II, Section 4.3	Oxide bedrock zone	
E.	Maps and Cross Sections of Geologic Structure of Area	·		
1.	Geologic maps			
	a. local area	Volume II, Section 2.1, Figure 2.1-1(II)		
	b. regional setting	Volume II, Section 3.4, Figure 3.4-1(II)		
2.	Structural contour map (mapped to top of proposed exempted aquifer)	Volume II, Section 3.4, Figure 4.3-8(II) Volume II, Section 4.3, Figures 4.3-5(II) and 4.3-6(II)		
3.	Stratigraphic column (local area)	Volume II, Section 3.4, Figure 3.4-5(II)		
	a. lithology of each formation	Volume II, Sections 3.7 and 4.3.1		
	b. mineralogy of proposed exempted aquifer and confining zones	Volume II, Section 4.3.2		
	c. thickness of each formation	Volume II, Section 4.3.2		
	d. hydraulic conductivity/permeability of proposed exempted aquifer and confining zones	Volume II, Sections 3.7 and 4.3.2		
	e. salinity profile (TDS)	Volume II, Section 4.5, Figure 4.5-2(II)		
	f. 10,000 mg/L TDS baseline (freshwater baseline)	Volume II, Section 4.5, Figure 4.5-2(II)		
	g. geologic time scale	Volume II, Section 3.4, Figure 3.4-5(II)		
4.	Stratigraphic column (regional setting)	Volume II, Section 3.4, Figure 3.4-5(II)		
5.	Regional geology (narrative description)	Volume II, Section 3.4		
	a. regional structural geology	Volume II, Section 3.4		
	b. regional stratigraphy	Volume II, Section 3.4		
	c. seismic activity	Volume II, Section 3.5.2		
	d. tectonic history	Volume II, Section 3.4		

Table 2.	Table 2.8-1. Minor UIC Aquifer Exemption Request Information Summary				
		Information Location	Comments		
F.	Operating Data and Injection Procedures	This volume, Section 2.4			
1.	Injection rate (average, maximum)	APP Volume I, Sections 4.2.1 and 4.5.2	Range 0.1 to 0.2 gallons per linear foot of injection on screen not to exceed fracture gradient pressure		
2.	Injection pressure (average, maximum)	APP Volume I, Sections 4.2.1 and 4.5.2	Less than 75 psi		
3.	Annular fluid (type, volume, additives, pressure, density/specific gravity)	Not applicable .	Due to design of well		
4.	Proposed injection procedures	APP Volume I, Section 4.5.2.1			
5.	Injection fluid characteristics	APP Volume I, Section 4.3			
	a. narrative description of individual waste streams	APP Volume I, Section 4.3	Minimal waste produced by in-situ mining		
	b. mix ratio (average, maximum, daily) of waste streams (if applicable)	Not applicable			
	c. RCRA waste characterization (for hazardous wastes refer to 40 C.F.R. 261 subparts C and D)	Not applicable			
	d. cumulative analysis of commingled injectate (if applicable)	Not applicable			
	e. detailed description of sampling and analytical methods	Not applicable			
	f. analysis of chemical, physical, radiological and biological characteristics, including temperature, pH, density, and corrosiveness	Volume V, Appendix F	See MSDS sheets		
	g. compatibility of waste stream(s) with receiving formation, well components, and other waste streams	Not applicable			
6.	Source of water (e.g., produced, facility supply well, municipal supply)	Volume II, Sections 3.9 and 4.6	Facility supply well.		

Table 2.	8-1. Minor UIC Aquifer Exemption Requ	est Information Summary	
		Information Location	Comments
G.	Formation Testing Program		
1.	Analysis of representative formation water sample (analysis of formation fluid to be conducted by an independent laboratory; analysis must address EPA Drinking Water Standards, i.e., MCLs and TDS at a minimum)	Volume II, Sections 3.8 and 4.5	
2.	Description of sampling and analytical procedures	Volume II, Section 2.3.4 Volume III	
3.	Direction and rate of regional groundwater flow	Volume II, Section 3.7, Volume IV	
4.	Direction and rate of injected fluid migration	Volume IV	
5.	Salinity (TDS) profiles (include all calculation procedures and logs)	Volume II, Section 3.8.3	
6.	Results of, or proposed, injectivity testing	Volume II, Section 4.3.2,5	
7.	Hydrogeology of confining zone	Volume II	Discusses no confining zone
	a. thickness		
	b. age		
	c. lithology		
	d. mineralogy (if available)		
	e. structure (presence of faults, fractures, or cavities)	Not applicable	No confining zone
	f. description of vertical and lateral continuity (e.g., depositional environment, facies changes, unconformities, and vertical and lateral extent of clay layers)	Not applicable .	No confining zone
	g. hydrologic parameters	Not applicable	No confining zone
	(i) hydraulic conductivity or permeability	Not applicable	No confining zone
	(ii) porosity	Not applicable	No confining zone

			Information Location	Comments
	(iii	oil/water saturation	Not applicable	No confining zone
	(iv	<u> </u>	Not applicable	No confining zone
	(v)		Not applicable	No confining zone
h	ı. po	tentiometric surface map	Not applicable	No confining zone
	Hydroge quifer	ology of proposed exempted	Volume II, Section 4.0	
a	. thi	ckness	Volume II, Section 4.3.3	
b	o. ag	е	Volume II, Section 4.3.3	
c	. lit	hology	Volume II, Section 4.3.3	
d	l. mi	neralogy (if available)	Volume II, Section 4.3.3	
е		ucture (presence of faults, fractures, cavities)	Volume II, Section 4.3.3	
f	co en un	scription of vertical and lateral ntinuity (e.g., depositional vironment, facies changes, conformities, presence of clay yers/lenses)	Volume II, Section 4.3.3	
g	g. hy	drologic parameters	Volume II, Section 4.3	
	(i)	hydraulic conductivity or permeability	Volume II, Section 4.3	
	(ii	) porosity	Volume II, Section 4.3	
	(ii	i) reservoir pressure	Volume II, Section 4.3	
	(iv	y) storage coefficient	Volume II, Section 4.3	
	(v	oil/water saturation	Not applicable	
	(v	i) compressibility	Volume II, Section 4.3	
	(v	ii) formation fracture pressure, from testing or calculations	Volume II, Section 4.3	
ŀ	n. po	otentiometric surface map	Volume II, Section 4.3, Figures 4.3-9(II), 4.3-10(II), 4.3-11(II), and 4.3-12(II)	

Table 2.	Table 2.8-1. Minor UIC Aquifer Exemption Request Information Summary			
		Information Location	Comments	
Н.	Technological and Economic Analysis of Aquifer Development as Water Supply	Not applicable		
	Technological and economic evaluations shall consider the availability of alternative supplies of water, the adequacy of alternative sources to meet present and future water needs, and a demonstration that there are major costs for treatment and/or development associated with the use of the aquifer as a source of water supply. The evaluation shall consider the above factors and the following:	·	·	
	Distance from the proposed exempted aquifer to public water supplies.	Not applicable		
	<ol> <li>Current sources of water supply for potential users of the proposed exempted aquifer.</li> </ol>	Not applicable		
	3. Availability and quality of alternative water supply sources.	Not applicable		
	4. Analysis of future water supply needs within the general area.	Not applicable		
	<ol> <li>Depth of the proposed exempted aquifer.</li> </ol>	Not applicable		
	<ol> <li>Quality of the water in the proposed exempted aquifer.</li> </ol>	Not applicable		
	7. The costs to develop the proposed exempted aquifer as a water supply source, including any treatment costs and costs to develop alternative water supplies. This should also include costs of well construction, transportation, water treatment, etcetera, for each source.	Not applicable		

Table 2.8	able 2.8-1. Minor UIC Aquifer Exemption Request Information Summary			
		Information Location	Comments	
I.	Technological and Economic Analysis of Aquifer Water Treatment	Not applicable		
consiconta the avadeque future are massoc water	nological and economic evaluations shall der the source, type, and severity of mination in the proposed exempted aquifer, vailability of alternative supplies of water, the lacy of alternative sources to meet present and e water needs, and a demonstration that there lajor costs for treatment and/or development lated with the use of the aquifer as a source of supply. The evaluation shall consider the e factors and the following:	Not applicable		
1.	Concentration and types of contaminants in the aquifer.	Not applicable		
2.	Source of contamination.	Not applicable		
3.	Whether the contamination source has been abated.	Not applicable		
4.	Extent of the contaminated area.	Not applicable		
5.	Probability that the contaminant plume will pass the proposed exempted area.	Not applicable		
6.	Availability of treatment technology to remove contaminants from the water.	Not applicable		
7.	Chemical content of proposed injection fluids.	Not applicable		
8.	Current water supply in the area.	Not applicable		
9.	Alternative water supplies.	Not applicable		
10.	Costs to develop current and probable future water supply from proposed exempted aquifer. This should include well construction costs, transportation costs, water treatment costs, etcetera.	Not applicable	,	

Table 2.8-1. Minor UIC Aquifer Exemption Request Information Summary				
	Information Location Comments			
11. Projections on future use of the proposed exempted aquifer.	Not applicable			

mg/L - milligrams per liter

psi - pounds per square inch

EPA - Environmental Protection Agency

MCLs - Maximum Contaminant Level

SX/EW - Solution Extraction/Electrowinning

UBFU - Upper Basin-Fill Unit

LBFU - Lower Basin-Fill Unit

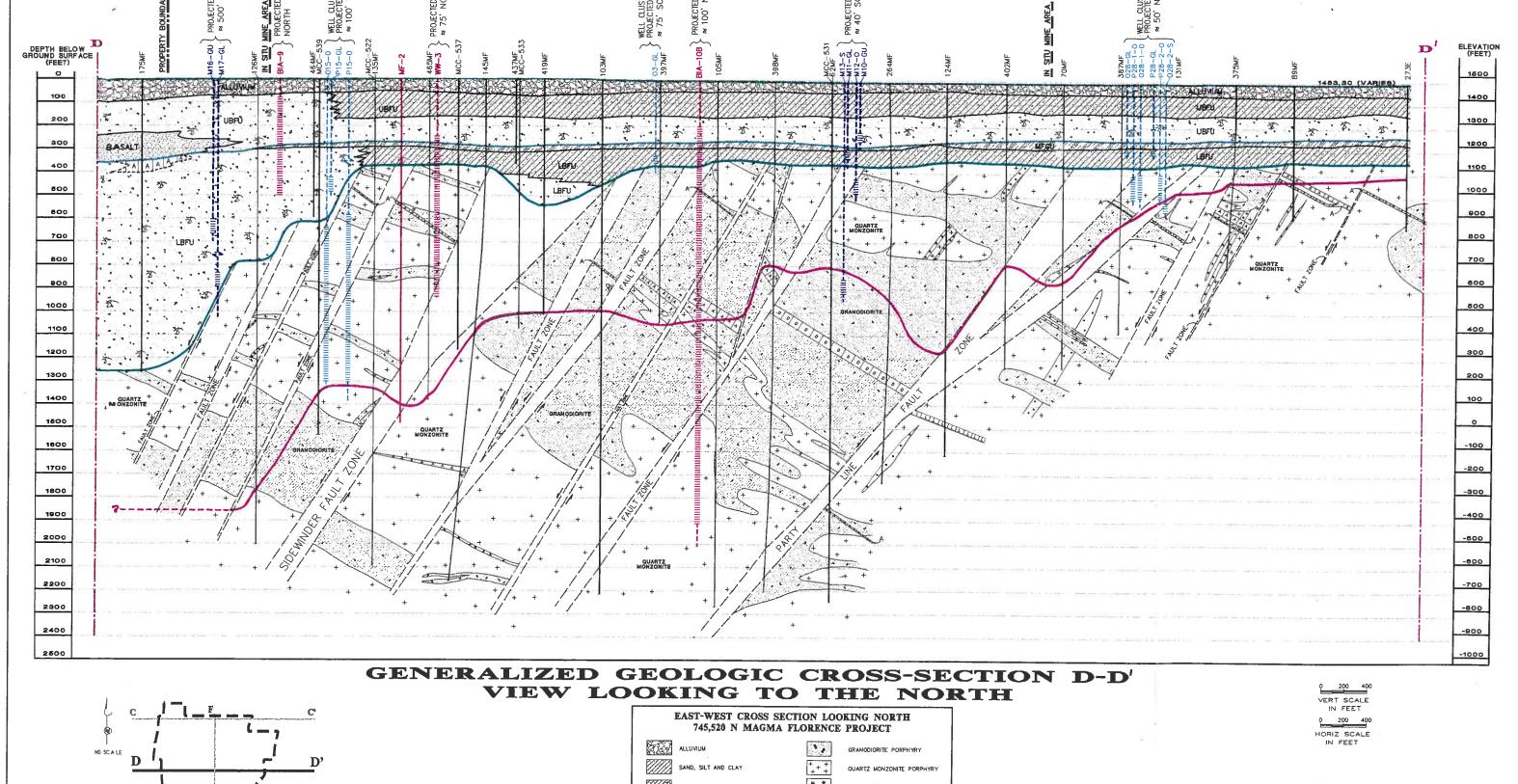
USDW - Underground Source of Drinking Water

TDS - Total Dissolved Solids

RCRA - Resource Conservation and Recovery Act

USGS - United States Geologic Survey

NA - Not applicable



PROPOSED IN-SITU MINE AREA

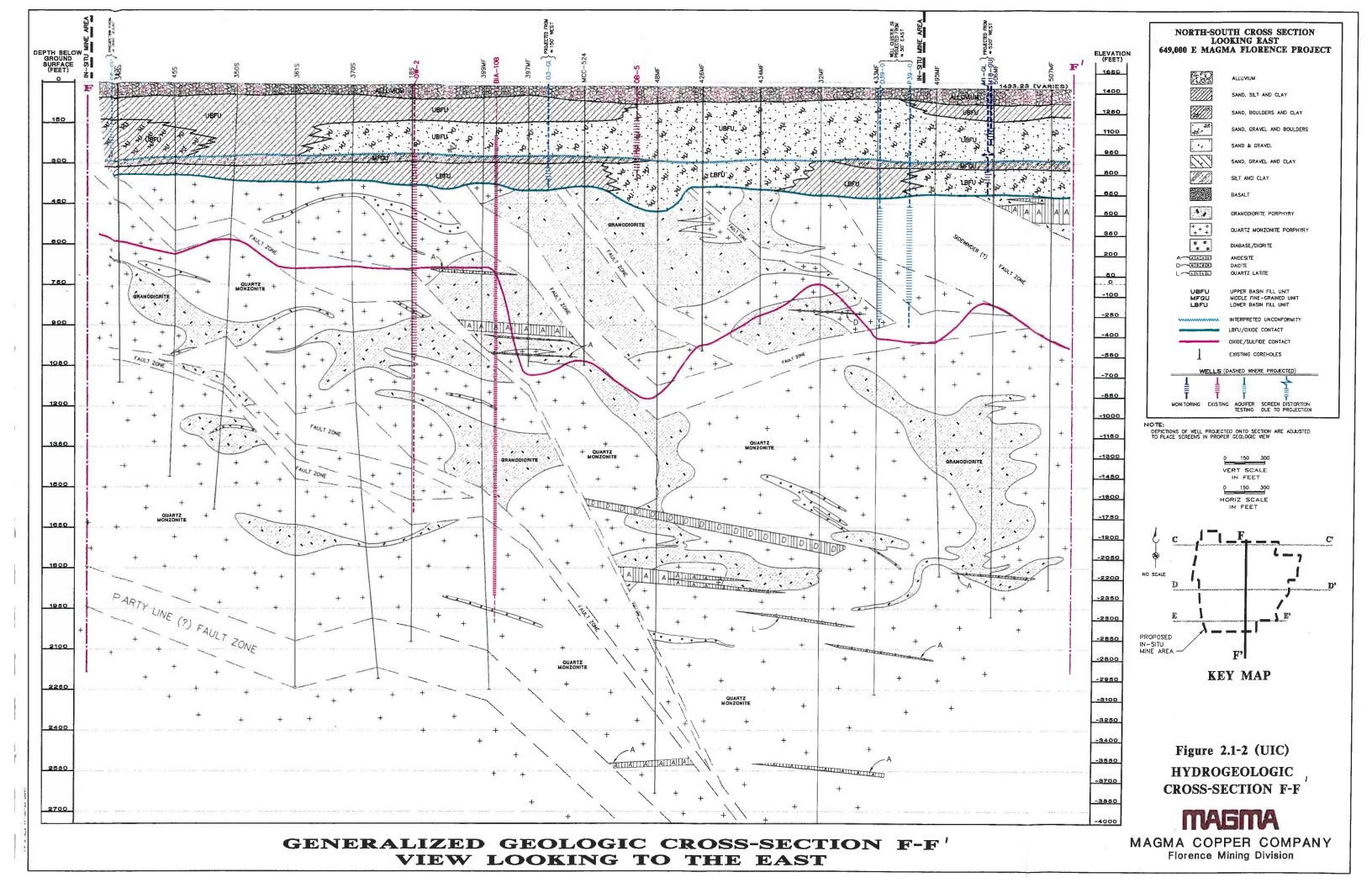
**KEY MAP** 

SAND, BOULDERS AND CLAY ANDESITE QUARTZ LATITE SAND & GRAVEL BASIN FILL UNCONFORMIT OXIDE/SULFIDE CONTACT EXISTING COREHOLES SILT AND CLAY UBFU UPPER BASIN FILL UNIT
MFGU MIDDLE FINE-GRAINED UNIT MONITORING EXISTING AQUIFER SCREEN DISTORTION TESTING DUE TO PROJECTION

Figure 2.1-1 (UIC) HYDROGEOLOGIC CROSS-SECTION D-D'

MAGMA COPPER COMPANY Florence Mining Division

DEPICTIONS OF WELL PROJECTED ONTO SECTION ARE ADJUSTED TO PLACE SCREENS IN PROPER GEOLOGIC VIEW



Original enclosed map Figure 2.2-1 included information about protected archeological sites.

EPA has removed this map because it is related to the NHPA records.

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#### **SECTION 3.0**

# UNDERGROUND INJECTION CONTROL (UIC) PERMIT APPLICATION FORM 4

#### 3.1 FORM 4

A completed and signed Form 4 is presented on the next page.

#### 3.2 FORM 4 CHECKLIST

A checklist and cross-reference is provided in Table 3.2-1 to assist the review in locating information required under Item XI of Form 4.

		INDEBUB!	CINTO IN TEACH	ROTECTION AGENC	Y 11	EPA ID NUMB			
4 8	EPA	PER	MIT APPLICA	ATION	H	AZD98348			
UIC		(Collected und	der the authority of t Sections 1421, 142	he Sefe Drinking	U	(Exempt	small qu	uantity	1
			ATTACHED INSTRU	CTIONS BEFORE ST	ARTING				L
Application appraise				AL USE ONLY					بعدا
	or me dey ye	per Permit/	Well Number			Comment	8		-
I. FACILITY NA	ME AND ADDRESS	6							
Facility Name						D ADDRESS		44. MA	
Street Address		ence Project		Owner/Operator		lagma Copj	per Comp	any	
		Hunt Highway		Street Address	7	400 Oraci	le Road		_
City	Florence	State AZ	<b>ZIP Code</b> 85322	City			State	ZIP Code	
V, OWNERSHIP	P STATUS (Mark 'x'		*i:100022	V. SIC CODES		ucson	AZ	85704	
JA Federal	☐ S. State	C. Private							
D. Public			•	1021					
I. WELL STATE	US (Mart: 'x')		na Tarini na mana a						
JA	Date Started								
Operating	mo day yes	B. MOGRICA	tion/Conversion	C. Proposed					
II. TYPE OF PE	RMIT REQUESTED	(Mark 'x' and specif	ty if required)		min	i - Maria		and the same of the same of	4.00
A. Individual		Number of Exist- ing wells NO	- Number of Pro-	Name(s) of field(s) of	or project(s				
		UIC wells	approx. 3,	000					
III. CLASS AND A. Class(se)	TYPE OF WELL (S	ee reverse)				Section 2		A	, <u>L</u>
A. Liass(es) Inter code(s))	8. Type(s) (enter code(s))	C. IT CIBES IS "OU	her" or type is code "			r of wells per			
III	G		•		2 00	O Thema C			
LOCATION O	I IF WELLIS) OR APP	PROXIMATE CENTER	R OF FIELD OR PRO	IECT CONTRACTOR		0 Type G			
A. Latitude	B. Longitud	de Township at	nd Range			X. INDIAN L	ANDS (Merk	'x')	1
~~   ~~   .	Sec   Deg   Min   100   111   25   1	Sec Twee Range 00 45 9E	Sec 16 Sec Feet for 28 with port	om Line Feet fro ions of adjoi	m Line	☐ Yes ections	₽ No		
. ATTACHMEN		Nadice market		AB COMPANY	-				10
(Complete	the following (	questions on a s	eparate sheet(s)	and number acc	ordinaly	r saa inetri	ictione)		a A
FUR CLAS	55ES I, II, III (and	d other classes)	complete and eu	hmit on conserve				(pp 2-6) a	8
your appli	· · · · · · · · · · · · · · · · · ·	- minera tadnite	u. List strechme	nts by letter whi	ch are a	pplicable ar	nd are incl	uded with	h
	ON SECONO	The state of the last	The state of the second						
									75
CERTIFICATION I	under the pi	enalty of law	that I have n	arconally ava	:		<i>-</i> - · · · ·	***	
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TABLES

Table 3.2-1. Form 4 - Underground Injection Con	Table 3.2-1. Form 4 - Underground Injection Control (UIC) Permit Application - Information Summary			
Information Requirement	Information Location	Comments		
I. Environmental Protection Agency (EPA) Identification Number		RCRA-AZD983481599 EPA - Exempt Small Quantity		
Fill in your EPA Identification Number. If you do not have a number, leave blank.		UIC - In progress Region IX EPA		
II. Facility Name and Address  Name of well, well field or company and address.	This volume, Section 1.3	Magma Florence Project 14605 East Hunt Highway Florence, Arizona 85232		
III. Owner/Operator Name and Address  Name and address of owner/operator of well or well field.	This volume, Section 1.3	Magma Copper Company 7400 Oracle Road, Suite 200 Tucson, Arizona 85704		
IV. Ownership Status  Mark the appropriate box to indicate the type of ownership.	This volume, Section 1.3	C. Private		
V. Standard Industrial Classification (SIC) Code  List at least one and no more than four SIC Codes that best describe the nature of the business in order of priority.	UIC Form 4	SIC Code 1021		
VI. Well Status  Mark Box A if the well(s) were operating as injection wells on the effective date of the UIC Program for the State. Mark Box B if the well(s) existed on the effective date of the UIC Program for the State but were not utilized for injection. Box C should be marked if the application is for an underground injection project not constructed or not completed by the effective date of the UIC Program for the State.	UIC Form 4	C. Proposed		

Table 3.2-1. Form 4 - Underground Injection Cor	Form 4 - Underground Injection Control (UIC) Permit Application - Information Summary			
Information Requirement	Information Location	Comments		
VII. Type of Permit	This volume, UIC Form 4, Section 3.2	B. Area Permit Approximately 3,000 proposed wells		
Mark "Individual" or "Area" to indicate the type of permit	·	Magma Florence Project		
desired. Note that area permits are at the discretion of the Director and that wells covered by an area permit must be at				
one site, under the control of one person and do not inject	·			
hazardous waste. IF an area permit is requested the number				
of wells to be included in the permit must be specified and				
the wells described and identified by location. If the area has				
a commonly used name, such as the "Jay Field", submit the name in the space provided. In the case of a project or field				
which crosses State lines, it may be possible to consider an				
area permit if EPA has jurisdiction in both States. Each such				
case will be considered individually, if the owner/operator				
elects to seek an area permit.				
VIII. Class and Type of Well	This volume, UIC Form 4, Section 3.2	Class III, Type G (solution mining well)		
Enter in these two positions the class and type of injection				
well for which a permit is requested. Use the most pertinent				
code selected from the list on the reverse side of Form 4.  When selecting type X, please explain in the space provided.				
	This volume, UIC Form 4, Section 3.2	Township 4 South, Range 9 East, Sections 27, 28, 33 and 34		
IX. Location of Well	This volume, OIC Form 4, Section 5.2	Latitude 33° 02' 00" North		
Enter the latitude and longitude of the existing or proposed		Longitude 111° 25' 00" West		
well expressed in degrees, minutes, and seconds or the		(Center of Magma Florence Project)		
location by township, and range, and section, as required by				
40 C.R.F. 146. If an area permit is being requested, give the latitude and longitude of the approximate center of the area.				
X. Indian Lands	This volume, UIC Form 4, Section 3.2	No part of the facility is located on Indian lands.		
A. Indian Lands	Time volume, OTC FORM 4, equipment 3.2	No part of the facility is focated off filtrain failus.		
Place an "X" in the box if any part of the facility is located				
on Indian lands.				

Form 4 - Underground Injection Control (UIC) Permit Application - Information Summary			
Information Requirement	Information Location	Comments	
XI. Attachments  Note that information requirements vary depending on the injection well class and status. Attachments for Class I, II, and III are described on pages 4 and 5 of this document and listed by Class on page 2. Place EPA ID number in the		,	
upper right hand corner of each page.  A. Area of Review Methods	UIC Volume I, Table B; maps showing area provided	The area of review includes a 100-square mile area surrounding the	
Give the methods and, if appropriate, the calculations used to determine the size of the area of review (fixed radius or equation). The area of review shall be a fixed radius of 1/4 mile from the well bore unless the use of an equation is approved in advance by the Director.	in Volumes II, IV, and V	proposed in-situ mine area. The in-situ area permit covers the 214 acres of the study area, with focus on impacts on the proposed aquifer exemption area. Since this is an area permit submission, the study area incorporates all of the areas within the proposed aquifer exemption. Models presented in APP Volume IV indicate no impact outside exemption area.	
B. Maps of Wells/Area and Area Review	This volume, Sheet 2.1-1	Proposed system monitoring points	
Submit a topographic map, extending 1 mile beyond the property boundaries, showing the injection well(s) or project area for which a permit is sought and the	Maps, Volume II Sheet 1.2-2 (II) Maps Volume II, Sheet 3.6-1 (II)	Wells within 1/4 mile of project, including pubic water systems	
applicable area of review. The map must show all intake and discharge structures and all hazardous waste, treatment, storage, or disposal facilities. If the application is for an area permit, the map should show the distribution manifold (if applicable) applying injection fluid to all wells in the area, including all system monitoring points. Within the area of review, the map must show the following:	Volume V, Section 1.0 Volume V, Appendix A	Operational components, including structures, treatment areas, storage areas and distribution elements. (Exact production well locations to be within proposed in-situ mine area.)  There are no intake or discharge structures, nor are there any TSDF in the area.	

Information Requirement	Information Location	Comments		
Class I				
The number, or name, and location of all producing wells, injection wells, abandoned wells, dry holes, surface bodies of water, springs, mines (surface and subsurface), quarries, and other pertinent surface features, including residences and roads, and faults, if known or suspected. In addition, the map must identify those wells, springs, other surface water bodies, and drinking water wells located with 1/4 mile of the facility property boundary. Only information of public record is required to be included on this map;	NA			
Class II				
In addition to requirements for Class I, include pertinent information known to the applicant. This requirement does not apply to existing Class II wells;	NA			
Class III				
In addition to requirements for Class I, include public water systems and pertinent information known to the applicant.	Refer to heading XI B.			
<ul> <li>a) Producing wells, injection wells, abandoned wells, dry holes.</li> </ul>		a. None of these wells.		
b) Surface bodies of water springs.		b. None.		
c) Mines.		c. Approximately 1.25 miles of underground drifts with 400 coreholes.		
d) Map of roads, etcetera.	Volume II, Figure 3.3-1			
C. Corrective Action Plan and Well Data  Submit a tabulation of data reasonably available form public records or otherwise known to the applicant on all wells within the area of review, including those on the map required in B, which penetrate the proposed injection zone. Such data shall include the following:	Volume II, Appendix B Sheet 2.1-2 (UIC) Volume V, Appendix E	Well location of corehole for 5-mile radius  Well and corehole abandonment plan		

Table 3.2-1.         Form 4 - Underground Injection Control (UIC) Permit Application - Information Summary			
Information Requirement	Information Location	Comments	
Class I			
A description of each well's type, construction, date drilled, location, depth, record of plugging and/or completion, and any additional information the Director may require. In the case of new injection wells, include the corrective action proposed to be taken by the applicant under 40 C.F.R. 144.55.	. NA		
Class II			
In addition to requirements for Class I, in the case of Class II wells operating over the fracture pressure of the injection formation, all known wells within the area of review which penetrate formations affected by the increase in pressure. This requirement does not apply to existing Class II wells.	· NA		
Class III			
In addition to requirements for Class I, the corrective action proposed under 40 C.F.R. 144.55 for all Class III wells.	Refer to XI.C. heading.		
, a. Class I information requirement.	a. See Appendix B, Volume II.	a. Water level and existing well data in 5-mile radius.	
	b. Sheet 2.1-1 (UIC)	b. Roads, structures, etcetera.	
b. Abandonment plan and corrective action.	c. Section 2, Volume V.	c. Corrective action plan.	
D. Maps and Cross-Sections of Underground Sources of Drinking Water (USDWs)  Submit maps and cross sections indicating the vertical limits of all underground sources of drinking water within the area of review (both vertical and lateral limits for Class I), their position relative to the injection formation and the direction of water movement, where known, in every underground source of drinking water which may be affected by the proposed injection. (Does not apply to Class II wells.)	This volume, Figure 2.1-2	Regional map. East-west cross-section. North-south cross-section.	

Table 3.2-1. Form 4 - Underground Injection Con	able 3.2-1. Form 4 - Underground Injection Control (UIC) Permit Application - Information Summary			
Information Requirement	Information Location	Comments		
E. Name and Depth of USDWs (Class II)  For Class II wells, submit geologic name, and depth to bottom of all underground sources of drinking water which may be affected by the injection.		Does not apply.		
F. Maps and Cross-Sections of Geologic Structure of Area  Submit maps and cross sections detailing the geologic structure of the local area (including the lithology of injection and confining intervals) and generalized maps and cross sections illustrating the regional geologic setting. (Does not apply to Class II wells.)	Volume II, Figure 4.3-1 Volume II, Figure 4.3-2 Volume II, Figure 4.3-3 Volume II, Figure 4.3-4	Detailed site characterization in Volume II.  Cross-sections in figures are noted.		
G. Geological Data on Injection and Contingency Zones (Class II)		Does not apply.		
For Class II wells, submit appropriate geological data on the injection zone and confining zones including lithologic description, geological name, thickness, depth and fracture pressure.				
H. Operating Data	a. Volume V, Section 2.0	a) Operating procedures		
Submit the following proposed operating data for each well (including all those to be covered by area permits:		·		
<ol> <li>average and maximum daily rate and volume of the fluids to be injected;</li> </ol>	Volume V, Section 1			
2. average and maximum injection pressure;	Volume V, Section 1			
3. nature of annulus fluid;	No annulus	No annulus.		
<ol> <li>for Class I wells, source and analysis of the chemical, physical, radiological and biological characteristics, including density and corrosiveness of injection fluids;</li> </ol>	NA	No Class I wells are proposed		
<ol> <li>for Class II wells, source and analysis of the physical and chemical characteristics of the injection fluid; and</li> </ol>	NA	No class II wells are proposed.		

Table 3.2-1. Form 4 - Underground Injection Control (UIC) Permit Application - Information Summary			
Information Requirement	Information Location	Comments	
<ol> <li>for Class III wells, a qualitative analysis and ranges in concentrations of all constituents of injected fluids. If the information is proprietary, maximum concentrations only may be submitted, but all records must be retained.</li> </ol>	APP Volume I, Section 4.3 Table 4.3-1 Volume IV, Section 3	Injected fluid generally consists of a weak sulfuric acid.	
I. Formation Testing Program	Volume II, Section 2.0		
Describe the proposed formation testing program.	·		
For Class I wells the program must be designed to obtain data on fluid pressure, temperature, fracture pressure, other physical, chemical, and radiological characteristics of the injection matrix and physical and chemical characteristics of the formation fluids.	NA	No Class I wells are proposed.	
For Class II wells the testing program must be designed to obtain data on fluid pressure, estimated fracture pressure, physical and chemical characteristics of the injection zone. (Does not apply to existing Class II wells or projects.)	NA	No Class II wells are proposed.	
For Class III wells the program must be designed to obtain data on fluid pressure, fracture pressure, and physical and chemical characteristics of the formation fluids if the formation is naturally water bearing.  Only fracture pressure is required if the formation is not water bearing. (Does not apply to existing Class III wells or projects.)	Volume II, Section 2.0.  Volume II, Appendix C.	Data was obtained during this investigation pertaining to formation characteristics. Section 2 (II) contains analysis of hydraulic and packer tests, existing groundwater data.	
J. Stimulation Program  Outline any proposed stimulation program.		A stimulation program may include over pressuring, jetting, or other well stimulation prior to operation.	
K. Injection Procedures  Describe the proposed injection procedures including pump, surge, tank, etcetera.	Volume V, Section 2 for well operations. Volume V, Section 1 for facility operation.	Injection pressure at the wellhead shall be calculated so as to assure that pressure in the injection zone during injection does not initiate new fractures or propagate existing fractures in the injection zone.	

Table 3.2-1. Form 4 - Underground Injection Con	able 3.2-1. Form 4 - Underground Injection Control (UIC) Permit Application - Information Summary			
Information Requirement	Information Location	Comments		
L. Construction Procedures  Discuss the construction procedures (according to § 146.12 for Class I, § 146.22 for Class II, and § 146.32 for Class III) to be utilized. This should include details of the casing and cementing program, logging procedures, deviation checks, and the drilling, testing and coring programs, and proposed annulus fluid. (Request and submission of justifying data must be made to use an alternative to a packer for Class I.)	Volume V, Section 2.0	All new Class III wells shall be cased and cemented to prevent the migration of fluids into or between underground sources of drinking water. The wells will meet the requirement of 146.32.  Because wells will be drilled on an annual basis, and this exemption is for an area permit, only a typical well is shown.		
M. Construction Details  Submit schematic or other appropriate drawings of the surface and subsurface construction details of the well.	Volume V, Section 2.0 Volume V, Figure 2.2-2(V)	Final well construction details will be submitted prior to initiation of mining operations.  Typical well design.		
N. Changes in Injected Fluid  Discuss expected changes in pressure, native fluid displacement, and direction of movement of injected fluid. (Class III wells only.)	Volume V, Section 2.0 Volume IV	No changes in pressure, native fluid displacement or movement of injected fluid are expected beyond the mining area.  Volume IV discussed the modeling and fluid movement.		
O. Plans for Well Failures  Outline contingency plans (proposed plans, if any, for Class II) to cope with all shut-ins or well failures, so as to prevent migration of fluids into any USDW.	Volume V, Section 2.0			
P. Monitoring Program  Discuss the planned monitoring program. This should be thorough, including maps showing the number and location of monitoring wells as appropriate and a discussion of monitoring devices, sampling frequency, and parameters measured. If a manifold monitoring program is utilized, pursuant to § 146.23(bX5), describe the program and compare it to individual well monitoring.	Volume V, Section 1.9 Volume III Volume V	Injection pressures will be monitored by manifold for discrete sets of wells on a daily basis.  See Volume III: Groundwater sampling and analysis plan.  See operational description in Section 1 of Volume V		

Information Requirement Information Location Comments			
Information Requirement  O. Plugging and Abandonment Plan	Volume V, Appendix E	Plugging and abandonment will be performed in accordance wit	
Submit a plan for plugging and abandonment of the well including:	Volume V, Section 2.0	information required on EPA Form 7520-14 and Arizona Depart of Water Resources regulations.	
Submit a plan for plugging and abandonment of the well including:			
<ol> <li>describe the type, number, and placement (including the elevation of the top and bottom) of plugs to be used;</li> </ol>	Volume V, Appendix E		
2. describe the type, grade, and quantity of cement to be used; and	Volume V, Appendix E		
3. describe the method to be used to place plugs.	Volume V, Appendix E		
Also for a Class III well that underlies or is in an exempted aquifer, demonstrate adequate protection of USDWs. Submit this information on EPA Form 7520-14, Plugging and Abandonment Plan.	Form 7520-14	To be submitted as wells are closed	
R. Necessary Resources  Submit evidence such as a surety bond or financial statement to verify that the resources necessary to close, plug or abandon the well are available.	APP Volume I, Section 3.0	See 10K form, and letter of assurance signed by Chief Financia Officer of Magma Copper Company.	
S. Aquifer Exemptions  If an aquifer exemption is requested, submit data necessary to demonstrate that the aquifer meets the following criteria:	This volume, see Table 2.8 for items 1, 2, and 3 below	Includes discussions pertaining to items 1-3. Underground sour of drinking water have been identified, including descriptions o geographic and geometric characteristics.	
1. does not serve as a source of drinking water;			
cannot now and will not in the future serve as a source of drinking water; and			
3. the TDS content of the groundwater is more than 3,000 and less than 10,000 mg/l and is not reasonably expected to supply a public water system.			

Table 3.2-1. Form 4 - Underground Injection Control (UIC) Permit Application - Information Summary			
Information Requirement	Information Location	Comments	
Data to demonstrate that the aquifer is expected to be mineral or hydrocarbon producing, such as general description of the mining zone, analysis of the amenability of the mining zone to the proposed method, and time table for proposed development must also be included. For additional information on aquifer exemptions, see 40 C.F.R. 144.7 and 146.4.			
T. Existing EPA Permits	This volume, Section 2.5.		
List program and permit number of any existing EPA permits, for example, NPDES, PSD, RCRA, etcetera.			
U. Description of Business	This volume, Section 1.0.		
Give a brief description of the nature of the business.			
XII. Certification			
All permit applications (except Class II) must be signed by a responsible corporate officer for a corporation, by a general partner for a partnership, by the proprietor of a sole proprietorship, and by a principal executive or ranking elected official for a public agency. For Class II, the person described above should sign, or a representative duly authorized in writing.	This volume, Section 2.9 and UIC Application Form 4.		
V. Level of Justification	V. Magma Level of Justification		
The most significant tasks in approving an aquifer exemption request are defining the aquifer, delineating its boundaries (including confining zones), and justifying the need for the exemption. A guide to the evidence is outlined in the following checklist.	Exemption. The left side of the page was extracted	viewing the Magma Aquifer Exemption Request for a Minor ed from EPA Region IX document dated March 1993 entitled	
This checklist is provided solely for use as an aid in preparing and reviewing aquifer exemption requests.  Refer to 40 CFR 144.7 for general provisions; to 40 CFR 146.04, for criteria and standards applicable to aquifer exemptions.			
Data and other evidence which are used to support the aquifer exemption request must be included with the application.			

Form 4 - Underground Injection Control (UIC) Permit Application - Information Summary			
Information Requirement	Information Location	Comments	
Economic analyses shall be done in a precise, detailed, and representative manner.			
Maps required for the aquifer exemption application are in addition to any maps required in other applications (e.g., permit applications). Other information required for the aquifer exemption request that is available as part of an accompany permit application may be incorporated by reference.	,		

NA - Not applicable

FIGURES

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#### **SECTION 4.0**

#### REFERENCES

- 1. Arizona Department of Environmental Quality (ADEQ), Aquifer Protection Permit Application Guidance Manual, Mod. September 11, 1991.
- 2. Arizona Department of Water Resources (ADWR), Well Registry Files and Driller's Logs in the Florence Project Area. 1995.
- 3. Beer, K.E., A Ground-water Survey and Predictive Model for the Town of Florence, Arizona, M.S. Thesis, University of Arizona, 105 p. 1988.
- 4. Conoco Copper Project, Florence, Arizona, Phase III Feasibility Study: Volume III, Hydrology, Geology, and Ore Reserves: Conoco Minerals Department. 1976.
- 5. Errol L. Montgomery and Associates (Montgomery), Hydrogeologic Investigation for Prefeasibility Studies for Florence Project, Magma Copper Company, Pinal County, Arizona. Tucson, Arizona. February, 1994.
- 6. Hardt, W.F. and Cattany, R.E., Description and Analysis of the Geohydrologic System in Western Pinal County, Arizona; U.S. Geological Survey Open-File Report 65-68. 1965.
- 7. U.S. Code of Federal Regulations, Title 40-Protection of the Environment; Chapter I-Environmental Protection Agency; Subchapter D-Water Programs; Parts 144-146-Underground Injection Control Program. July 1, 1986.
- 8. U.S. Congress, Safe Drinking Water Act of 1974, Public Law 93-523, December 14, 1974, and Subsequent Amendments.
- 9. U.S. Environmental Protection Agency (USEPA), Region IX Aquifer Exemption Guidance. March, 1993.

ACBI

### CONFIDENTIAL BUSINESS INFORMATION

**VOLUME I OF V** 

INTRODUCTION AND REQUIRED ELEMENTS

MAGMA FLORENCE IN-SITU PROJECT
UNDERGROUND INJECTION CONTROL APPLICATION

#### APPENDIX A

PRE-FEASIBILITY STUDY FLORENCE PROJECT
MAGMA COPPER COMPANY
EXECUTIVE SUMMARY

Information contained in Appendix A has sensitive business information concerning unit costs, revenue forecasts, and other similar information of a proprietary nature that if released to the public may have an adverse financial impact on the Magma Copper Company.

**JANUARY 1996** 



MAGMA COPPER COMPANY

Florence, Arizona

#### APPENDIX A

# PRE-FEASIBILITY STUDY FLORENCE PROJECT MAGMA COPPER COMPANY EXECUTIVE SUMMARY

Please refer to the additional binder for Appendix A.

Copies of the designs and full size drawings (contained in tubes) can be found at:

Arizona Department of Environmental Quality, Phoenix, Arizona U.S. Environmental Protection Agency, San Francisco, California Magma Copper Company, Tucson, Arizona

# APPENDIX B SECTION 5, VOLUME I AQUIFER PROTECTION PERMIT APPLICATION

#### **SECTION 5.0**

#### COMPLIANCE WITH AQUIFER WATER QUALITY STANDARDS

#### 5.1 COMPLIANCE MONITORING STRATEGY

Magma Copper Company's (Magma's) proposed monitoring program is designed to ensure that the Aquifer Water Quality Standards (AWQS) will be protected in the manner prescribed in A.R.S. §§ 49-241 through 49-249. The program takes into account site characteristics, facility design, existing groundwater quality, and existing and future uses of the groundwater.

Information presented in Section 4.0 of this volume describes the control technologies that have been selected to eliminate discharges from surface facilities and to establish hydraulic controls for the in-situ mining operations that will ensure protection of the AWQS at the points of compliance (POCs) during the operating and post-closure phases of the facility.

Information presented in Section 6.0 of this volume describes methods that will be used to monitor facility operations and the steps that will be taken in the event of an AWQS exceedance or in the event that the AWQS are threatened.

The closure and post-closure plans presented in Section 7.0 of this volume describe steps that will be taken to clean and/or remove all surface components of the facility except the tailings ponds and to properly close the wells used in the in-situ mining operation. As closure is accomplished, the hydraulic controls that existed during operations will cease and the leached zones will be allowed to return to equilibrium with the surrounding aquifer.

The Groundwater Monitoring Plan presented in Volume III of this application is designed to present accurate data regarding the quality of groundwater at the POC. The location and design of the wells located, or proposed to be located, at the proposed POC have been selected after completing detailed simulation analyses presented in Volume IV of this application. Those analyses took into account the proposed design of the in-situ mining operation and the hydrogeologic features of the area as reported in Volume II of this application.

#### 5.2 POINTS OF COMPLIANCE

#### 5.2.1 Pollutant Management Area (PMA)

Pursuant to A.R.S. § 49-244, the POC for hazardous substances and the limit of the Pollutant Management Area (PMA) are identical. The PMA is defined as the horizontal boundary of an individual discharging unit or an imaginary line circumscribing several discharging activities. Under certain circumstances, the Arizona Department of Environmental Quality (ADEQ) director may establish POC for nonhazardous substances up to 750 feet outside a PMA.

The PMA for the facility as it will exist during the operational phase is shown on Figure 5.1-1(I). As closure activities proceed as described in Section 7.0 of this volume, the PMA surrounding the SX/EW plant will contract and eventually encompass only the tailing ponds which are

proposed to be closed with sediment remaining in place. The facility will then contain two PMAs, one encompassing the tailings ponds and the other encompassing the in-situ mine area.

#### 5.2.2 Discharge Impact Area (DIA)

Discharge Impact Area (DIA) is defined at A.R.S. § 49-201.11 as the potential areal extent of pollution migration, as projected on the land surface, as the result of a discharge from a facility. As reported in Volume IV of this application, detailed studies using groundwater flow and solute transport models were used to evaluate the potential impacts of the in-situ mining operations. (Although the proposed impoundments are considered "discharging" facilities pursuant to A.R.S. § 49-241.B, they have been designed to have no discharges.) The studies covered the full extent of the proposed operation, all closure activities, and the 30-year post-closure period. They were used in the location and design of the monitoring wells described in Table 5.2-1 below.

The modeling studies indicate that hydraulic controls can be maintained during the mining operations such that groundwater will flow into, not out of, the leach zone. The hydraulic controls thereby assure that the leaching activities will not contribute to AWQS exceedance during the period of facility operations.

The models were also used to evaluate DIA during the 30-year post-closure period when there will be no hydraulic controls. The outer limit of the 30-year DIA is shown on Figure 5.1-1(I). It is shown as a function of sulfate distribution because sulfate is the predominate anion in the leachate stream. (See Table 4.3-1 for estimated composition of solution after attenuation after block wash.) The models indicate that the AWQS for hazardous substances will be maintained through the 30-year post-closure period and that the maximum limit of the DIA will shift northward no more than 1,700 feet during the 30-year period.

The low concentrations of hazardous and non-hazardous substances in the solutions remaining in the leached zone after closure and the slow movement of the plume (less than 1,700 feet during the 30-year post-closure period) provides assurance that the mine activity will present little threat to the surrounding aquifer during the post-closure period and beyond. In the event that elevated concentrations are seen at the POC wells during the post-closure period, there will be adequate opportunity to alert downstream users, take additional samples, and if needed, install additional samples wells outside the PMA as indicated in the post-closure plan described in Section 7 of this volume.

#### 5.2.3 Proposed POC Monitoring Well System

In consideration of the anticipated lateral extent of the project DIA, the control technologies employed, and the hydrogeologic characteristics of the Magma Florence site, the following POC strategy and monitoring well configuration is proposed:

• Establish POC monitoring wells along the western and northern boundary of the in-situ mine area for use during the operational and post-closure periods. As depicted in Figure 5.2-l(I) and listed in Table 5.2-1, use of 20 monitoring wells screened in either the Lower Basin-Fill Unit (LBFU) or the Oxide Bedrock Zone along the proposed extent of the POC is proposed. This well array is located

downgradient from the proposed in-situ leaching activity under ambient groundwater conditions, with all wells located within 400 feet of the boundary of the ore body slated for mining. Of the 20 proposed POC wells, eleven are currently in place and nine are planned.

- The selection of the lateral position of the proposed wells, and the intercept of the screened intervals has taken into consideration the need to monitor the flow of groundwater along the two principal fault systems (The Sidewinder and the Party Line faults), with screens also placed in two apparent structural features that traverse the western boundary of the in-situ mine area. The vertical distribution of well screens in the LBFU is designed to monitor water quality in both the upper and lower strata of the unit.
- Use of the well set described above to monitor a suite of indicator water quality parameters for the detection of excursions of both hazardous and nonhazardous constituents of the process solutions throughout the operational and closure phases of the project. If a release of a nonhazardous analyte is confirmed through the assessment of water chemistry from the primary well suite, then Magma proposes that the Arizona Department of Environmental Quality (ADEQ) consider the subsequent selection of appropriate nonhazardous POC wells in downgradient locations that will ensure the protection of future uses of the overlying aquifer. It is anticipated that these response POC wells would be located no further downgradient than the project property line, to a maximum distance of 1/2 mile from the boundary of the in-situ mine area.
- Placement of two wells downgradient and northwest of the proposed SX/EW facility and the evaporation/tailings ponds (wells F and G on Figure 5.2-1[I]). These wells would contain screens that intercept the upper 100 feet of the Upper Basin-Fill Unit (UBFU), from the water table downward. These wells are proposed as a means of monitoring the performance of the discharging surface facilities. The operational detection monitoring in these wells would essentially be the same as that established for the POC wells flanking the in-situ well field.
- Upon completion of the post-operational closure period, Magma proposes that ADEQ consider the relocation of the non-hazardous POC to the downgradient fringe at the post-closure DIA depicted on Figure 5.1-1(I). During the 30-year post-closure period, compliance to hazardous constituent standards would be demonstrated at the wells depicted on Figure 5.2-1(I).
- Inclusion of four well installations in the upper alluvial overlying the oxide ore (wells M2-GU, M3-GL, M4-0 and H) to monitor groundwater quality upgradient from the mine operations. These wells are positioned to intercept the appropriate geologic units in regards to the potential for impacts to water quality that could occur downgradient from each location.

#### 5.3 GROUNDWATER QUALITY MONITORING PROGRAM

The proposed program for monitoring groundwater quality during mining operations is presented in this section. The discussion is focused on information goals, network design, data analysis, and reporting. Procedural aspects of the program, including sampling protocols, quality assurance/quality control (QA/QC), and data management, are described in the Groundwater Sampling and Analysis Plan presented in Volume III. The groundwater sampling and analysis plan has been revised and commented upon by ADEQ and EPA. Revisions were made based upon those recommendations and are included in the plan. Other topics related to the compliance monitoring program that are discussed elsewhere are as follows:

Торіс	Section
Proposed points of compliance	Volume I, Section 5.2
Contingency plan for exceedance of groundwater compliance levels	Volume I, Section 6.3
Post-closure groundwater monitoring program	Volume I, Section 7.3
Monitoring well design and construction	Volume II, Section 2.3
Water level measurements	Volume II, Section 2.3
Baseline monitoring program	Volume II, Section 4.5

#### 5.3.1 Legal Authority

Significant legislative and regulatory provisions governing groundwater compliance monitoring for Aquifer Protection Permits (APP) in Arizona are listed below.

Document Name	Section Number	Section Name
Arizona Revised Statutes	49-221	Water quality standards in general
Arizona Revised Statutes	49-223	Aquifer water quality standards
Arizona Revised Statutes	49-244	Point of compliance
Arizona Administrative Code	R18-9-110	Individual permit conditions: alert levels
Arizona Administrative Code	R18-9-112	Individual permit conditions: monitoring requirements
Arizona Administrative Code	R18-9-113	Individual permit conditions: reporting requirements
Arizona Administrative Code	R18-9-114	Individual permit conditions: contingency plan requirements
Arizona Administrative Code	R18-11-405	Narrative aquifer water quality standards
Arizona Administrative Code	R18-11-406	Numeric aquifer water quality standards: drinking water protected use

#### 5.3.2 Information Goals

Information goals form the basis for development of the proposed groundwater monitoring program. A three step process, described by Adkins et al. (1995), was used to identify information goals. First, regulatory information goals (RIGs) were identified by reviewing laws and regulations. Monitoring information goals (MIGs) were then established to meet the regulatory goals. Finally, when statistical methods are chosen to achieve the monitoring goals, specific statistical information goals (SIGs) will be prepared.

RIGs are broad, qualitative statements that describe the underlying motives for conducting monitoring. They tend to address general objectives rather than the specifics of monitoring. MIGs are designed to be as specific as possible, but like RIGs, are stated in purely qualitative terms. MIGs are narrative statements that describe exactly why monitoring is being conducted. SIGs are quantitative, as well as specific. They describe the mechanics of how statistics will be used to extract information from data.

The following regulatory information goals were identified for the compliance monitoring program:

- Protect public health and the environment.
- Ensure protection of all current and reasonably foreseeable future uses of the aquifer.
- Determine compliance with water quality standards.
- Obtain early warnings that may indicate potential violations of water quality standards.
- Ensure compliance with Aquifer Protection Permit conditions.
- Evaluate the effectiveness of actions taken to mitigate the impacts of any exceedances in water quality that may occur.

The following monitoring information goals were identified for the compliance monitoring program:

- Monitor concentrations of constituents that will be the most likely to indicate an increased potential for exceedance of Aquifer Quality Limits (AQLs).
- Become aware of any exceedances of AQLs as soon as possible.

<sup>&</sup>lt;sup>1</sup> In: The Role of Data Analysis Protocols in Obtaining Groundwater Quality Management Information; Procedures for the International Union of Geodesy and Geophysics, XXI General Assembly, Boulder, Colorado, July 2 to 14, 1995.

- Monitor all hydrogeologic units where contamination from mining operations could potentially occur.
- Concentrate monitoring efforts in the hydrogeologic units where the effects of mining are the most likely to occur (e.g. near the oxide/basin-fill contact).
- Monitor in the lateral portion of the aquifer where the effects of mining are the most likely to occur (e.g. downgradient of mining operations).

Statistical information goals will be developed when statistical methods are chosen.

## 5.3.3 Determination of Compliance Levels and Verification of Compliance Level Exceedances

The statistical approach for determining compliance levels has not been finalized. In general, statistical methods will be proposed that (1) are appropriate for the data distributions, (2) will maximize power and minimize the occurrence of false positives, and (3) will minimize the effects of spatial and temporal correlation. Statistical principles that will be used for determining compliance levels and verifying compliance level exceedances are outlined in Appendix F of Volume I.

Tables 5.3-1 and 5.3-2 show which water quality variables would have alert levels (ALs) and which would have AQLs. In general, alert levels would be assigned to those variables that can serve as indicators for potential AQL exceedances, and AQLs would be assigned to variables that have AWQSs.

#### 5.3.4 Compliance Monitoring Locations

All 22 hazardous POC wells identified in Table 5.2-1 will be monitored on a quarterly basis during mining operations and closure. The rationale for choosing the proposed POCs is presented in Section 5.2 of this volume, and Section 5.0 of Volume II.

#### 5.3.5 Water Quality Variables to be Measured

Two sets of chemical water quality variables, Level 1 and Level 2, were selected for compliance monitoring at the hazardous POCs (Tables 5.3-1 and 5.3-2). Level 1 variables will be monitored on a quarterly basis to provide early warning of potential AQL exceedances. Level 2 variables will monitored annually regardless of the results of Level 1 monitoring. In addition, Level 2 variables will be monitored quarterly if alert levels are exceeded for Level 1.

Level 1 variables were chosen based on their ability to provide early warning of potential AQL exceedances. Effective "early warning" indicators should have the following characteristics:

- Relatively high mobility and low attenuation.
- Provide sufficient warning of potential AQL exceedances.

• Occur in a significantly higher concentration in mining impacted groundwater than in unimpacted groundwater.

Fluoride, magnesium, sulfate and total dissolved solids were chosen as the four water quality variables that best meet these criteria based on water quality information presented in Volumes I, III, and IV.

Level 2 water quality variables are assigned to one of three categories. The first category, "selected constituents with AWQSs", consists of all inorganic chemicals with AWQSs that have the potential to exceed those standards due to mining activities. Asbestos, cyanide, nitrate, and nitrite were not included because they are not present in the mining solution and cannot result from the mining process. Fluoride was not included because it is a Level 1 indicator parameter.

Radionuclides, the second category of water quality variables in Level 2, consists of radionuclides that are used in calculations to determine compliance with Arizona numeric aquifer water quality standards (A.A.C R18-11-406). The third category of water quality variables primarily consists of cations and anions that will be used for quality control purposes.

#### 5.3.6 Sampling Frequency

In general, sampling will be conducted quarterly or annually during operational compliance monitoring. The determination of which months form the four quarters will be determined after baseline data has been evaluated for seasonality. As more information is obtained on water quality and hydrogeology, it may become evident that sampling frequencies in some wells should be modified on either a temporary or permanent basis. Proposed changes in sampling frequencies will be carefully reviewed by Magma and submitted to ADEQ for approval prior to implementation.

As stated previously, Level 1 variables will be monitored on a quarterly basis to provide early warning of potential AQL exceedances. Level 2 variables will monitored annually regardless of the results of Level 1 monitoring. In addition, Level 2 variables may be monitored quarterly if alert levels are exceeded for Level 1 variables.

Annual monitoring of Level 2 constituents will help to ensure that the Level 1 indicator parameters are providing adequate warning of potential AQL exceedances. In addition, annual monitoring will provide an ongoing record of water quality that will be unaffected by seasonality (assuming that sampling will be conducted at approximately the same time each year).

If new wells are constructed for compliance monitoring, they will be sampled monthly for 1 year (or quarterly for 2 to 3 years) to obtain data for establishing compliance limits.

#### 5.3.7 Data Analysis

There are several applications where data analysis will be conducted for the groundwater compliance monitoring program; evaluation of baseline data, calculation of compliance levels, determination of exceedance of compliance levels, and summarization of compliance monitoring data. Each application is described below.

After all 12 months of baseline water quality data are collected, descriptive statistical methods will be used to characterize the data. Temporal and spatial variability, central tendency, and distributional shape will be examined. The data will also be evaluated for the presence of seasonality and, based on that evaluation, sampling quarters will be defined.

Baseline data collected from the proposed POC wells will be used to calculate ALs and AQLs. As mentioned previously, statistical methods chosen to calculate compliance levels will be appropriate for the data distributions, will maximize power and minimize the occurrence of false positives, and will minimize the effects of spatial and temporal correlation. Statistical methods will also be used to determine if compliance levels have been exceeded. Statistical principles that will be used for determining compliance levels and verifying compliance level exceedances are outlined in Appendix F.

Descriptive statistical methods will be used to define the characteristics of compliance monitoring data. On an annual basis, the data will be summarized using simple data analysis procedures such as time-concentration plots and boxplots. The purpose of the evaluation will be to convey general information about water quality that is difficult to obtain from tabulated data.

#### 5.3.8 Reporting

A groundwater compliance monitoring report will be submitted after each quarterly sampling period. The report will be submitted to ADEQ by the last day of the first month following each quarter. For example, if a quarter included February, March, and April, the report will be submitted by May 31. The report will include the following information:

- Sampling data (location of sample, date and time of sample collection, sampler's name, chain of custody forms).
- Field data (pH, specific conductance, temperature, purge volume, and relevant field notes).
- Laboratory data (laboratory name, sample analysis date, analysis method, and analytical results).
- Description of variances, if any, from the Sampling and Analysis Plan.
- Description of verification analysis or sampling, if any, that occurred within the last quarter.
- Descriptive statistics of water quality data (annually).

If an AL exceedance is verified, a report will be submitted to ADEQ within 30 days after verification of the exceedance. The report will include the following information:

• Either a demonstration that the cause of the AL exceedance is not the result of the permitted facility activities; or

A description of the causes, impacts, or mitigation of the discharge.

If an AQL exceedance is verified, a report will be submitted to ADEQ within 30 days after verification of the exceedance. The report will include the following information:

- A description of the exceedance and its cause.
- The period of exceedance, including exact date(s) and time(s), if known, and the anticipated time period during which the exceedance is expected to continue.
- Any action taken or planned to mitigate the effects of the exceedance, or to eliminate or prevent recurrence of the exceedance.
- Any monitoring activity or other information which indicates that any pollutants would be reasonably expected to cause a violation of an AWQS.
- Any malfunction or failure of pollution control devices or other equipment or process.

#### 5.4 PRESENT AND ANTICIPATED FUTURE AQUIFER USAGE

Detailed descriptions of present groundwater usage in the 100-square mile Florence project area and the proposed in-situ mine area are presented in Volume II, Sections 3.9 and 4.6, respectively, of this application. The Florence Project Area is located on the northern boundary of the Eloy subbasin within the Pinal Active Management Area (AMA). Arizona Department of Water Resources (ADWR) Second Management Plan, 1990-2000, Final Active Management Area, 289 p., January, 1991. Approximately 80 percent of the Pinal AMA population resides in the Eloy basin. Approximately 50 percent of agricultural activity in the Pinal AMA also occurs in the Eloy subbasin.

Presently approximately 382 registered wells (ADWR, 1995) are located within a 5-mile radius of the proposed in-situ mine area (Sheet 1.1-1[I]), approximately 65 percent of which withdraw groundwater. The majority of groundwater is used for irrigation, primarily by the San Carlos Irrigation Project (SCIP), which is used to supplement surface water derived from the Gila River. A total of 22 SCIP wells are located within the 100-square mile Florence Project Area which pump an average of 13,200 acre-feet of groundwater each year. Three irrigation wells in close proximity to the proposed in-situ mine area are planned to be abandoned and relocated prior to commencement of mining activities. The proposed in-situ mining operations will not affect agricultural groundwater withdrawals in the area. Thirteen irrigation wells not operated by SCIP (private wells) are located within 1 mile of the proposed in-situ mine area, which withdraw approximately 4,385 acre feet annually.

The Town of Florence operates five public water supply wells in and around the Florence Project Area. Two wells are located approximately 2.5 miles east and two are located approximately 3 miles south of the proposed in-situ mine area (see Sheet 1.1-1[I]). The Arizona Department of Corrections operates two public supply wells located approximately 2.5 miles south and 3 miles

east of the proposed in-situ mine area. These seven municipal water supply wells pump an average of 1,722 acre feet of groundwater each year. All of these public supply wells are generally hydraulically upgradient from the proposed in-situ mine area and will not be affected by proposed mining operations.

Approximately 134 private domestic wells are located within the 100-square mile Florence Project Area which pump an average of 52 acre feet of groundwater annually. This is about 2 to 3 percent of the total groundwater use in the area. Two private domestic wells are located within 1 mile of the proposed in-situ mine area but are not used for drinking water due to the high nitrate levels. These wells are located on Magma lands and the users use bottled water for consumptive purposes. These wells are operated by Magma and will not be used for domestic purposes during mining operations. Private domestic wells in the model area will not be affected by proposed in-situ mining operations.

As the result of groundwater management practices implemented in the Pinal AMA, ADWR (1991) predicts that irrigation efficiency will increase 10 to 40 percent. This, combined with retirement of agricultural lands and substitution of approximately 50 percent of present groundwater used for agriculture with Central Arizona Project Water, will greatly reduce groundwater usage associated with agriculture.

Domestic groundwater use will increase in the next 10 to 20 years. The Town of Florence has projected a residential growth rate of 74 percent over the next 15 years, and combined residential and institutional growth rate of 54 percent. It is anticipated that this could increase groundwater usage from the current amount of 1,722 acre-feet to 3,602 acre-feet.

Groundwater withdrawals associated with proposed in-situ mining operations are estimated to be to 1,293 acre-feet annually occurring over a period of approximately 15 years from the beginning of mining activities. Overall groundwater withdrawals are expected to generally remain similar to current amounts or decline slightly. Proposed in-situ mining operations are not expected to influence groundwater withdrawals in the future and in fact groundwater use will be reduced during the life of mine as over 200 acres will be taken out of agricultural use.

Model II	Table 5.2-1		sed Point of Com	inliance	and Upgray	dient Monitori	ing Wells - W	ell Location,	Construction,	and Lithole	ogy						
15°N   Sercence   Co.D. in.   Diameter   Diameter   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.   Co.D. in.						Casir	36		Screen			ar Seal		D eference	Depth Center of	Distance from Center of Screen to Geologic Contact	Center of gic Contact
157N   590   LBFU   5 9/16 LCS   -1.2 to 524   5 9/16 PVC   524 to 563   39   Bentonite     4.8'N   940   LBFU   4.12 LCS   591 to 1011   4 1/2 PVC   1011 to 1070   59   Cement     4.7'N   1110   Oxide   4 1/2 LCS   591 to 1011   4 1/2 PVC   1011 to 1070   59   Cement     4.7'N   1110   Oxide   4 1/2 LCS   591 to 1011   4 1/2 PVC   1011 to 1070   59   Cement     4.7'N   1110   Oxide   4 1/2 LCS   591 to 1011   4 1/2 PVC   1011 to 1070   59   Cement     4.7'N   1130   Oxide   5 9/16 LCS   -1.8 to 778   5 9/16 PVC   554 to 594   40   Bentonite     4.3'N   1150   Oxide   5 9/16 LCS   -1.8 to 598   5 9/16 PVC   598 to 658   60   Cement     4.3'N   1130   LBFU   5 9/16 LCS   -1.8 to 598   5 9/16 PVC   598 to 658   60   Cement     4.3'N   1130   LBFU   5 9/16 LCS   -1.8 to 598   5 9/16 PVC   598 to 658   60   Cement     4.3'N   1130   Oxide   5 9/16 LCS   -1.8 to 598   5 9/16 PVC   598 to 658   60   Cement     4.3'N   1130   Oxide   5 9/16 LCS   -1.8 to 938   5 9/16 PVC   598 to 658   60   Cement     4.3'N   1130   Oxide   5 9/16 LCS   -1.8 to 938   5 9/16 PVC   598 to 658   60   Bentonite     4.5'N   1130   Oxide   5 9/16 LCS   -1.8 to 938   5 9/16 PVC   1130 to 1130   200   Bentonite     4.5'N   680   Oxide   6 5/8 PVC   -2.0 to 402   6 5/8 PVC   1100 to 130   Coment     4.5'N   680   Oxide   6 5/8 PVC   -2.0 to 402   6 5/8 PVC   Coment     4.5'N   680   Oxide   6 5/8 PVC   -2.0 to 402   6 5/8 PVC   Coment     4.5'N   680   Oxide   6 5/8 PVC   -2.0 to 402   6 5/8 PVC   Coment     4.5'N   680   Oxide   6 5/8 PVC   -2.0 to 402   6 5/8 PVC   Coment     4.5'N   680   Oxide   6 5/8 PVC   -2.0 to 402   6 5/8 PVC   Coment     4.5'N   680   Oxide   6 5/8 PVC   -2.0 to 402   6 5/8 PVC   Coment     4.5'N   680   Oxide   6 5/8 PVC   -2.0 to 402   6 5/8 PVC   Coment     4.5'N   680   Oxide   6 5/8 PVC   -2.0 to 402   6 5/8 PVC   Coment     4.5'N   680   Oxide   6 5/8 PVC   -2.0 to 402   6 5/8 PVC   Coment     4.5'N   680   Oxide   6 5/8 PVC   -2.0 to 402   6 5/8 PVC   -2.0 to 402   6 5/8 PVC   -2.0 to 402   6 5/8 PVC   -2.0	Existing or Planned	Well ID	Latitude/ Longitude		Unit	Diameter and Type (O.D. in.)	Interval (ft)	Diameter and Type (O.D. in.)	Interval (ft)	Length (ft)	Type	Interval (ft)	Surface Elevation (ft)	Point Elevation (ft)	Screened Interval (ft)	Geologic Contact	Distance <sup>(4)</sup> (ft)
MG-GU         111726' 95"W         59/16 LCS*         -1.45 to 0         59/16 PVC         -1.45 to 0         59/16 PVC         59/16 LCS*         -1.45 to 0         59/16 PVC         59/16 PVC         59/16 PVC         59/16 PVC         59/16 LCS         -1.45 to 0         939         4 1/2 PVC         859 to 928         69         Cement           MR-GL         111726' 19.7W         110         Oxide         4 1/2 LCS         59/16 LCS         -1.4 to 591         4 1/2 PVC         1011 to 1070         59         Cement           MI3-GL         111726' 11.7W         1110         Oxide         4 1/2 LCS         59/16 PVC         1011 to 1070         59         Cement           MI3-GL         111726' 13.7W         59         LBFU         59/16 LCS         -1.4 to 19         59/16 PVC         59/16 PVC         59/16 PVC         Cement           MI3-GL         111726' 13.7W         69         LBFU         59/16 LCS         -1.8 to 59         59/16 PVC         60         Cement           MI3-GL         111726' 12.7'W         119         LBFU <td>Point of</td> <td>Complian</td> <td>ce Wells</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td> -</td> <td></td> <td></td> <td></td>	Point of	Complian	ce Wells											-			
M7-GL III 26 95"W 940 LBFU 41/2 LCS 591 6 101 4 1/2 PVC 859 to 928 69 Cement M3-9 111 26 10.1"W 1110 Oxide 4 1/2 LCS 591 to 1011 4 1/2 PVC 1011 to 1070 59 Cement M14-GL III 26 10.1"W 1110 Oxide 4 1/2 LCS 591 to 1011 4 1/2 PVC 1011 to 1070 59 Cement M14-GL III 26 113."W 950 LBFU 59/16 LCS 1-14 to 19 59/16 PVC 554 to 594 40 Bentonite B <sub>DX</sub> 11126 113."W 630 LBFU 59/16 LCS 1-14 to 19 59/16 PVC 554 to 594 60 Cement M15-GU III 26 113."W 630 LBFU 59/16 LCS 0 to 930 59/16 PVC 598 to 658 60 Cement M16-GU III 26 12."W 690 LBFU 59/16 LCS 1.8 to 598 59/16 PVC 938 to 998 60 Bentonite M16-GU III 26 12."W 690 LBFU 59/16 LCS 1.8 to 598 59/16 PVC 938 to 998 60 Cement M17-GL III 26 12."W 1350 Oxide 59/16 LCS 0 to 1130 59/16 PVC 1130 to 1130 Cement Pl91-D 11125 12."W 680 Oxide 658 PVC 12.0 to 10 10 658 PVC 1130 to 1130 Cement Pl91-D 11125 12."W 680 Oxide 658 PVC 12.0 to 10 10 658 PVC 1130 to 1130 Cement Cement Pl91-D 11125 12."W 680 Oxide 658 PVC 12.0 to 10 10 658 PVC 12.0 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 658 PVC 1130 to 10 10 10 658 PVC 1130 to 10 10 10 658 PVC 1130 to 10 10 10 658 PVC 1130 to 10 10 10 658 PVC 1130 to 10 10 10 10 10 658 PVC 1130 to 10 10 10 10 10 10 10 10 10 10 10 10 10	E(p)	M6-GU	33°3' 15"N 111°26' 9.7"W	980		5 9/16 LCS <sup>(4)</sup> 5 9/16 PVC	-1.45 to 0 -1.2 to 524	5 9/16 PVC	524 to 563	39.	Cement Bentonite	0 to 150 150 to 500	1480.5	1481.72	543	UBFU/LBFU LBFU/Oxide	+263
M8-O   111°26   10.1°W   1110   Oxide   4 1/2 LCS   591 to 1011   4 1/2 PVC   1011 to 1070   59   Cement   M14-GL   111°26   13.3°W   630   LBFU   5 9/16 LCS   -1.8 to 78   5 9/16 PVC   778 to 838   60   Bentonite   M15-GU   111°26   13.3°W   630   LBFU   5 9/16 LCS   14 to 19   5 9/16 PVC   554 to 594   40   Bentonite    M15-GU   111°26   13.3°W   1150   Oxide   5 9/16 LCS   0 to 930   5 9/16 PVC   554 to 594   40   Bentonite    M16-GU   111°26   12.7°W   630   LBFU   5 9/16 LCS   -1.8 to 598   5 9/16 PVC   598 to 658   60   Cement    M17-GL   111°26   12.7°W   130   LBFU   5 9/16 LCS   -1.8 to 598   5 9/16 PVC   598 to 658   60   Cement    M17-GL   111°26   12.7°W   1350   Oxide   5 9/16 LCS   0 to 1130   5 9/16 PVC   130 to 1330   Cement    M17-GL   111°26   12.7°W   1350   Oxide   5 9/16 LCS   0 to 1130   5 9/16 PVC   1130 to 1330   Cement    Plo, LO   111°25   12.6°W   680   Oxide   6 5/8 PVC   -2.0 to 402   6 5/8 PVC   402 to 601   199   Bentonite    Plo, LO   111°25   56°W   Cement   Cement    Plo, LO   111°25   12.0°W   680   Oxide   6 5/8 PVC   12.0 to 601   199   Bentonite    Plo, LO   111°25   56°W   Cement   Cement   Cement    Plo, LO   111°25   12.0°W   680   Oxide   6 5/8 PVC   12.0 to 601   199   Bentonite    Plo, LO   111°25   12.0°W   680   Oxide   6 5/8 PVC   12.0 to 601   199   Bentonite    Plo, LO   111°26   12.0°W   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130   130	б	M7-GL	33°3' 14.8"N 111°26' 9.5"W	940	LBFU		-1.0 to 593 593 to 859	4 1/2 PVC	859 to 928	69	Cement	0 to 838	1480	1480.95	868	UBFU/LBFU LBFU/Oxide	+828
M13-GU II1°26′ 13.3"W 630 LBFU 59/16 LCS -1.8 to 778 59/16 PVC 778 to 838 60 Bentonite  M15-GU II1°26′ 13.3"W 1150 Oxide 59/16 LCS 0 to 930 59/16 PVC 554 to 594 40 Bentonite  B <sub>OX</sub> 111°26′ 13.3"W 1150 Oxide 59/16 LCS 0 to 930 59/16 PVC 930 to 1130 Cement 33°2′ 50°N M16-GU II1°26′ 12.7"W 690 LBFU 59/16 LCS -1.8 to 938 59/16 PVC 938 to 638 60 Cement Bentonite  M17-GL II1°26′ 12.7"W 690 LBFU 59/16 LCS -1.8 to 938 59/16 PVC 938 to 638 60 Cement Bentonite  M17-GL II1°26′ 12.7"W 690 LBFU 59/16 LCS -1.8 to 938 59/16 PVC 938 to 998 60 Bentonite  M17-GL II1°26′ 12.7"W 680 Oxide 65/8 PVC -1.8 to 938 59/16 PVC 1130 to 1330 Cement Pl9.LO 0xide 65/8 PVC -1.8 to 998 60 Bentonite  Cement Cement Bentonite  Cement Bentonite  Cement Bentonite  Cement Bentonite  Cement Bentonite  Cement Bentonite  Cement Bentonite  Cement Bentonite  133°2′ 35.9"N 680 Oxide 65/8 PVC -1.8 to 938 60 Bentonite  Cement Bentonite  Cement Bentonite  Cement Bentonite  Cement Bentonite  Cement Bentonite  Cement Bentonite  Cement Bentonite  Cement Bentonite  133°2′ 35.9"N 680 Oxide 65/8 PVC -1.8 to 90 60 Bentonite	(a) El	O-8W	33°3' 14.7"N 111°26' 10.1"W	1110	Oxide		-1.4 to 591 591 to 1011		1011 to 1070	59	Cement	0 to 970	1479.1	1480.46	1040	LBFU/Oxide Oxide/Sulfide	+100
M14-GL 111°26′ 13.3"W 950 LBFU 5 9/16 LCS -1.8 to 778 5 9/16 PVC 778 to 838 60 Bentonite 33°3′ 3.7"N 630 LBFU 5 9/16 PVC 19 to 554 5 9/16 PVC 554 to 594 40 Bentonite B <sub>DX</sub> 111°26′ 13.3"W 1150 Oxide 5 9/16 LCS -1.8 to 938 5 9/16 PVC 930 to 1130 Cement 33°2′ 49.5"N 690 LBFU 5 9/16 LCS -1.8 to 938 5 9/16 PVC 938 to 658 60 Cement M14-GL 111°26′ 12.7"W 130 LBFU 5 9/16 LCS -1.8 to 938 5 9/16 PVC 938 to 658 60 Cement A <sub>DX</sub> 111°26′ 12.7"W 130 Oxide 5 9/16 LCS -1.8 to 938 5 9/16 PVC 1130 to 1330 Cement Pl9.1-O 111°25′ 12.9"N 680 Oxide 6 5/8 PVC -2.0 to 402 6 5/8 PVC 1130 to 1330 Cement Cement 111°25′ 12.9"N 680 Oxide 6 5/8 PVC -2.0 to 402 6 5/8 PVC -2.0 to 402 6 6/8 PUC -2.0 to 402 6 6/8 PUC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402 6 6/8 PVC -2.0 to 402																	
M15-GU         111°26′ 13.9″W         630         LBFU         5 9/16 LCS         -1.4 to 19         5 9/16 PVC         554 to 554         40         Bennonite           B <sub>0x</sub> 111°26′ 13.9″W         630         LBFU         5 9/16 LCS         0 to 930         5 9/16 PVC         930 to 1130         200         Bennonite           M16-GU         111°26′ 12.7″W         690         LBFU         5 9/16 LCS         -1.8 to 598         5 9/16 PVC         598 to 658         60         Cement           M17-GL         111°26′ 12.7″W         130         LBFU         5 9/16 LCS         -1.8 to 938         5 9/16 PVC         598 to 658         60         Bentonite           M17-GL         111°26′ 12.7″W         130         Cxide         5 9/16 LCS         -1.8 to 938         5 9/16 PVC         938 to 998         60         Bentonite           Aox         111°26′ 12.7″W         1350         Oxide         5 9/16 LCS         0 to 1130         5 9/16 PVC         1130 to 1330         200         Bentonite           Pl91-C         111°26′ 12.6″W         680         Oxide         5 9/16 LCS         0 to 1130         5 9/16 PVC         1130 to 1330         200         Bentonite	93	Mi4-GL		950	LBFU	\$ 9/16 LCS	-1.8 to 778	5 9/16 PVC	778 to 838	09	Cement Bentonite	0 to 17 17 to 748	1472.8	1474.58	808	MFGU/LBFU LBFU/Oxide	+524
33°2′ 50°N   33°2′ 50°N   59/16 LCS   0 to 930   59/16 PVC   930 to 1130   200   Bentonite   Cement   33°2′ 50°N   113°0   LBFU   59/16 LCS   -1.8 to 938   59/16 PVC   938 to 658   60   Cement   Bentonite   33°2′ 50°N   113°0   LBFU   59/16 LCS   -1.8 to 938   59/16 PVC   938 to 998   60   Bentonite   Cement   33°2′ 53.9°N   130   Oxide   59/16 LCS   0 to 1130   59/16 PVC   113°0 to 133°0   20°0   Bentonite   Cement   33°2′ 53.9°N   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0   20°0	(g)	M15-GU	33°3' 3.8"N 111°26' 13.9"W	630	$\vdash$	5 9/16 LCS 5 9/16 PVC	-1.4 to 19 19 to 554	5 9/16 PVC	554 to 594	40	Cement Bentonite	0 to 20 20 to 533	1472.6	1474.01	574	MFGU/LBFU LBFU/Oxide	+290
33°2′ 50"N 690 LBFU 59/16 LCS -1.8 to 598 59/16 PVC 598 to 658 60 Cement 33°2′ 49.5"N 1130 LBFU 59/16 LCS -1.8 to 938 59/16 PVC 938 to 998 60 Bentonite Cement 33°2′ 53.9"N 1350 Oxide 59/16 LCS 0 to 1130 59/16 PVC 1130 to 1330 200 Bentonite Cement 33°3′ 12.9"N 680 Oxide 65/18 PVC -2.0 to 402 65/8 PVC 402 to 601 199 Bentonite Cement 5500 111°25′ 56 "W 680 Oxide 65/16 LCS 12.6"D 65/16 PVC 12.0 to 402 65/8 PVC 402 to 601 199 Bentonite Cement 6500 111°25′ 56 "W 680 Oxide 65/16 LCS 12.6"D 65/16 PVC 12.0 to 402 65/8 PVC 402 to 601 199 Bentonite Cement 6500 111°25′ 56 "W 680 Oxide 65/16 LCS 12.6"D 65/16 PVC 12.0 to 402 65/8 PVC 402 to 601 199 Bentonite	<u>%</u>	B	33°3° 4.3"N 111°26° 13.3"W	1150	<del></del>	5 9/16 LCS	0 to 930		930 to 1130	200	Cement Bentonite	0 to 20 20 to 910	1472(6)	NA	1030	LBFU/Oxide	+150
33°2′ 50"N   59/16 LCS   -1.8 to 598   59/16 PVC   598 to 658   60   Cement     33°2′ 49.5"N   1130   LBFU   59/16 LCS   -1.8 to 938   59/16 PVC   938 to 998   60   Bentonite     33°2′ 49.5"N   130   LBFU   59/16 LCS   -1.8 to 938   59/16 PVC   938 to 998   60   Bentonite     33°2′ 53.9"N   1350   Oxide   59/16 LCS   0 to 1130   59/16 PVC   1130 to 1330   200   Bentonite     33°3′ 12.9"N   680   Oxide   65/8 PVC   -2.0 to 402   65/8 PVC   402 to 601   199   Bentonite     50° 111°25′ 56"W   680   Oxide   65/8 PVC   -2.0 to 402   65/8 PVC   402 to 601   199   Bentonite     50° 111°25′ 56"W   680   Oxide   65/8 PVC   -2.0 to 402   65/8 PVC   65/8 PVC   402 to 601   199   Bentonite     50° 111°25′ 56"W   680   Oxide   65/8 PVC   15.6.10   65/8 PVC   65/8 PVC   402 to 601   199   Bentonite     50° 111°25′ 56"W   680   Oxide   65/8 PVC   16.6.10   65/8 PVC   402 to 601   199   Bentonite     50° 111°25′ 56"W   680   Oxide   65/8 PVC   16.6.10   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   60° 100° 100°   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC   65/8 PVC													1				
33°2' 49.5"N   130   LBFU   5 9/16 LCS   -1.8 to 938   5 9/16 PVC   938 to 998   60   Bentonite	9	M16-GU	33°2' 50"N 111°26' 12.7"W	069	LBFU	5 9/16 LCS	-1.8 to 598	5 9/16 PVC	598 to 658	09	Cement Bentonite Cement	0 to 20 20 to 495 495 to 562	1464.3	1466.05	628	MFGU/LBFU LBFU/Oxide	+328
A <sub>OX</sub> 111°26′ 12.6″W 1350 Oxide 5 9/16 LCS 0 to 1130 5 9/16 PVC 1130 to 1330 200 Bentonite Bentonite 111°25′ 56″W 680 Oxide 6 5/8 PVC 2.0 to 402 6 5/8 PVC 402 to 601 199 Bentonite Cement Cement Communications and the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contractions of the contracti	Ęn ê	MI7-GL	33°2° 49.5"N 111°26° 12.7"W	1130	LBFU	s 9/16 LCS	-1.8 to 938	5 9/16 PVC	938 to 998	09	Cement Bentonite	0 to 20 20 to 917	1464.4	1466.16	896	MFGU/LBFU LBFU/Oxide	+668
33°3′ 12.9"N 680 Oxide 6 5/8 PVC -2.0 to 402 6 5/8 PVC   65/8 PVC   111°25′ 56"W 680   Oxide   65/8 PVC   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 60.10   15 6	<u>§</u>	Aox	33°2' 53.9"N 111°26' 12.6"W	1350	Oxide	S 9/16 LCS	0 to 1130	5 9/16 PVC	1130 to 1330	200	Cement Bentonite	0 to 20 20 to 1110	1464 <sup>(c)</sup>	NA	1230	LBFU/Oxide	+150
33°3′ 12.9°N 680 Oxide -2.0 to 402 65/8 PVC -2.0 to 402 FVC 402 to 601 199 Bentonite Cement									ļ								
Ot 20 2 1 2 00 2	'n	P19.1-0		089	Oxide	6 5/8 PVC	-2.0 to 402	6 5/8 PVC	402 to 601	199	Cement Bentonite	0 to 20 20 to 370	1483	1484.72	501	LBFU/Oxide Oxide/Sulfide	+146
W 460 LBFU 5.9/16 PVC 19 to 375 5.9/16 PVC 375 to 435 60 Bentonite	ш	O19-GL		<u> </u>	·	5 9/16 LCS 5 9/16 PVC	-1.6 to 19 19 to 375	5 9/16 PVC	375 to 435	09	Cement Bentonite	0 to 20 20 to 347	1481.7	1483.28	405	MFGU/LBFU LBFU/Oxide	+101 NA

Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part   Part	Table 5 2-1		sed Point of Com	nliance	and Upgra	dient Monitori	ing Wells - W	ell Location,	Construction,	and Lithol	logy						
12   12   12   13   13   14   15   14   15   14   15   14   14						Casir	ĝı		Screen			ar Seal		Reference	Depth Center of	Distance from Center of Screen to Geologic Contact	Center of gic Contact
118°N 1288 Oxide 658 PVC 20 to 808 658 PVC 661 to 721 60 Bentonite 20 to 760 1461.8  117°N 740 LBFU 59/16 PVC -0.9 to 661 59/16 PVC 661 to 721 60 Bentonite 20 to 50 1461.8  117°N 445 LBFU 59/16 LCS 0 to 70 0 50 5 59/16 PVC 740 to 800 60 Bentonite 20 to 355 1485° 1485° 158° 158° 158° 158° 158° 158° 158° 1	Existing or Planned	Well ID	Latitude/ Longitude		Unit	Diameter and Type (O.D. in.)	Interval (ft)	Diameter and Type (O.D. in.)	Interval (ft)	Length (ft)	Туре	Interval (ft)	Surface Elevation (ft)	Point Elevation (ft)	Screened Interval (ft)	Geologic Contact	Distance <sup>(d)</sup> (ft)
Pagoo   33-2' 41.8Th   288   Oxide   6.58 PVC   2.0 to 808   6.58 PVC   661 to 721   60   General   0 to 500   1461.8     Ogg-CL   111726 '58'W   1288   Oxide   59/16 PVC   0.9 to 661   59/16 PVC   661 to 721   60   General   0 to 500   1461.2     Ogg-CL   111726 '14"W   455   LBFU   59/16 PVC   20 to 355   59/16 PVC   661 to 721   60   General   0 to 50   0 to 50   0 to 60     Chart   111726 '14"W   455   LBFU   59/16 PVC   20 to 355   59/16 PVC   740 to 800   60   General   0 to 20   0 to 20     Chart   111726 '14"W   255   LBFU   59/16 LCS   0 to 200   59/16 PVC   740 to 800   60   General   0 to 20   0 to 20     Chart   111726 '14"W   255   LBFU   59/16 LCS   0 to 200   59/16 PVC   740 to 800   60   General   0 to 20   1485°     Oxide   59/16 LCS   0 to 200   59/16 PVC   20 to 315   59/16 PVC   20 to 315   20/16 PVC   20 to 315   20/16 PVC   20 to 315   20/16 PVC   20 to 315   20/16 PVC   20 to 316   20/16 PVC   20 to 316   20/16 PVC   20 to 316   20/16 PVC   20 to 316   20/16 PVC   20 to 316   20/16 PVC   20 to 316   20/16 PVC   20 to 316   20/16 PVC   20 to 316   20/16 PVC   20 to 316   20/16 PVC   20 to 316   20/16 PVC   20 to 316   20/16 PVC   20 to 316   20/16 PVC   20 to 316   20/16 PVC   20 to 316   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC   20/16 PVC	Point of	Complian	ce Wells													:	
Q99-GL         111726 '13"W         740   LBFU         5916 PVC         -9 in 661         5716 PVC         661 in 721         60         Gement         0 to 20         14612           C <sub>Gurn</sub> 111726 '13"W         436         LBFU         5916 PVC         20 in 20         Coment         0 to 20         1485%           C <sub>Gurn</sub> 111726 '44"W         455         LBFU         5916 LCS         0 to 20         S716 PVC         740 in 800         60         Bentonite         20 to 23         1485%           C <sub>Gurn</sub> 111726 '44"W         820         LBFU         5916 LCS         0 to 20         S916 PVC         740 in 800         60         Bentonite         20 to 20         1485%           C <sub>Gurn</sub> 111726 '35"W         820         15 Fig         PVC         740 in 800         60         Bentonite         20 to 20         1485%           D <sub>Das</sub> 111726 '35"W         111726 '35"W         111727 '35"W         111727 '35"W         111727 '35"W         111727 '35"W         111727 '35"W         111727 '35"W         111727 '35"W         111727 '35"W         111727 '35"W         111727 '35"W         111727 '35"W         111727 '35"W         111727 '35"W         111727 '35"W         111727 '35"W         111727 '35"W         111727 '35"W	Щ	P49-O	33°2' 41.8"N 111°26' 5.8"W	1288	Oxide	6 5/8 PVC	-2.0 to 808	6 5/8 PVC	808 to 1222	414	Cement Bentonite	0 to 20 20 to 760	1461.8	1463.12	1015	LBFU/Oxide Oxide/Sulfide	+250 NA
C <sub>LBP</sub> 33°3′ 16.4°N         435         LBFU         5 9/16 LCS         0 to 20         5 9/16 PVC         375 to 435         60         Bentonite         20 to 23         1485°°           C <sub>LBP</sub> 111726′ 3.9°W         435         LBFU         5 9/16 LCS         0 to 740         5 9/16 PVC         740 to 800         60         Cement         0 to 20         1485°°           C <sub>LBP</sub> 111726′ 3.9°W         820         18FU         5 9/16 LCS         0 to 740         5 9/16 PVC         740 to 800         Cement         0 to 20         1485°°           D <sub>bar</sub> 111726′ 3.9°W         820         18FU         5 9/16 LCS         0 to 20         5 9/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         39/16 PVC         400 to 550         150         Cement         0 to 20         1486°°           E <sub>tb</sub> 111725′ 3.5°         30.0°         5 9/16 PVC         20 to 20         5 9/16 PVC	ш	O49-GL	33°2′ 41.7″N 111°26′ 7.3″W	740	LBFU		199 ot 6:0-	5 9/16 PVC	661 to 721	09	Cement Bentonite	0 to 20 20 to 610	1461.2	1462.08	681	MFGU/LBFU LBFU/Oxide	+381
C <sub>LIM</sub> 33°3° 16,4°N         upper         5 9/16 LCS         0 b 20         5 9/16 PVC         375 to 435         60         Bentonite         20 to 355         1485°°           C <sub>LIM</sub> 111°26′ 39°W         45         LBPU         5 9/16 LCS         0 to 20         5 9/16 PVC         20 to 355         5 9/16 PVC         135 to 435         60 to 20         1485°°           C <sub>LIM</sub> 111°26′ 39°W         111°26′ 39°W         10 to 20         5 9/16 LCS         0 to 20         5 9/16 PVC         20 to 800         110°         20         1485°°           C <sub>LIM</sub> 111°26′ 39°W         111°26′ 39°W         33°9′ 129°W         30°0 110°         20         Bentonite         20 to 830         1485°°           D <sub>LM</sub> 111°26′ 39°W         33°9′ 129°W         39°16 LCS         0 to 20         59′16 PVC         30°16 PVC         315 to 330         15         Bentonite         20 to 20         1485°°           D <sub>LM</sub> 111°26′ 33°W         33°9′ 129°W         39°16 LCS         0 to 20         59′16 PVC         30°16 PVC         316 to 20         150° 1380         1485°°           D <sub>LM</sub> 111°25′ 36°W         30°16 LCS         0 to 20         59′16 PVC         20° to 30°         150° 16 PVC         20° to 30° <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>ļ</td><td></td><td></td><td></td><td></td><td></td></t<>												ļ					
C <sub>LBT</sub> 333-31 64"N         820         LBFU         5 9/16 LCS         0 to 740         5 9/16 PVC         740 to 800         60         Bentonite         20 to 720         1485%           C <sub>LBT</sub> 111726 3.39"W         820         LBFU         5 9/16 LCS         0 to 900         5 9/16 PVC         900 to 1100         200         Bentonite         20 to 20         1485%           D <sub>DAS</sub> 111726 3.37"W         3193-7 L29"N         340/16 LCS         0 to 20         5 9/16 PVC         20 to 315         5 9/16 PVC         315 to 330         15         Bentonite         20 to 295         1485%           D <sub>DAS</sub> 111726 3.37"W         360         5 9/16 LCS         0 to 20         5 9/16 PVC         20 to 315         5 9/16 PVC         400 to 550         150         Bentonite         20 to 295         1485%           B <sub>DAS</sub> 111725 46.1"W         88         Oxide         5 9/16 PVC         20 to 310         5 9/16 PVC         400 to 550         150         Bentonite         20 to 380         1486%           B <sub>DAS</sub> 111725 46.1"W         835         Oxide         5 9/16 PVC         20 to 310         5 9/16 PVC         20 to 50         20 to 50         100 to 50         100 to 50         100 to 50         100 to 20 <td>рс</td> <td>2</td> <td>33°3' 16.4"N 111°26' 4.4"W</td> <td>455</td> <td>upper</td> <td>5 9/16 LCS 5 9/16 PVC</td> <td>0 to 20 20 to 355</td> <td>5 9/16 PVC</td> <td>375 to 435</td> <td>09</td> <td>Cement Bentonite</td> <td>0 to 20 20 to 355</td> <td>1485(9)</td> <td>NA</td> <td>405</td> <td>UBFU/LBFU LBFU/Oxide</td> <td>+80</td>	рс	2	33°3' 16.4"N 111°26' 4.4"W	455	upper	5 9/16 LCS 5 9/16 PVC	0 to 20 20 to 355	5 9/16 PVC	375 to 435	09	Cement Bentonite	0 to 20 20 to 355	1485(9)	NA	405	UBFU/LBFU LBFU/Oxide	+80
Construct         Oxide         5 9/16 LCS         0 to 900         5 9/16 PVC         900 to 1100         200 to 880         1485%           D <sub>LBF</sub> 111°26′ 33"W         1120         Oxide         5 9/16 LCS         0 to 900         5 9/16 PVC         315 to 330         15 to 880         1485%         1485%           D <sub>LBF</sub> 111°26′ 346."W         340         LBFU         5 9/16 LCS         0 to 20         5 9/16 PVC         20 to 315         5 9/16 PVC         315 to 330         15 Gement         0 to 20         1485%           D <sub>Dox</sub> 111°25′ 46."W         340         LBFU         5 9/16 LCS         0 to 20         5 9/16 PVC         20 to 400         5 9/16 PVC         310 to 330         1485%         1485%           E <sub>LBF</sub> 111°25′ 46.1"W         585         Oxide         5 9/16 PVC         20 to 400         5 9/16 PVC         400 to 550         150         Gement         0 to 20         1485%           E <sub>LBF</sub> 111°25′ 46.1"W         58         Oxide         5 9/16 PVC         20 to 20         5 9/16 PVC         20 to 20         5 9/16 PVC         400 to 550         150         Gement         0 to 20         1480%           E <sub>Day</sub> 111°25′ 36.7"W         5 9/16 PVC         20 to 20 <td< td=""><td>þe</td><td>C E</td><td>33°3' 16.4"N 111°26' 3.9"W</td><td>820</td><td>lower</td><td>5 9/16 LCS</td><td>0 to 740</td><td>5 9/16 PVC</td><td>740 to 800</td><td>60</td><td>Cement Bentonite</td><td>0 to 20 20 to 720</td><td>1485(e)</td><td>Ϋ́</td><td>770</td><td>UBFU/LBFU LBFU/Oxide</td><td>+445</td></td<>	þe	C E	33°3' 16.4"N 111°26' 3.9"W	820	lower	5 9/16 LCS	0 to 740	5 9/16 PVC	740 to 800	60	Cement Bentonite	0 to 20 20 to 720	1485(e)	Ϋ́	770	UBFU/LBFU LBFU/Oxide	+445
D <sub>LBF</sub> 133°3′12.94°N         340°1 LBFU         5 9/16 LCS         0 to 20         315 to 330         15         Cement         0 to 20         1485°0           D <sub>DAS</sub> 111°25′ 46.6°W         340         LBFU         5 9/16 LCS         0 to 20         5 9/16 PVC         315 to 330         15         Bentonite         20 to 295         1485°0           B <sub>LBF</sub> 111°25′ 46.1°W         585         Oxide         5 9/16 LCS         0 to 20         5 9/16 PVC         20 to 400         5 9/16 PVC         310 to 330         150         Bentonite         20 to 390         1485°0           E <sub>LBF</sub> 111°25′ 36.9°W         340         LBFU         5 9/16 LCS         0 to 20         5 9/16 PVC         310 to 330         20         Bentonite         20 to 390         1480°0           E <sub>CMF</sub> 111°25′ 36.4°W         535         Oxide         5 9/16 LCS         0 to 20         5 9/16 PVC         400 to 500         100         20         1480°0           F <sub>DMF</sub> 111°25′ 36.4°W         535         Oxide         5 9/16 LCS         0 to 20         5 9/16 PVC         400 to 500         100         1480°0         1480°0           F <sub>DMF</sub> 111°25′ 36.4°W         245         UBFU         5 9/16 PVC <t< td=""><td>ğ</td><td>Š</td><td>33°3' 16.4"N 111°26' 3.3"W</td><td>1120</td><td>Oxide</td><td>\$ 9/16 LCS</td><td>0 to 900</td><td>5 9/16 PVC</td><td>900 to 1100</td><td>200</td><td>Cement Bentonite</td><td>0 to 20 20 to 880</td><td>1485(6)</td><td>NA</td><td>1000</td><td>LBFU/Oxide</td><td>+150</td></t<>	ğ	Š	33°3' 16.4"N 111°26' 3.3"W	1120	Oxide	\$ 9/16 LCS	0 to 900	5 9/16 PVC	900 to 1100	200	Cement Bentonite	0 to 20 20 to 880	1485(6)	NA	1000	LBFU/Oxide	+150
D <sub>LMS</sub> 33°3′ 12.94″N         340         LBFU         5 9/16 LCS         0 to 20         5 9/16 PVC         315 to 330         15         Cement Bentonite         20 to 295         1485%           D <sub>CMS</sub> 111°25′ 46.6″W         340         LBFU         5 9/16 LCS         0 to 20         5 9/16 PVC         20 to 400         5 9/16 PVC         400 to 550         150         Bentonite         20 to 295         1485%           B <sub>LMS</sub> 111°25′ 46.1″W         585         Oxide         5 9/16 LCS         0 to 20         5 9/16 PVC         400 to 550         150         Bentonite         20 to 380         1485%           E <sub>LMS</sub> 111°25′ 36.9″W         340         LBFU         5 9/16 LCS         0 to 20         5 9/16 PVC         20 to 300         16 PVC         400 to 500         Cement         0 to 20         1480%           E <sub>LMS</sub> 111°25′ 36.9″W         340         LBFU         5 9/16 LCS         0 to 20         5 9/16 PVC         20 to 30         10 to 30         1480%           E <sub>DMS</sub> 111°25′ 36.4″W         535         Oxide         5 9/16 LCS         0 to 20         5 9/16 PVC         20 to 105         100 to 20         100 to 20         100 to 20         1480%           F <sub>DMS</sub> 111°25′											į			•			
Dox         111°25° 46.1"W         585         Oxide         59/16 LCS         0 to 20         59/16 PVC         20 to 400         5 9/16 PVC         400 to 550         150         Bentonite         20 to 380         1485 <sup>49</sup> E <sub>Lisp</sub> 111°25° 46.1"W         585         Oxide         5 9/16 LCS         0 to 20         5 9/16 PVC         20 to 20         150         Bentonite         20 to 290         1480 <sup>49</sup> E <sub>Lisp</sub> 111°25° 36.9"W         340         LBFU         5 9/16 LCS         0 to 20         59/16 PVC         310 to 330         20         Bentonite         20 to 290         1480 <sup>49</sup> E <sub>Lisp</sub> 111°25° 36.9"W         340         LBFU         5 9/16 LCS         0 to 20         59/16 PVC         400 to 500         100         Bentonite         20 to 380         1480 <sup>49</sup> E <sub>Lisp</sub> 111°25° 36.4"W         535         Oxide         5 9/16 PVC         20 to 400         5 9/16 PVC         125 to 225         100         Bentonite         20 to 136         1475 <sup>49</sup> E <sub>lisp</sub> 111°25° 20.5"W         245         UBFU         5 9/16 PVC         20 to 120         5 9/16 PVC         125 to 225         100         Bentonite         20 to 106         1490 <sup>49</sup>	Pe	D	33°3° 12.94"N 111°25° 46.6"W	340		5 9/16 LCS 5 9/16 PVC	0 to 20 20 to 315	5 9/16 PVC	315 to 330	15	Cement Bentonite	0 to 20 20 to 295	1485(4)	NA	322.5	MFGU/LBFU LBFU/Oxide	+12.5
E <sub>I.PF</sub> 33°3′ 12.9°N         34°3′ 12.9°N         34°0′ 12.9°N         34°0′ 12.9°N         34°0′ 12.9°N         34°0′ 12.9°N         34°0′ 12.9°N         34°0′ 12.9°N         34°0′ 12.9°N         34°0′ 12.9°N         39°16 LCS         0 to 20         59′16 PVC         20 to 310         59′16 PVC         310°10 330         20         Bentonite         20 to 20         1480°0           E <sub>OX</sub> 111°25′ 36.4°W         535         Oxide         59′16 PVC         20 to 40°         59′16 PVC         40°0 to 50°         10°         Bentonite         20 to 38°         1480°0           F <sub>UBF</sub> 111°25′ 20.5°W         245         UBFU         59′16 PVC         20 to 20°         59′16 PVC         125 to 225         10°         Bentonite         20 to 10°         1475°0           G <sub>Ing</sub> 111°25′ 20.5°W         240         UBFU         59′16 PVC         20 to 12°         59′16 PVC         12° to 22°         10°         Bentonite         20 to 10°         149°°	ŝ.	Dox	33°3° 12.9"N 111°25° 46.1"W	585		5 9/16 LCS 5 9/16 PVC	0 to 20 20 to 400	5 9/16 PVC	400 to 550	150	Cement Bentonite	0 to 20 20 to 380	1485(*)	NA	475	LBFU/Oxide Oxide/Sulfide	+125
E <sub>IBF</sub> 33°3′ 12.9°N         34°3′ 12.9°N         59/16 LCS         0 to 20         59/16 PVC         20 to 310         59/16 PVC         310 io 330         20         Bentonite         20 to 290         1480 <sup>(d)</sup> E <sub>MB</sub> 111°25′ 36.9°W         340°3′ 12.9°N         59/16 PVC         20 to 310         59/16 PVC         20 to 400         59/16 PVC         400 to 500         100         Bentonite         20 to 380         1480 <sup>(d)</sup> E <sub>OX</sub> 111°25′ 36.4°W         535         Oxide         59/16 PVC         20 to 400         59/16 PVC         400 to 500         100         Bentonite         20 to 380         1480 <sup>(d)</sup> F <sub>DBF</sub> 111°25′ 36.4°W         245         UBFU         59/16 PVC         20 to 125         59/16 PVC         125 to 225         100         Bentonite         20 to 105         1475 <sup>(d)</sup> G <sub>IBF</sub> 33°3′ 14.1°N         59/16 PVC         20 to 120         59/16 PVC         125 to 225         100         Bentonite         20 to 100         1490 <sup>(e)</sup>																	
E <sub>OX</sub> 33°3' 12.9"N         5 9/16 LCS         0 to 20         5 9/16 PVC         20 to 400         5 9/16 PVC         400 to 500         100         Bentonite         20 to 380         1480 <sup>(e)</sup> F <sub>D3P</sub> 111°25' 36.4"W         535         Oxide         5 9/16 PVC         20 to 400         5 9/16 PVC         400 to 500         100         Bentonite         20 to 380         1480 <sup>(e)</sup> F <sub>D3P</sub> 111°25' 20.5"W         245         UBFU         5 9/16 LCS         0 to 20         5 9/16 PVC         125 to 225         100         Bentonite         20 to 105         1475 <sup>(e)</sup> G <sub>Inst</sub> 111°25' 6.2"W         246         UBFU         5 9/16 PVC         20 to 120         5 9/16 PVC         120 to 220         100         Bentonite         20 to 100         1490 <sup>(e)</sup>	<u>§</u>	R.	33°3' 12.9"N 111°25' 36.9"W	340	LBFU	5 9/16 LCS 5 9/16 PVC	0 to 20 20 to 310	5 9/16 PVC	310 io 330	20	Cement Bentonite	0 to 20 20 to 290	1480 <sup>(d)</sup>	NA	320	MFGU/LBFU LBFU/Oxide	+20
33°3′3′6″N 245 UBFU 59/16 LCS 0 to 20 59/16 PVC 125 to 225 100 Bentonite 20 to 105 1475 <sup>(c)</sup> Gine 111°25′5 6.2″W 240 UBFU 59/16 PVC 20 to 120 59/16 PVC 120 to 220 100 Bentonite 20 to 100 1490 <sup>(c)</sup>	<u> </u>	Eox	33°3° 12.9"N 111°25° 36.4"W	535		5 9/16 LCS 5 9/16 PVC	0 to 20 20 to 400	5 9/16 PVC	400 to 500	100	Cement Bentonite	0 to 20 20 to 380	1480(e)	NA	450	LBFU/Oxide Oxide/Sulfide	+100
F <sub>DBF</sub> 33°3′3.6"N 245 UBFU 59/16 LCS 0 to 20 59/16 PVC 125 to 225 100 Bentonite 20 to 105 1475 <sup>(e)</sup> Centent 0 to 20 1475 <sup>(e)</sup> 141°25′20.5"W 246 UBFU 59/16 LCS 0 to 20 59/16 PVC 120 to 220 100 Bentonite 20 to 100 1490 <sup>(e)</sup>									3								
33°3′ 14.1"N	Pe	Fusiv	33°3° 3.6"N 111°25° 20.5"W	245		5 9/16 LCS 5 9/16 PVC	0 to 20 20 to 125	5 9/16 PVC	125 to 225	001	Centent Bentonite	0 to 20 20 to 105	1475(e)	NA	175	Alluvium/UBFU UBFU/MFGU	+95 -75
┨	P <sup>(c)</sup>	G <sub>tiBr</sub>	33°3° 14.1"N 111°25° 6.2"W	240		5 9/16 LCS 5 9/16 PVC	0 to 20 20 to 120	5 9/16 PVC	120 to 220	001	Cement Bentonite	0 to 20 20 to 100	1490(e)	NA	170	Alluvium/UBFU UBFU/MFGU	08-

Table 52	-1 Propo	Table 5.2.1 Proposed Point of Compliance and Ungradient Monitoring Wells - Well Location, Construction, and Lithology	ndiance	and Upgra	dient Monitor	ing Wells - M	'ell Location, '	Construction,	and Lithol	logy						
					Casing	20		Screen			Annular Scal		C	Depth	Distance from Center of Screen to Geologic Contact	Center of gic Contact
Existing or Planned	Existing or Planned Well ID	Latitude/ Longitude	Total Depth	Unit	Diameter and Type (O.D. in.)	Interval (ft)	Diameter and Type (O.D. in.)	Interval (ft)	Length (fi)	Туре	Interval (ft)	Surface Elevation (ft)	Reference Point Elevation (ft)	Screened Interval (ft)	Geologic Contact	Distance <sup>(4)</sup> (ft)
Upgradie	ent Monite	Upgradient Monitoring Wells														
9 9	M2-GU	33°2' 37"N M2-GU 111°25' 18.3"W	270	UBFU	5 9/16 LCS 5 9/16 PVC	-1.8 to 18 18 to 181	\$ 9/16 PVC	198 to 237	39	Cement Bentonite	0 to 19 19 to 170	1459	1460.80	217	Alluvium/UBFU UBFU/MFGU	+147
. ®3	M3-GL	33°2' 36.5"N M3-GL 111°25' 18.5"W	370	LBFU	5 9/16 LCS 5 9/16 PVC	-1.9 to 19 19 to 298	5 9/16 PVC	298 to 338	40	Cement Bentonite	0 to 20 20 to 270	1458.8	1460.74	318	MFGU/LBFU LBFU/Oxide	+47 -53
<b>₩</b>	M4-0	33°2' 36.8"N 111°25' 18.5"W	510	Oxide	5 9/16 LCS 5 9/16 PVC	-1.7 to 19 19 to 405	5 9/16 PVC	405 to 464	59	Cement Bentonite	0 to 20 20 to 380	1458.9	1460.60	434	LBFU/Oxide Oxide/Sulfide	+64
þ(e)	H <sub>effs</sub>	33°3° 47.4"N 111°24° 33.2"W	245	UBFU	5 9/16 LCS 5 9/16 PVC	0 to 20 20 to 125	5 9/16 PVC	125 to 225	001	Cement Bentonite	0 to 20 20 to 105	1460(e)	NA	175	Alluvium/UBFU UBFU/MFGU	+95 -75

<sup>(</sup>a) LCS casing placed over the PVC at M6-GU to provide structural support for the dedicated pump.

<sup>(</sup>b) Wells have dedicated pumps installed.

<sup>(</sup>c) Planned well completion details estimated and subject to slight adjustment.

<sup>(</sup>d) Positive values represent distance above the center of the screened interval; negative values are below.

<sup>(</sup>e) Surface elevation estimated, the planned wells will be surveyed after completion.

LCS - Low Carbon Steel.

PVC - Polyvinyl Chloride.

SS - Stainless Steel

UBFU - Upper Basin-Fill Unit.

MFGU - Middle Fine-Grained Unit.

LBFU - Lower Basin-Fill Unit.

E - Existing well.

P - Planned well.

NA - Data not available.

All existing well screened intervals are sand packed with #6-9 Colorado silica sand to approximately 50 feet above the top of screened interval and 10 feet of #30 silica sand.

Table 5.3-1 Water Quality Variables - Level 1		
Water Quality Variables	AL (mg/L)	Analytical Method
Fluoride*	TBD	EPA 340.2
Magnesium	TBD	EPA 200.7
Sulfate	TBD	EPA 300
Total Dissolved Solids	TBD	EPA 160.1
pH	NA	EPA 150.1
Specific Conductance	NA	EPA 120.1
Temperature	NA	NA

<sup>\*</sup>AQL to be determined

NA - Not applicable

TBD - To be determined

AL - Alert Level

AQL - Aquifer Quality Limit

Table 5.3-2 Water Quality Variables - Level 2		
WATER QUALITY VARIABLES	AQL (mg/L)	Analytical Method
Selected Constituen	ts With AWQSs	
Antimony	TBD	EPA 200.7
Arsenic	TBD	EPA 206.2
Barium	TBD	EPA 200.7
Beryllium	TBD	EPA 200.7
Cadmium	TBD	EPA 200.7
Chromium	TBD	EPA 218.2
Lead	TBD	EPA 239.2
Mercury	TBD	EPA 245.1
Nickel	TBD	EPA 200.7
Selenium	TBD	EPA 270.2
Thallium	TBD	EPA 279.2
Radionu	clides	
Gross Alpha	TBD	EPA 900.0
Gross Beta	TBD	EPA 900.0

Table 5.3-2 Water Quality Variables - Level 2		
Radium-226	TBD	EPA 901.1 or EPA 903/904
Radium-228	TBD	EPA 901.1 or EPA 903/904
Radon 222	NA	Emination 903 or Lucas (Cell)
Total Uranium (natural)	NA	908.0 or SM 7500
Other Var	iables	
Aluminum	NA	EPA 204.2
Bicarbonate	NA	EPA 310.1
Calcium	NA	EPA 200.7
Carbonate	NA	EPA 310.1
Cobalt	NA	EPA 200.7
Chloride	NA	EPA 300
Copper	NA	EPA 200.7
Iron	NA	EPA 200.7
Manganese	NA	EPA 200.7
Nitrate	NA	EPA 300
Silver	NA	EPA 200.7
Sodium	NA	EPA 200.7
Potassium	NA	EPA 200.7
Zinc	NA	EPA 200.7
ТРН	NA	EPA 8015M
TRPH	NA	EPA 418.1

NA - Not applicable

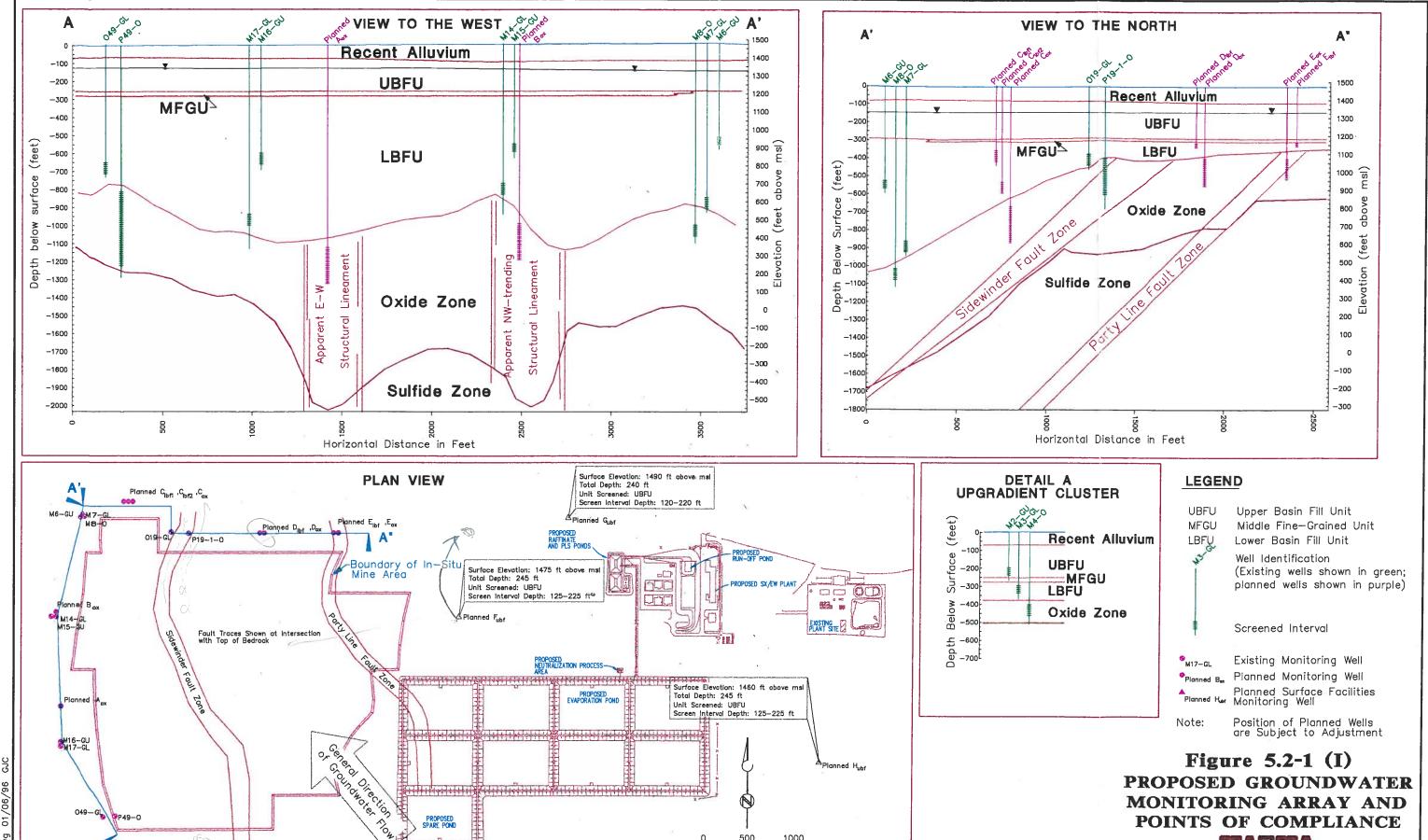
TBD - To be determined

TPH - Total Petroleum Hydrocarbons

TRPH - Total Recoverable Petroleum Hydrocarbons

AQL - Aquifer Quality Limit

			•



Scale in feet

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Florence, Arizona

M3-GL 80 M4-0 → See Detail A

